

ANSWER THIS PROBLEM USING THE FIELD BELOW

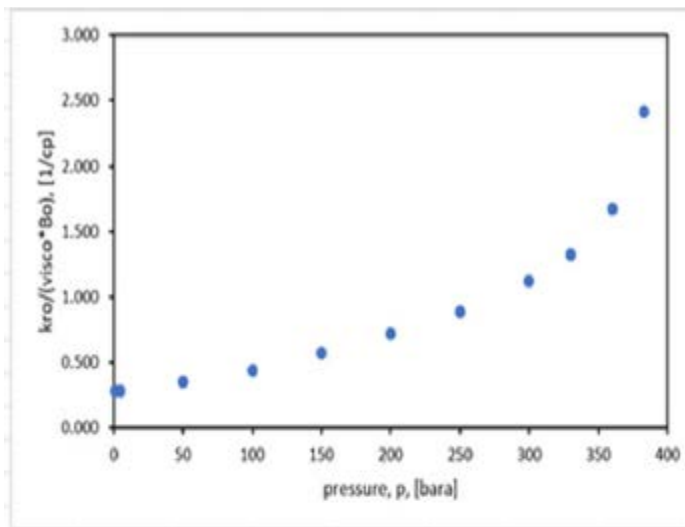
PROBLEM 1 (5 POINTS). When deriving analytically the IPR equation for a saturated oil well with solution gas drive, one needs to integrate the term $k_{ro}/(B_o \cdot \mu_o)$ from bottom-hole to reservoir pressure.

Task 1 (2 POINTS). Make a sketch showing how does the term $k_{ro}/(B_o \cdot \mu_o)$ behaves versus pressure.

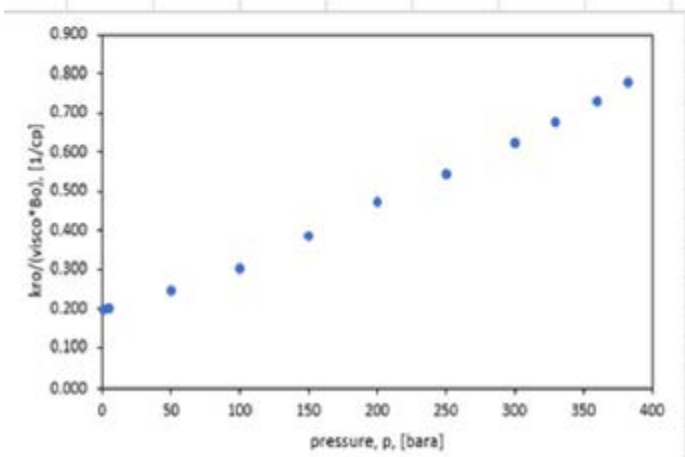
Task 2 (3 POINTS). In the video lectures, for one particular case, the output of the analytical derivation was Vogel's equation. What assumptions must be taken for this to occur?

SOLUTION:

Task 1. Some examples from video lecture 19:



NOT LINEAR!!!



LINEAR??

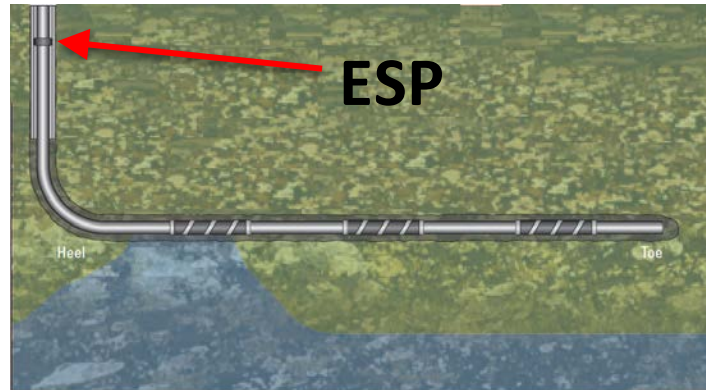
Task 2.

