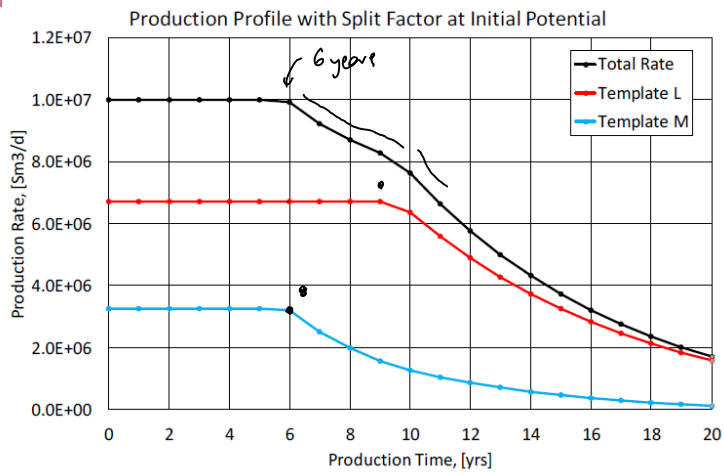
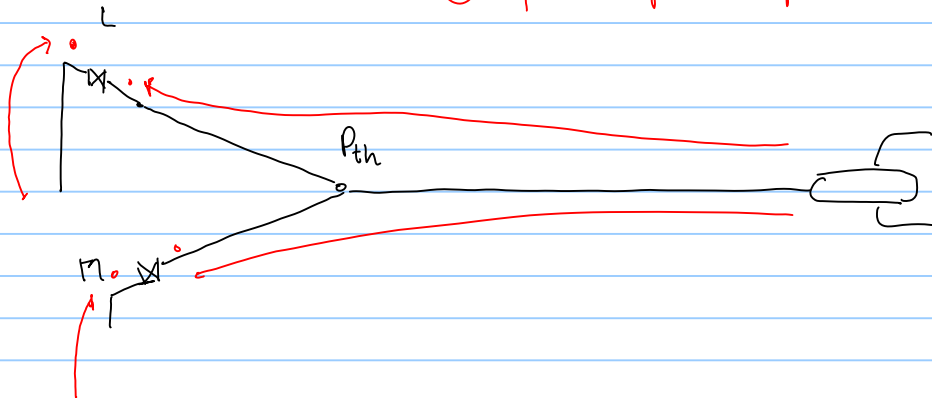


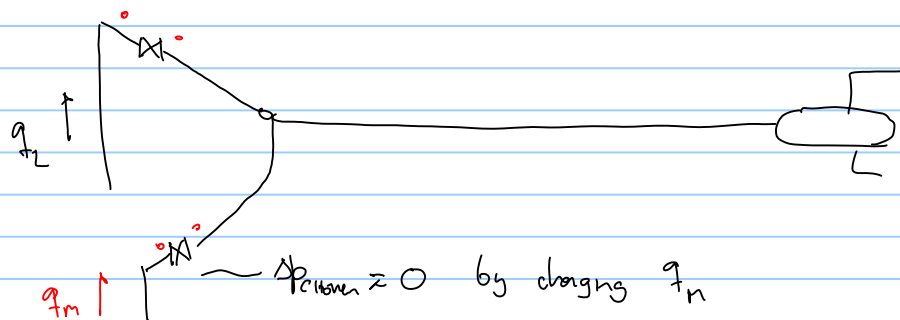
- Review of problem 1, ex. set 3
- class exercise (exam problem)



