

Monday 25.01.2016 Prof. Michael Golan

Tuesday 26.01.2016 Dr. Mahmoud Eternadhar, Sevan Marine

"Deep water field developments planning"



Summary of yesterday

Expertise using excel: VOF, VBA, solver, linear interpolation on tables

table interpolator: excel solver doesn't work properly with this function

time [years]	qfield [sm ³ /d]	Gp [sm ³]	qpptf [sm ³ /d]
0.0	2.00E+07	0	7.64E+07
0.5	2.00E+07	3.55E+09	7.53E+07
1.0	2.00E+07	7.10E+09	7.42E+07
1.5	2.00E+07	1.07E+10	7.29E+07
2.0	2.00E+07	1.42E+10	7.17E+07
2.5	2.00E+07	1.78E+10	7.04E+07
3.0	2.00E+07	2.13E+10	6.91E+07
3.5	2.00E+07	2.49E+10	6.78E+07
4.0	2.00E+07	2.84E+10	6.66E+07
4.5	2.00E+07	3.20E+10	6.54E+07
5.0	2.00E+07	3.55E+10	6.41E+07
5.5	2.00E+07	3.91E+10	6.29E+07
6.0	2.00E+07	4.26E+10	6.17E+07
6.5	2.00E+07	4.62E+10	6.05E+07
7.0	2.00E+07	4.97E+10	5.93E+07
7.5	2.00E+07	5.33E+10	5.82E+07
8.0	2.00E+07	5.68E+10	5.70E+07
8.5	2.00E+07	6.04E+10	5.58E+07
9.0	2.00E+07	6.39E+10	5.47E+07
9.5	2.00E+07	6.75E+10	5.36E+07
10.0	2.00E+07	7.10E+10	5.24E+07
10.5	2.00E+07	7.46E+10	5.13E+07
11.0	2.00E+07	7.81E+10	5.02E+07
11.5	2.00E+07	8.17E+10	4.91E+07
12.0	2.00E+07	8.52E+10	4.80E+07
12.5	2.00E+07	8.88E+10	4.69E+07
13.0	2.00E+07	9.23E+10	4.58E+07
13.5	2.00E+07	9.59E+10	4.47E+07
14.0	2.00E+07	9.94E+10	4.37E+07
14.5	2.00E+07	1.03E+11	4.26E+07
15.0	2.00E+07	1.07E+11	4.15E+07
15.5	2.00E+07	1.10E+11	4.05E+07
16.0	2.00E+07	1.14E+11	3.94E+07
16.5	2.00E+07	1.17E+11	3.84E+07
17.0	2.00E+07	1.21E+11	3.73E+07
17.5	2.00E+07	1.24E+11	3.63E+07
18.0	2.00E+07	1.28E+11	3.52E+07
18.5	2.00E+07	1.31E+11	3.42E+07
19.0	2.00E+07	1.35E+11	3.31E+07
19.5	2.00E+07	1.38E+11	3.21E+07
20.0	2.00E+07	1.42E+11	3.11E+07
20.5	2.00E+07	1.46E+11	3.00E+07
21.0	2.00E+07	1.49E+11	2.90E+07
21.5	2.00E+07	1.53E+11	2.79E+07
22.0	2.00E+07	1.56E+11	2.69E+07
22.5	2.00E+07	1.60E+11	2.59E+07
23.0	2.00E+07	1.63E+11	2.48E+07
23.5	2.00E+07	1.67E+11	2.38E+07
24.0	2.00E+07	1.70E+11	2.27E+07
24.5	2.00E+07	1.74E+11	2.17E+07
25.0	2.00E+07	1.78E+11	2.06E+07
25.25	2.00E+07	1.80E+11	2.00E+07
25.5	1.85E+07	1.85E+11	1.38778E-17
25.75	1.85E+07	1.85E+11	1.38778E-17
26.0	1.85E+07	1.85E+11	1.38778E-17
26.25	1.85E+07	1.85E+11	1.38778E-17
26.5	1.85E+07	1.85E+11	1.38778E-17
26.75	1.85E+07	1.85E+11	1.38778E-17
27.0	1.85E+07	1.85E+11	1.38778E-17
27.25	1.85E+07	1.85E+11	1.38778E-17
27.5	1.85E+07	1.85E+11	1.38778E-17
27.75	1.85E+07	1.85E+11	1.38778E-17
28.0	1.85E+07	1.85E+11	1.38778E-17
28.25	1.85E+07	1.85E+11	1.38778E-17
28.5	1.85E+07	1.85E+11	1.38778E-17
28.75	1.85E+07	1.85E+11	1.38778E-17
29.0	1.85E+07	1.85E+11	1.38778E-17
29.25	1.85E+07	1.85E+11	1.38778E-17
29.5	1.85E+07	1.85E+11	1.38778E-17
29.75	1.85E+07	1.85E+11	1.38778E-17
30.0	1.85E+07	1.85E+11	1.38778E-17
30.25	1.85E+07	1.85E+11	1.38778E-17
30.5	1.85E+07	1.85E+11	1.38778E-17
30.75	1.85E+07	1.85E+11	1.38778E-17
31.0	1.85E+07	1.85E+11	1.38778E-17
31.25	1.85E+07	1.85E+11	1.38778E-17
31.5	1.85E+07	1.85E+11	1.38778E-17