Vogel's equation was obtained if the term $k_{ro}/(B_o \cdot \mu_o)$ is assumed to be linear with pressure, and the value at the origin is equal to 1/9 the value at reservoir pressure.

SOLVE THIS PROBLEM USING THE EXCEL FILE PROVIDED

PROBLEM 2 (20 POINTS). Estimation and verification of ESP requirements

The Rio Ariari complex is a field currently under development in the region of “Los llanos” in Colombia. The reservoir has a thin layer (19 m) containing undersaturated oil and a very strong bottom aquifer. There is coning from the water layer into the well. The field will be produced with ESP-lifted horizontal wells like the one shown in the figure below.



The Wood company has proposed a unique ESP model (TE7000) with 50 stages which they claim has a wide operational envelope to handle all possible well operational conditions. Your task is to estimate and verify the ESP requirements for a well in the Ariari Field.

TASKS:

Task 1 (5 POINTS). What is the effective viscosity (in cP) of the oil-water mixture (using the Richardson emulsion equation) when the well is producing a total liquid rate of 250 Sm³/d with 54% water cut?

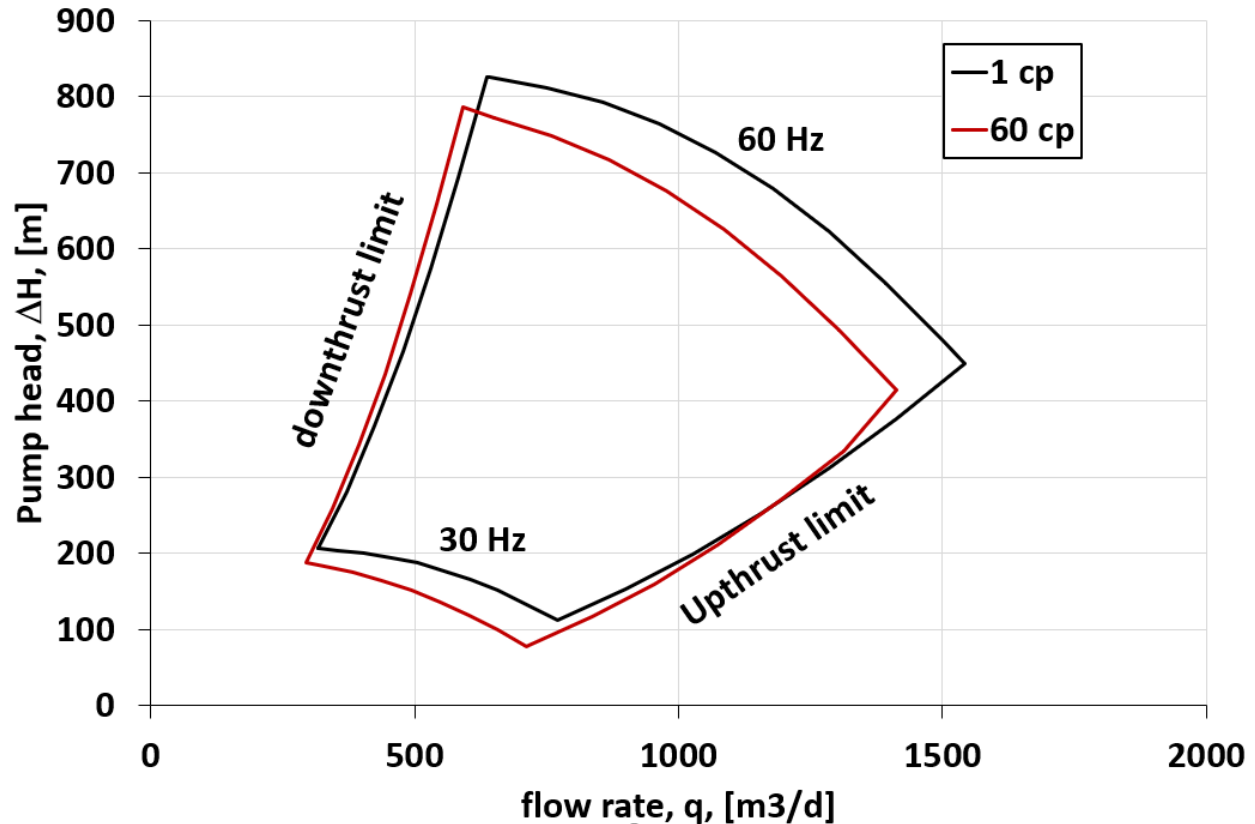
Explain how you have performed this task.