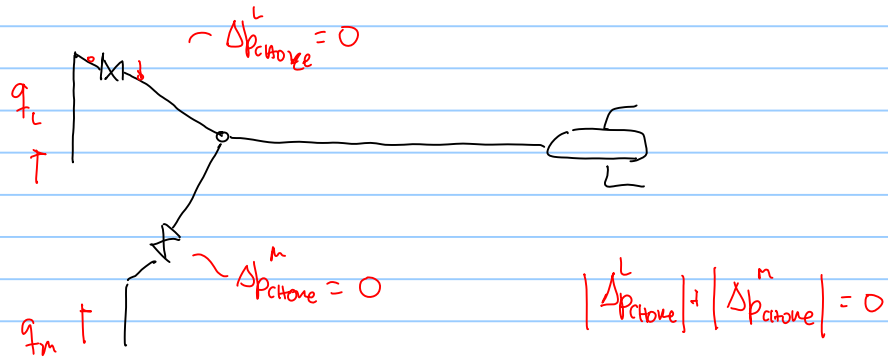
① equilibrium point in plateau



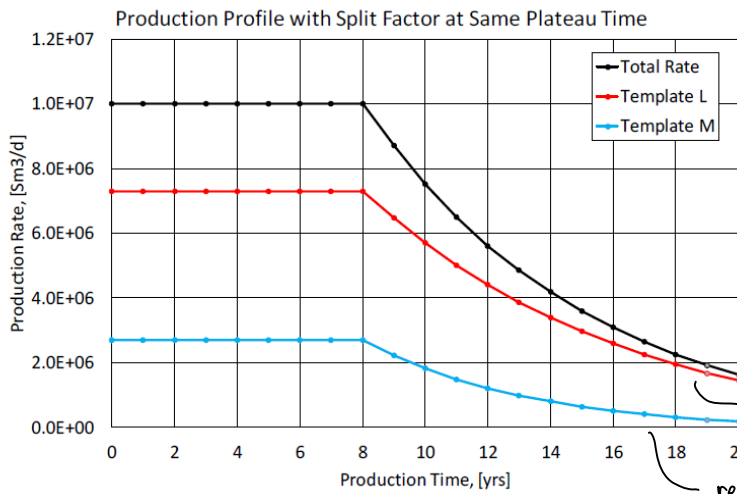
② template M enters in decline $\Delta p_{chore} \leq 0$



③ template L alters in decline



Changing the production splitting can change significantly the plateau duration.

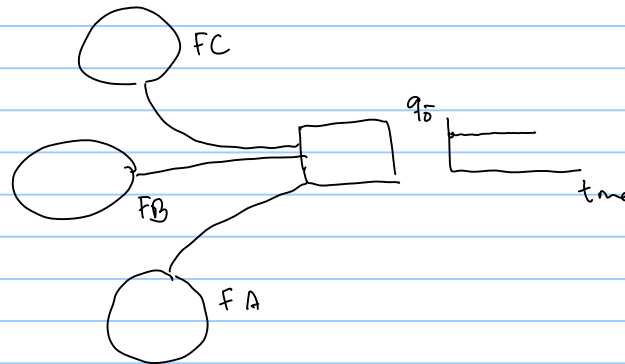


0.73 template L

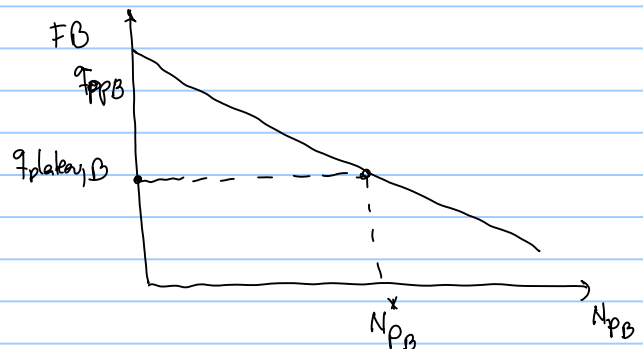
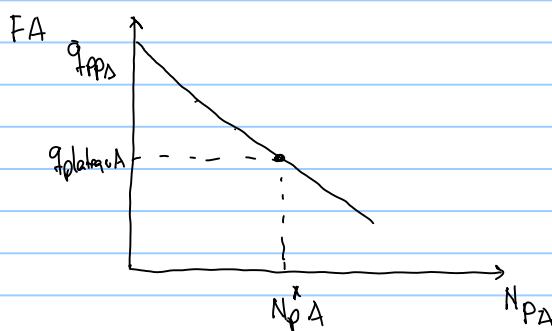
0.27 template M

reservoir B-14

for multi-reservoir systems



when 2 reservoirs



given $q_{f,plateau}$

chose $q_{\text{plateau},A}$, read Np_A^*

$$t_{\text{end,plateau}}^A = \frac{Np_A^*}{q_{\text{plateau},A} \cdot \text{Nday/year}}$$

