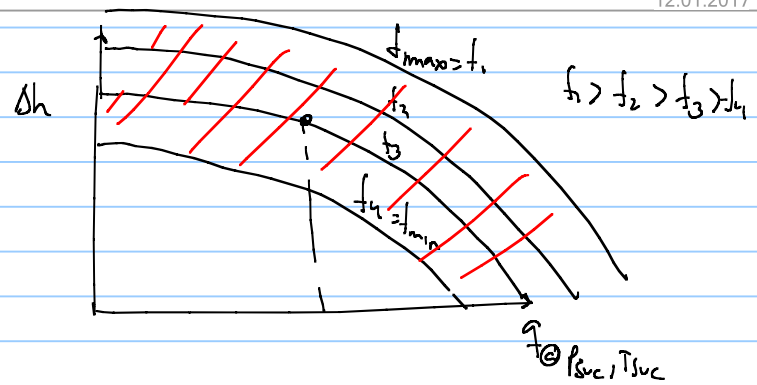


20180320 lead $\Delta h = \frac{\Delta p}{\rho \cdot g}$

pure oil $\rho_o = 790 \text{ kg/m}^3$
 $\Delta p = \Delta h \cdot 790 \text{ kg/m}^3$

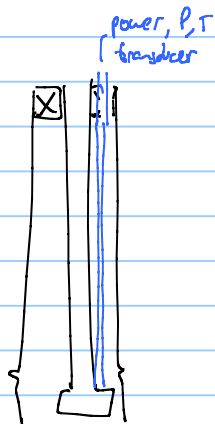
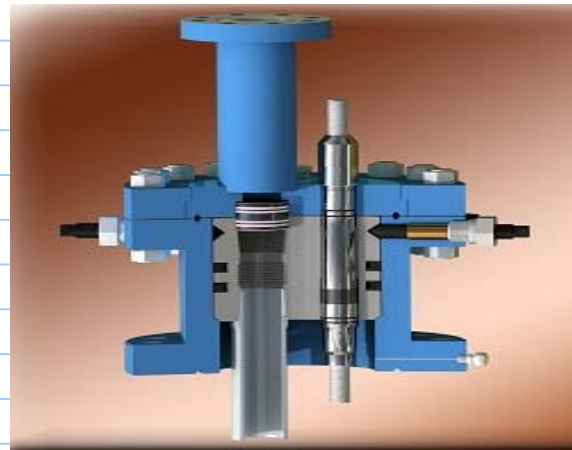
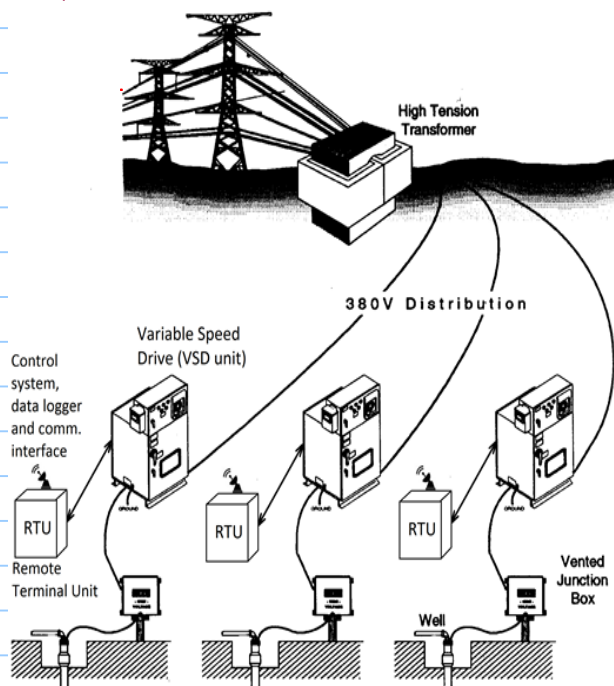
pure water $\rho_w = 1024 \text{ kg/m}^3$