Task 2 (10 POINTS). -For the total liquid rates of 250 Sm³/d, estimate the required pump pressure boost (DP in bar, input a positive number) and pump power (in kW) to deliver the rate if the wellhead pressure is constant and equal to 40 bara.

Explain how you have performed this task.

Task 3 (5 POINTS). -According to the ESP envelope given below, will the ESP model suggested be able to deliver the desired rate of 250 Sm³/d?

Explain how you have performed this task.



Additional information

- Neglect the flow pressure drop from the bottom-hole to the pump suction (i.e. $p_{\text{suc}} = p_{\text{wf}}$).
- Assume that the oil compressibility and GOR can be neglected such as the rate at standard conditions is equal to the rate at local conditions p and T .
- The Water cut (WC , in fraction) is defined as

$$WC = \frac{q_w}{q_o + q_w}$$

- The well inflow can be represented with a linear PI equation:

$$q = J \cdot (p_R - p_{\text{wf}})$$

Where:

qtotal liquid rate in Sm^3/d

Jproductivity index for total liquid flow [**100 $\text{Sm}^3/\text{d}/\text{bar}$**],

p_Rreservoir pressure [**82.7 bara**]

p_{wf}bottom-hole flowing pressure [bara]

This equation is programmed in VBA functions called “IPRq” and “IPRpwf” provided in the Excel sheet. IPRq is the equation provided above. IPRpwf is when p_{wf} is cleared out in the equation above.

- The density of the oil water mixture is calculated using the following expression:

$$\rho_m = WC \cdot \rho_w + (1 - WC) \cdot \rho_o$$

Where the water density is 1025 kg/m^3

The oil density is 897 kg/m^3

WC is input in fraction.

This equation is programmed in a VBA function called “Avprop” provided in the Excel sheet.

- The oil+water mixture exhibits an emulsion behavior where its viscosity is a function of the water volume fraction. The cutoff watercut is 60%.

Regime	Richardson emulsion viscosity
Oil continuous (WC < 60%)	$\mu_m = \mu_o \cdot e^{3.215 \cdot WC}$
Water continuous (WC > 60%)	$\mu_m = \mu_w \cdot e^{3.089 \cdot (1-WC)}$

The viscosity of the oil is 10 cp and viscosity of the water is 1 cp (1 cp = 1 E-3 Pa s). **WC is input in fraction.**

This equation is programmed in a VBA function called “Rich_emul_visc” provided in the Excel sheet.

- The pump power [in watts, W] can be estimated with:

$$Power = \frac{q \cdot \Delta p \cdot 1E5}{\eta \cdot 24 \cdot 3600}$$

Where Δp [bara], q in [m³/d]. Assume a constant pump efficiency (η) of 0.6.

This equation is programmed in a VBA function called “ESPpower” provided in the Excel sheet.

- The pump head [m] is

$$\Delta h = \frac{\Delta p \cdot 10^5}{\rho_m \cdot g}$$

Where Δp [bara], ρ_m [kg/m³] and $g = 9.81$ [m/s²]