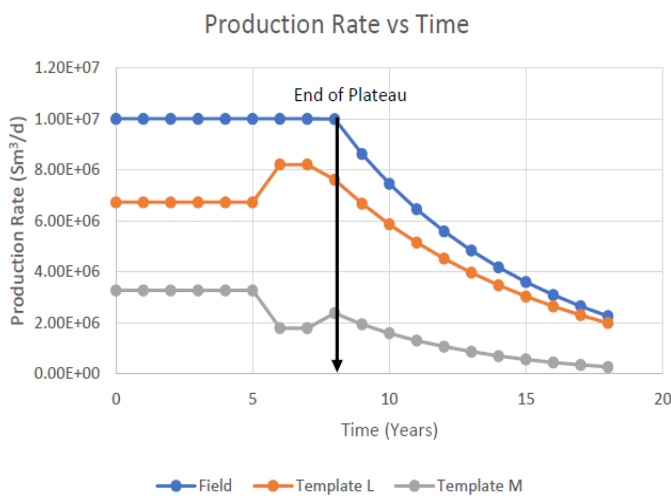
$$q_{\text{plateau},B} = q_{\text{field,plateau}} - q_{\text{plateau},A}$$

to maximize plateau duration

$$t_{\text{end,plateau}}^A = t_{\text{end,plateau}}^B$$

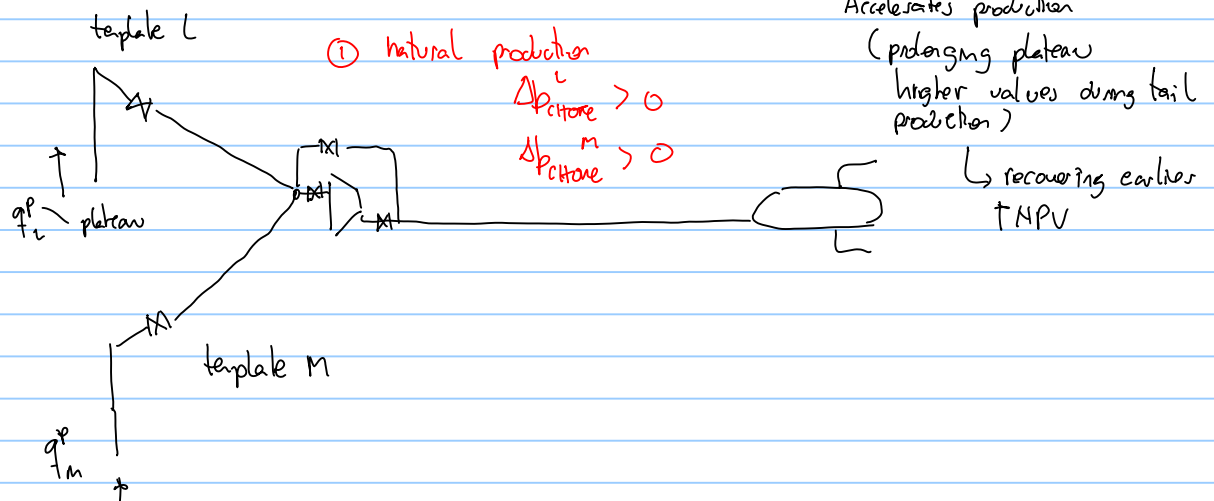
$$t_{\text{end,plateau}}^B = \frac{Np_B^*}{q_{\text{plateau},B} \cdot \text{Nday/year}}$$

Note: be careful with constraints! $\rightarrow$ maximum allowable production per well
API blending
 CO_2 , H_2S content
etc.

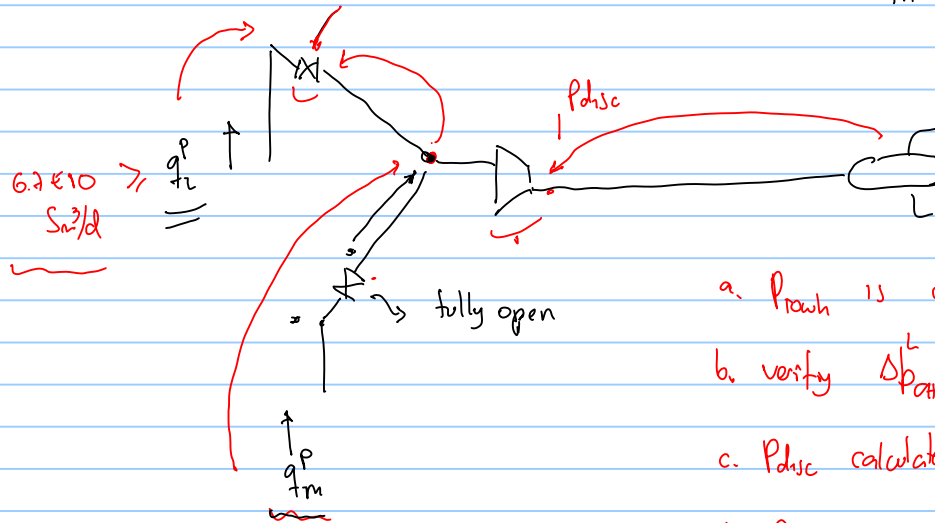


It is also possible to change production splitting mid-way

• Task 2. simplified compressor



② template M enters in decline, but we still want to produce it in plateau mode!