$\Delta p_{\text{water}} = \Delta h \cdot 1024 \text{ kg/m}^3$



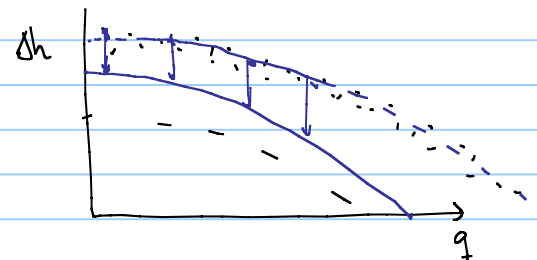
to control performance EJP one can change the rotational speed of pump (impeller) frequency h_z

30 - 70



$$\Delta h = a \cdot q^4 + b \cdot q^3 + c \cdot q^2 + d \cdot q + e$$

manufacturers usually measure for a ref fluid (water) at reference frequency (60 Hz)



$$\frac{\Delta h_1}{\Delta h_{ref}} = \left(\frac{f_1}{f_{ref}} \right)^2$$

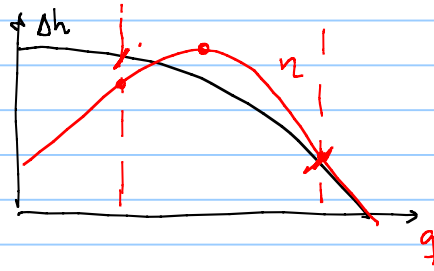
$$\frac{q_1}{q_{ref}} = \frac{f_1}{f_{ref}}$$

$$q_{ref} = q \cdot \left(\frac{f_{ref}}{f_1} \right)$$

$$\Delta h_{\text{of}} = \left(a \cdot q^4 + b \cdot q^3 + c \cdot q^2 + d \cdot q + e \right) \left(\frac{f}{f_{ref}} \right)^2$$

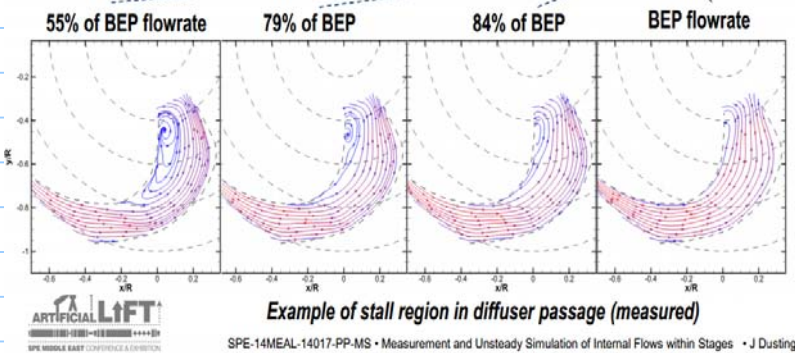
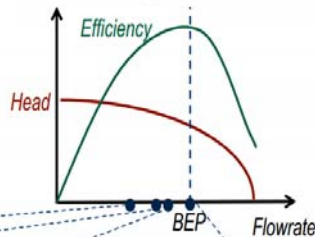
$$\Delta h_{\text{of}} = a \left[q_1 \cdot \left(\frac{f_{ref}}{f_1} \right) \right]^4 + b \left[q_1 \cdot \frac{f_{ref}}{f_1} \right]^3 + c \left[q_1 \cdot \frac{f_{ref}}{f_1} \right]^2 + d \left[q_1 \cdot \frac{f_{ref}}{f_1} \right] + e$$

other operational constraints :