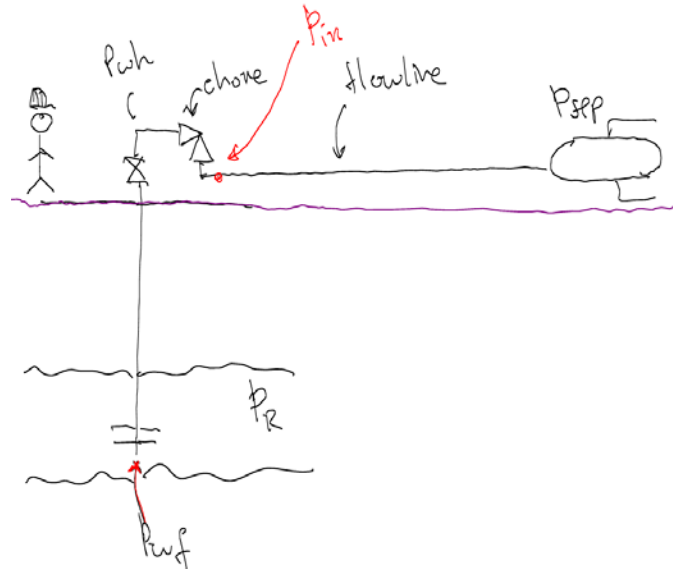
- Two VBA functions are provided in the Excel sheet to calculate pressure drop in pipe for incompressible flow:
 - “pin” allows to estimate required pressure at the inlet of the pipe if outlet pressure and rate are provided.
 - “pout” allows to estimate available pressure at the pipe outlet if inlet pressure and rate are provided.

- **SOLUTION:**
- See the excel file attached.

SOLVE THIS PROBLEM USING THE EXCEL FILE PROVIDED

PROBLEM 3 (15 POINTS).

Consider the dry gas production system shown in the figure below:



Assume that the wellhead choke is 20% closed and that the system is producing a dry gas rate of 2.0 E6 Sm³/d.

Task (15 POINTS): The engineering team wants to increase the well rate by opening the wellhead choke, but this might take time since the well is located in a remote location with difficult access and the choke is manually actuated. Instead of opening the choke, a member of the team has suggested to route the production of the well to another separator that has lower pressure (20 bara). **Assess this idea and provide your recommendation.**

Additional information:

- The choke critical pressure ratio is 0.5
- Neglect the pressure drop in the flowline, i.e. assume $p_{in} = p_{sep} = 40$ bara
- Use the following equations:

Inflow equation:

$$q_g = C_R \cdot (p_R^2 - p_{wf}^2)^n$$

With

$$C_R = 104 \text{ Sm}^3/\text{d}/\text{bar}^{2n}$$

$$n = 0.9$$

$$p_R = 304 \text{ bara}$$

Tubing equation:

$$q_g = C_T \cdot \left(\frac{p_{wf}^2}{e^S} - p_{wh}^2 \right)^{0.5}$$

$$C_T = 4.41 \text{ E4 Sm}^3/\text{d}/\text{bar}$$

$$S = 0.31$$

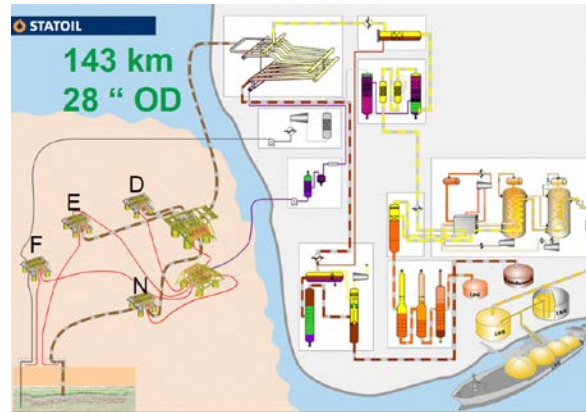
SOLUTION

See the Excel file attached.

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PROBLEM 4 (25 POINTS). Flow equilibrium in the Snøhvit CO₂ injection well using the equations for incompressible liquid flow.

The Snøhvit field is a subsea dry gas field, located in the Barents Sea. The field produces to a LNG facility on the island of Melkøya through a pipeline that is 140 km long. In the LNG plan, CO₂ is captured, it is then pumped and transported for 140 km back to the field and injected in a deep formation (Tubåen). The CO₂ is injected in an aquifer, but in this problem, we will assume that the layer has only CO₂.



Task (25 POINTS). Perform a flow equilibrium calculation in the Snøhvit CO₂ injection well to find the equilibrium rate. Use the well bottom-hole as equilibrium point. Plot the IPR and TPR. Explain how you have performed this task.