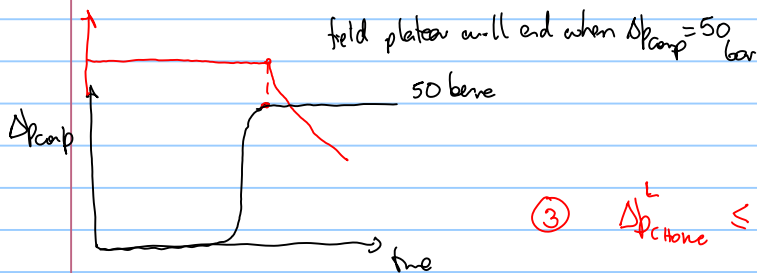
a. P_{flow} is calculated co-current from M

b. verify $\Delta p_{plateau}^L > 0$

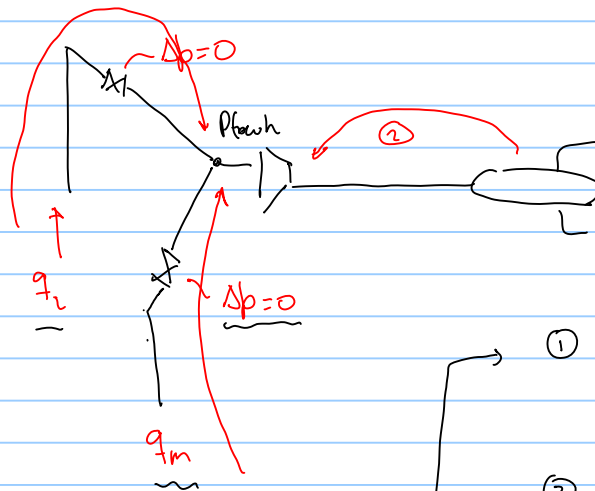
c. P_{disch} calculated from P_{pump}

d. $P_{disch} - P_{flow} > 0$

$P_{dis} - P_{flow} \leq 50 \text{ bar}$



③ $\Delta p_{plateau}^L \leq 0$ - fully open chance with $\Delta p_{comp} = 50 \text{ bar}$



① assume $q_r < q_p$
 $q_m < q_p$

② calculate P_{disch} (counter-current from rrp)

③ max q_{field} is obtained when Δp_{comp} is maximum, therefore:

$$P_{flow} = -50 + P_{disch}$$

④ move co-current to pflow from L and M and check if

$$P_{flow} = P_{flow}^n = P_{flow}^L ?$$

not

↓ see solution

alternative:

④) now counter current from P_{towh} to P_{lemp}^m
and $P_{tow} \rightarrow P_{lemp}^L$

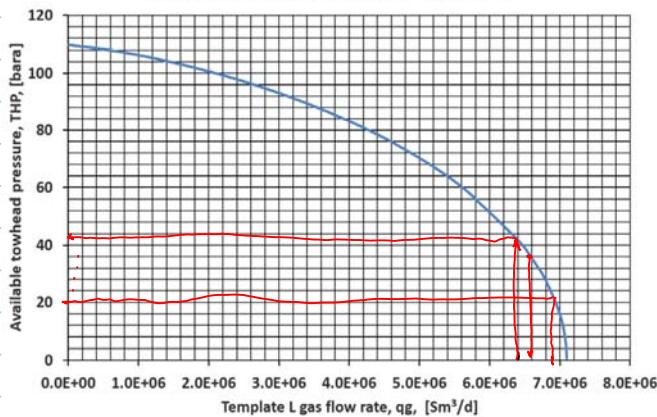
now co-current from m to P_{wh}^m

now co-current from L to P_{wh}^L

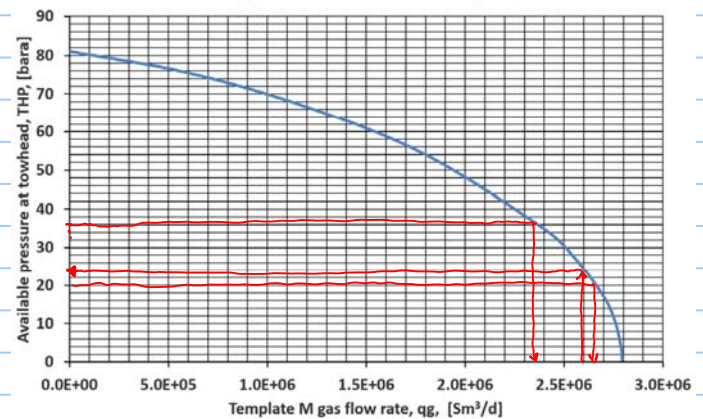
change q_L and q_m such that $\begin{cases} \Delta p^m = 0 \\ \Delta p^L = 0 \end{cases}$