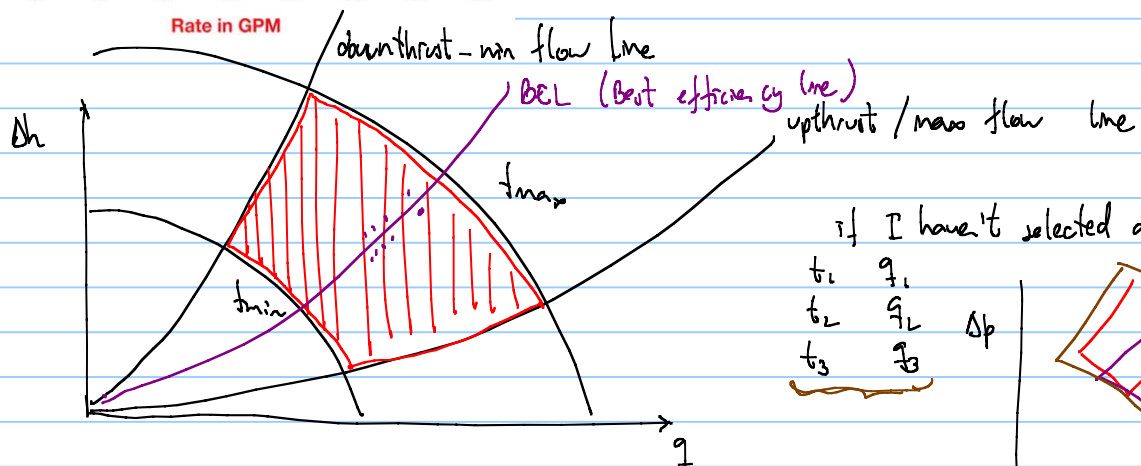
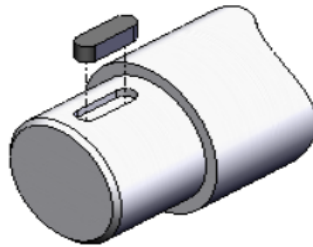
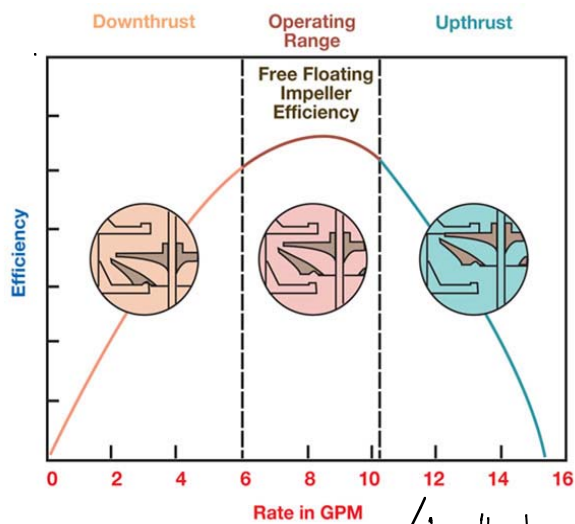


PIV measurement in a radial flow stage

- Flow features in diffuser and impeller may be identified from measurements
- Flow misalignment and recirculations reduce efficiency