Additional information:

- The maximum allowed flowing bottom-hole pressure is 390 bara (to avoid fracking the reservoir)
- For the IPR use a linear equation with $J = 240$ [t/d/bar]. Assume a reservoir pressure equal to 300 bara.
- Assume the wellhead pressure is kept fixed at a value of 100 bara.
- For the TPR use the Bernoulli equation for pressure drop in conduit for incompressible liquid flow. Two VBA equations are provided in the Excel file:
 - “pin” that allows to calculate required inlet pressure if outlet pressure and mass flow are given
 - “pout” that allows to calculate available pressure at the discharge of the pipe if inlet pressure and mass flow are given
- It is recommended you perform your flow equilibrium calculations using mass flow rate instead of standard conditions volumetric rates or local conditions volumetric rates.

- SOLUTION
- See the Excel file attached.
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SOLVE THIS PROBLEM USING THE EXCEL FILE PROVIDED

PROBLEM 5 (25 POINTS).

A pressure survey has been performed in a producing oil well (production rate of 1394 Sm³/d and GOR = 155.1), and pressure and temperature at several depths have been recorded. The values are provided in the Excel file attached.

Task (25 POINTS). Calculate the following variables along the well:

- Non-slip gas volume fraction
- Gas void fraction
- Oil and gas real velocities
- The slip ratio
- The hydrostatic pressure gradient

Useful information:

- ε is the gas void fraction, equal to:

$$\varepsilon = \frac{A_g}{A_l + A_g}$$

A VBA function named “e_simpson” is provided to calculate the void fraction using the gas density, liquid density, and non-slip gas volume fraction (λ_g).

- The following matrix to convert from standard conditions to local conditions

$$\begin{bmatrix} q_g \\ q_o \\ q_w \end{bmatrix} = \begin{bmatrix} \frac{B_g}{1 - R_s \cdot r_s} & \frac{-R_s \cdot B_g}{1 - R_s \cdot r_s} & 0 \\ -B_o \cdot r_s & B_o & 0 \\ \frac{1 - R_s \cdot r_s}{0} & \frac{1 - R_s \cdot r_s}{0} & B_w \end{bmatrix}_{(p,T)} \cdot \begin{bmatrix} q_{\bar{g}} \\ q_{\bar{o}} \\ q_{\bar{w}} \end{bmatrix}$$

There are two VBA functions available in the Excel sheet.: “qg_local”, to calculate local gas rates from SC oil and gas rates and black oil properties and “qo_local”, to calculate local oil rates from SC oil and gas rates and black oil properties

- A VBA function called “TwoDimInterpol” is provided to find BO properties at any p-T by interpolating on the table provided on the sheet “BO_tables”

SOLUTION

See the Excel file attached.

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PROBLEM 6 (10 POINTS).

A test has been performed on an oil well and the following pairs of oil rate and flowing bottomhole pressure are reported:

Test point	qo [Sm3/d]	pwf [bara]
1	1080	270
2	2050	180

The reservoir pressure is 360 bara and the bubble point pressure at reservoir pressure is 250 bara.

Task (10 POINTS): Propose an IPR equation to use for this well and calculate all the parameters in the equation suggested using the test data. Justify your answer.

Additional information:

Some IPRs:

Dry gas backpressure equation:

$$q_g = C_R \cdot (p_R^2 - p_{wf}^2)^n$$

Saturated oil Vogel equation

$$q_o = q_{o,max} \left[1 - 0.2 \cdot \frac{p_{wf}}{p_R} - 0.8 \cdot \left(\frac{p_{wf}}{p_R} \right)^2 \right]$$

Saturated oil Fetkovich equation

$$q_o = q_{o,max} \left[1 - \left(\frac{p_{wf}}{p_R} \right)^2 \right]$$

Undersaturated oil, OR high pressure gas equation

$$q = J \cdot (p_R - p_{wf})$$

SOLUTION

See the Excel file attached.