Class exercise:

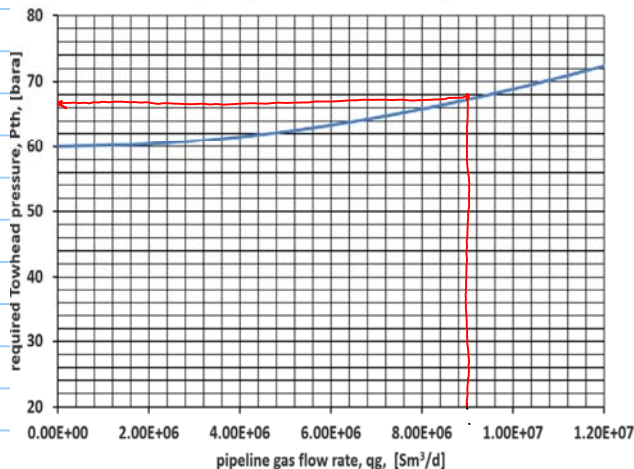
Available pressure at towhead - template L



Available pressure at towhead - Template M



Pipeline performance relationship



$$q_m + q_L = 9.00 \text{ E}06 \text{ Sm}^3/\text{d}$$

① $P_{disc} = 67 \text{ bara}$

② assume $P_j = 20 \text{ bara}$

$$q_L = 6.9 \text{ E}06 \text{ Sm}^3/\text{d}$$

$$q_m = 2.65 \text{ E}06 \text{ Sm}^3/\text{d}$$

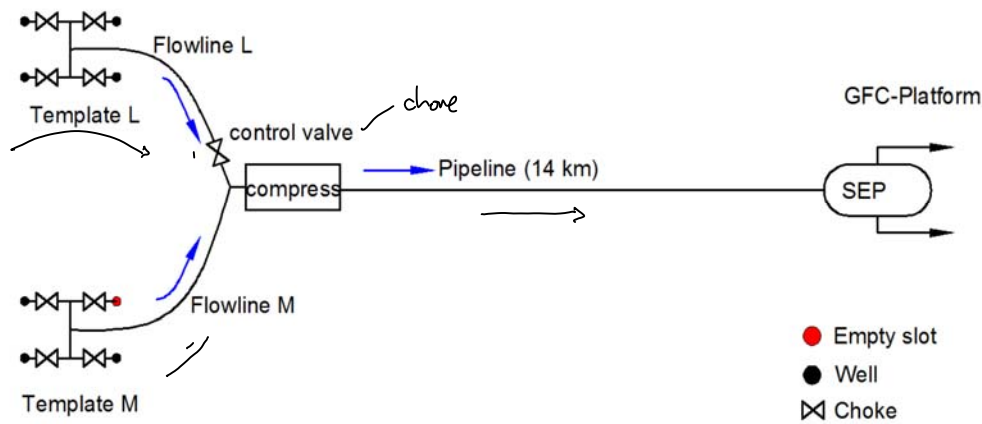
$$q_f = 9.5 \text{ E}06 \text{ Sm}^3/\text{d}$$

assume $P_j = 36 \text{ bara}$

$$q_m = 2.35 \text{ E}06 \text{ Sm}^3/\text{d}$$

$$q_L = 6.6 \text{ E}06 \text{ Sm}^3/\text{d}$$

it is possible $\Delta p_{comp} = 67 - 36 = 31 \text{ bar}$



task 2. $P_{ch} = 67 \text{ bara}$ $f(q_{held})$

$$q_{held} = 9.6 \text{ Sm}^3/\text{d}$$

$$q_L = 6.4 \text{ Sm}^3/\text{d}$$

$$P_{\text{upstream control valve}} = 41 \text{ bara}$$

$$P_{wh}^L$$

$$q_M = 7.6 \text{ Sm}^3/\text{d}$$

$$P_{wh}^M = P_{puct} = 24 \text{ bara}$$

$$\Delta P_{choke}^L > 0 \quad 41 - 24 = 17 \text{ bar}$$

$$\Delta P_{pump} > 0 \quad 67 - 24 = 43 \text{ bar}$$