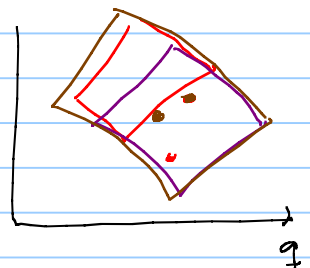
upthrust and downthrust

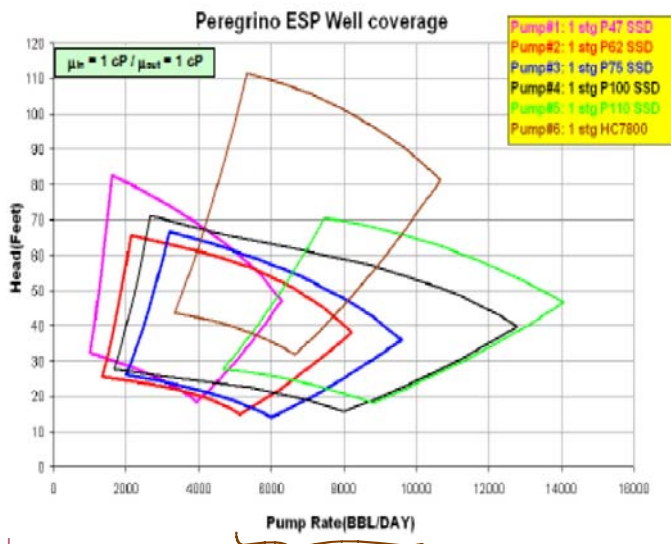


if I haven't selected an tDP get

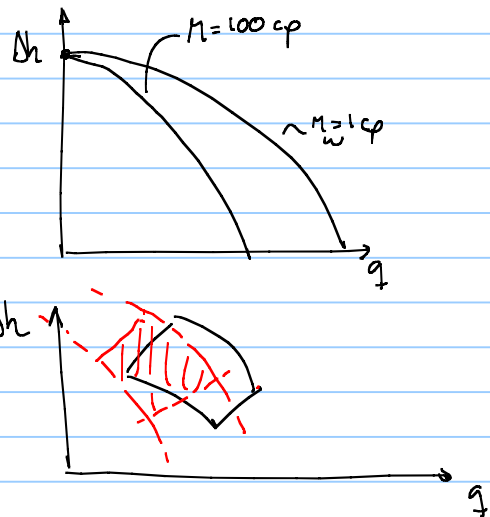
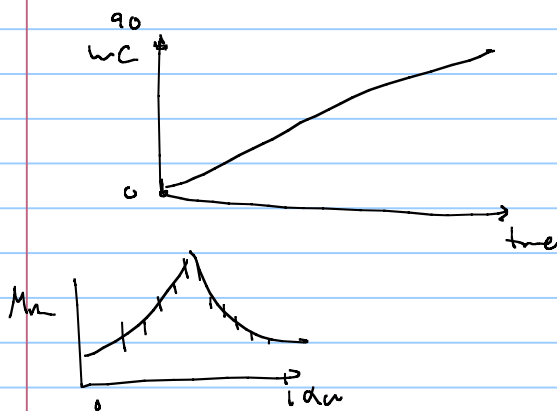
t_1	q_1
t_2	q_2
t_3	q_3

Δp





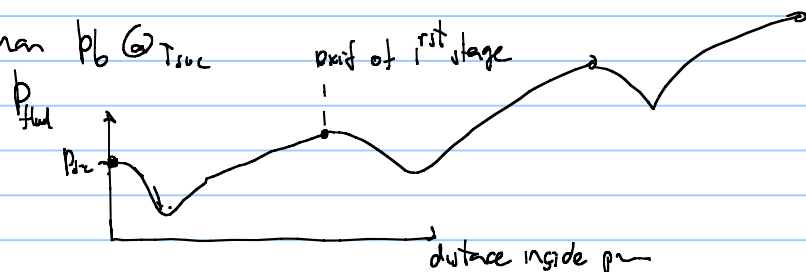
the performance of ESP is reduced by increased viscosity!



to estimate performance for a different viscosity

→ measurements
→ American national standard (Hydraulic Institute)
ANSI/HI 9.6.7 - 2015

- Power has to be greater than $P_b @ T_{suc}$

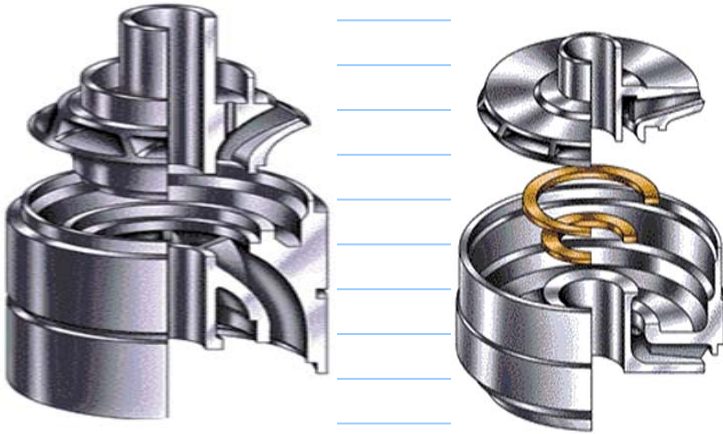


$$P_{ave} > F \cdot P_b @ T_{suc}$$

Leakage factor

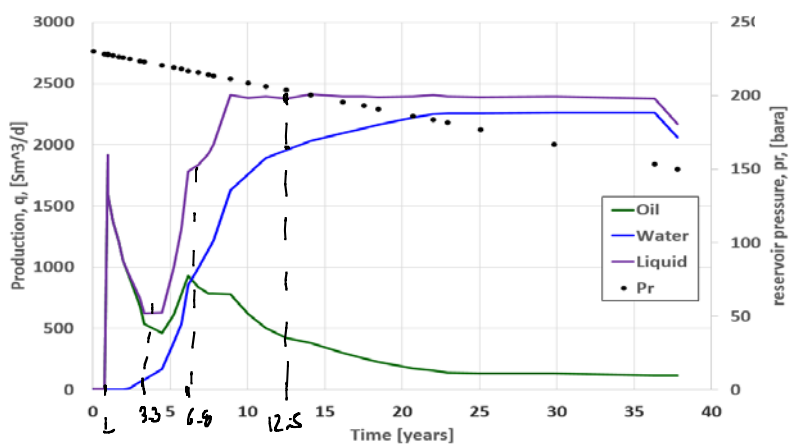
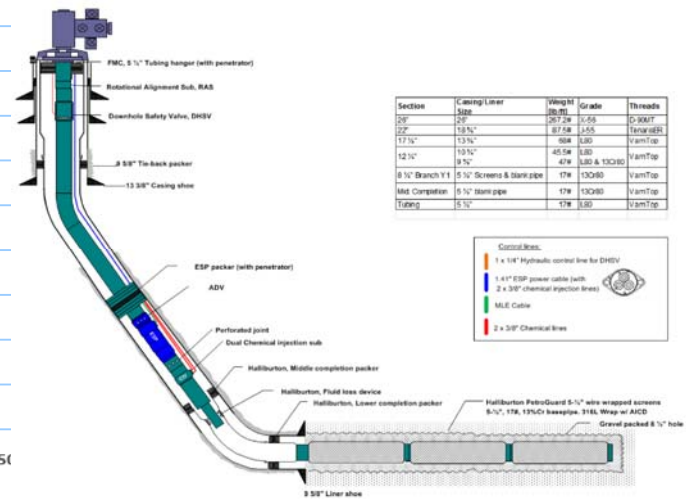
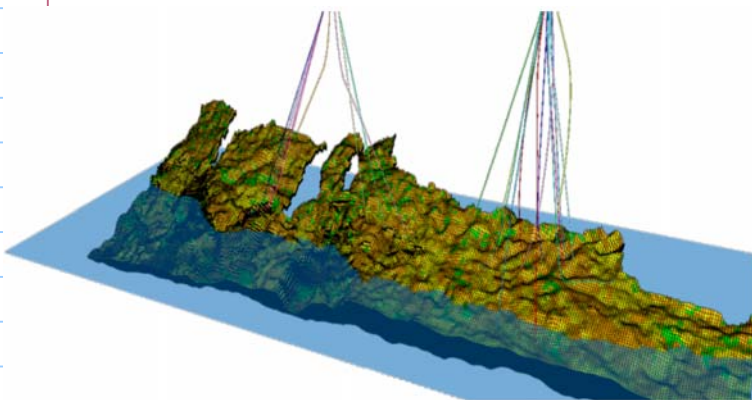
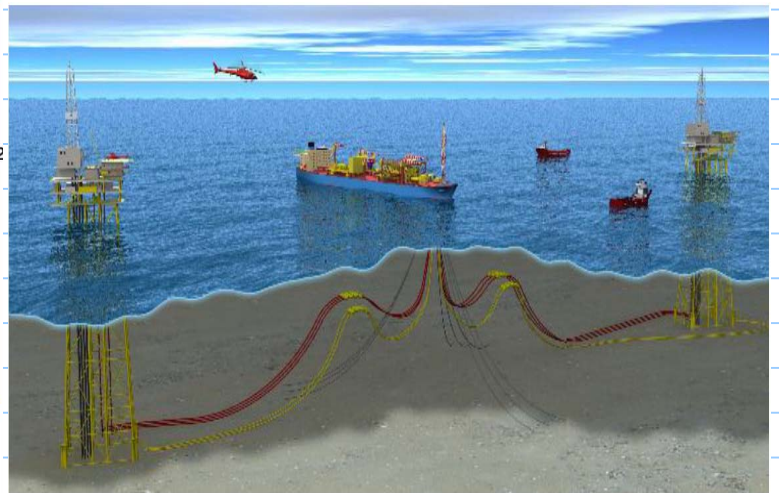
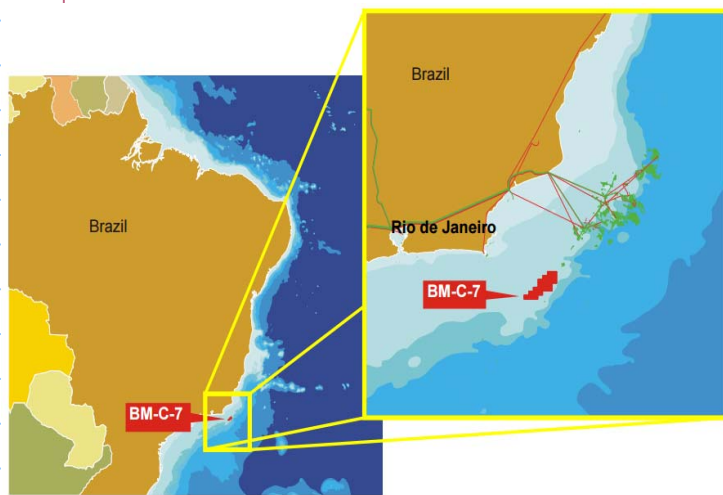
- $P_{ower} \leq P_{ower \text{ capacity motor}}$

$$P_{ower \text{ pump}} = \frac{\Delta p \cdot q}{\eta_m \eta_h}$$



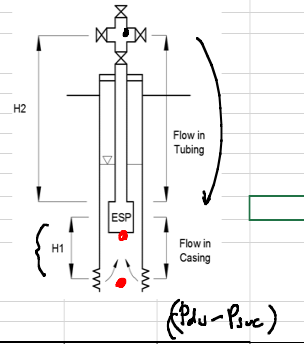
Class exercise:

http://folk.ntnu.no/stanko/Courses/TPG4230/2018/Class_files/20180320/



2018.03.20, TPG4230, Class Exercise, M. Stanko

Wells	P _R	J, for total liquid flow	h ₁	h ₂	d ₁	d ₂	Pumpname	Stages
-	bara	Sm ³ /d/bar	m	m	m	m	-	-
1	231	14	380	1960	0.24	0.14	Centrilift 675	78
Fluid Density	Water 1025	Oil 897 [kg/m ³]						
Richardson Emul. exp.	13	3.215						
Viscosity	1.00E-03	0.1 [Pa s]						
α _w cut off	0.60							
Roughness tubing and lines	0.00010 m							
Bubble point pressure [bara]	30 [bara]							
							Required pressure at pump intake	36



Date	P _R	WC	Average density	Effective viscosity	q _{tot}	P _{wf}	q _o	q _w	P _{suc}	P _{disc}	ΔP _{ESP}	Δh _{ESP}	P _{wh}	Pump power	Hydraulic Eff	frequency
[years]	bara	[-]	kg/m ³	Pa s	Sm ³ /d	bara	Sm ³ /d	Sm ³ /d	bara	bara	bara	m	bara	[hp]	[%]	Hz
1.0	230	0.00			1912								7			
3.3	223	0.13			621								7			
6.8	216	0.54			1833								7			
12.5	204	0.82			2379								7			

$$I_{PR} \quad \checkmark \quad \checkmark$$

$$q_c = J_L (P_R - P_{wf})$$

Function Pout(qt, ID, den, visc, Length, teta, pin, roughness)

$$\text{assume } B_o \approx 1$$

$$B_w \approx 1$$

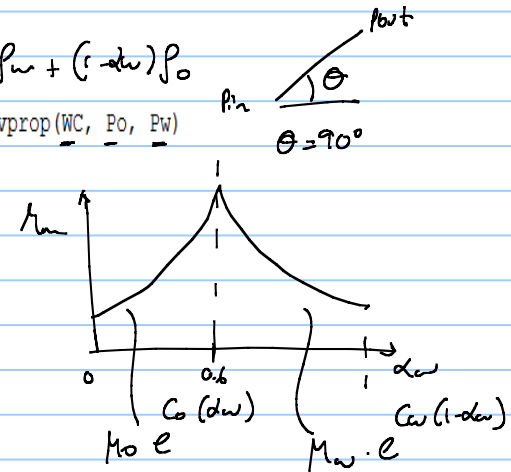
$$q_o = q_o @ P_{wf}$$

$$q_w = q_w @ P_{wf}$$

$$WC = \frac{q_w}{q_o + q_w} = \alpha_w = \frac{q_w}{q_o + q_w}$$

$$P_{in} = P_{wf} + \Delta P$$

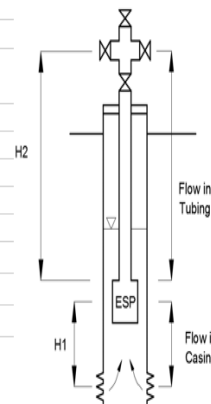
$$P_m = \alpha_w P_w + (1 - \alpha_w) P_o$$

Function Avprop(WC, P_o, P_w)Rich emul_visc(mu_o, mu_w, alpha_w, expo, expw, alpha_w_cutoff)

final operating points after adjustments

2018.03.20, TPG4230, Class Exercise, M. Stanko

Wells	P _R	J, for total liquid flow	h ₁	h ₂	d ₁	d ₂	Pumpname	Stages
-	bara	Sm ³ /d/bar	m	m	m	m	-	-
1	231	14	380	1960	0.24	0.14	Centrilift 675	78
Fluid Density	Water 1025	Oil 897 [kg/m ³]						
Richardson Emul. exp.	13	3.215						
Viscosity	1.00E-03	0.1 [Pa s]						
α _w cut off	0.60							
Roughness tubing and lines	0.00010 m							
Bubble point pressure [bara]	30 [bara]							
							Required pressure at pump intake	36



Date	P _R	WC	Average density	Effective viscosity	q _{tot}	P _{wf}	q _o	q _w	P _{suc}	P _{disc}	ΔP _{ESP}	Δh _{ESP}	P _{wh}	Pump power	Hydraulic Eff
[years]	bara	[-]	kg/m ³	Pa s	Sm ³ /d	bara	Sm ³ /d	Sm ³ /d	bara	bara	bara	m	bara	[hp]	[%]
1.0	230	0.00	897	0.100	1912	93			59.9	186	127	1439	7		
3.3	223	0.13	914	0.153	621	179			144.5	184	40	442	7		
6.8	216	0.54	966	0.572	1400	116			79.5	202	123	1298	7		
12.5	204	0.82	1002	0.010	1800	75			37.7	203	166	1684	7		

for year 6.0 :