31.75	1.85E+07	1.85E+11	1.38778E-17
32.0	1.85E+07	1.85E+11	1.38778E-17
32.25	1.85E+07	1.85E+11	1.38778E-17
32.5	1.85E+07	1.85E+11	1.38778E-17
32.75	1.85E+07	1.85E+11	1.38778E-17
33.0	1.85E+07	1.85E+11	1.38778E-17
33.25	1.85E+07	1.85E+11	1.38778E-17
33.5	1.85E+07	1.85E+11	1.38778E-17
33.75	1.85E+07	1.85E+11	1.38778E-17
34.0	1.85E+07	1.85E+11	1.38778E-17
34.25	1.85E+07	1.85E+11	1.38778E-17
34.5	1.85E+07	1.85E+11	1.38778E-17
34.75	1.85E+07	1.85E+11	1.38778E-17
35.0	1.85E+07	1.85E+11	1.38778E-17
35.25	1.85E+07	1.85E+11	1.38778E-17
35.5	1.85E+07	1.85E+11	1.38778E-17
35.75	1.85E+07	1.85E+11	1.38778E-17
36.0	1.85E+07	1.85E+11	1.38778E-17
36.25	1.85E+07	1.85E+11	1.38778E-17
36.5	1.85E+07	1.85E+11	1.38778E-17
36.75	1.85E+07	1.85E+11	1.38778E-17
37.0	1.85E+07	1.85E+11	1.38778E-17
37.25	1.85E+07	1.85E+11	1.38778E-17
37.5	1.85E+07	1.85E+11	1.38778E-17
37.75	1.85E+07	1.85E+11	1.38778E-17
38.0	1.85E+07	1.85E+11	1.38778E-17
38.25	1.85E+07	1.85E+11	1.38778E-17
38.5	1.85E+07	1.85E+11	1.38778E-17
38.75	1.85E+07	1.85E+11	1.38778E-17
39.0	1.85E+07	1.85E+11	1.38778E-17
39.25	1.85E+07	1.85E+11	1.38778E-17
39.5	1.85E+07	1.85E+11	1.38778E-17
39.75	1.85E+07	1.85E+11	1.38778E-17
40.0	1.85E+07	1.85E+11	1.38778E-17
40.25	1.85E+07	1.85E+11	1.38778E-17
40.5	1.85E+07	1.85E+11	1.38778E-17
40.75	1.85E+07	1.85E+11	1.38778E-17
41.0	1.85E+07	1.85E+11	1.38778E-17
41.25	1.85E+07	1.85E+11	1.38778E-17
41.5	1.85E+07	1.85E+11	1.38778E-17
41.75	1.85E+07	1.85E+11	1.38778E-17
42.0	1.85E+07	1.85E+11	1.38778E-17
42.25	1.85E+07	1.85E+11	1.38778E-17
42.5	1.85E+07	1.85E+11	1.38778E-17
42.75	1.85E+07	1.85E+11	1.38778E-17
43.0	1.85E+07	1.85E+11	1.38778E-17
43.25	1.85E+07	1.85E+11	1.38778E-17
43.5	1.85E+07	1.85E+11	1.38778E-17
43.75	1.85E+07	1.85E+11	1.38778E-17
44.0	1.85E+07	1.85E+11	1.38778E-17
44.25	1.85E+07	1.85E+11	1.38778E-17
44.5	1.85E+07	1.85E+11	1.38778E-17
44.75	1.85E+07	1.85E+11	1.38778E-17
45.0	1.85E+07	1.85E+11	1.38778E-17
45.25	1.85E+07	1.85E+11	1.38778E-17
45.5	1.85E+07	1.85E+11	1.38778E-17
45.75	1.85E+07	1.85E+11	1.38778E-17
46.0	1.85E+07	1.85E+11	1.38778E-17
46.25	1.85E+07	1.85E+11	1.38778E-17
46.5	1.85E+07	1.85E+11	1.38778E-17
46.75	1.85E+07	1.85E+11	1.38778E-17
47.0	1.85E+07	1.85E+11	1.38778E-17
47.25	1.85E+07	1.85E+11	1.38778E-17
47.5	1.85E+07	1.85E+11	1.38778E-17
47.75	1.85E+07	1.85E+11	1.38778E-17
48.0	1.85E+07	1.85E+11	1.38778E-17
48.25	1.85E+07	1.85E+11	1.38778E-17
48.5	1.85E+07	1.85E+11	1.38778E-17
48.75	1.85E+07	1.85E+11	1.38778E-17
49.0	1.85E+07	1.85E+11	1.38778E-17
49.25	1.85E+07	1.85E+11	1.38778E-17
49.5	1.85E+07	1.85E+11	1.38778E-17
49.75	1.85E+07	1.85E+11	1.38778E-17
50.0	1.85E+07	1.85E+11	1.38778E-17
50.25	1.85E+07	1.85E+11	1.38778E-17
50.5	1.85E+07	1.85E+11	1.38778E-17
50.75	1.85E+07	1.85E+11	1.38778E-17
51.0	1.85E+07	1.85E+11	1.38778E-17
51.25	1.85E+07	1.85E+11	1.38778E-17
51.5	1.85E+07	1.85E+11	1.38778E-17
51.75	1.85E+07	1.85E+11	1.38778E-17
52.0	1.85E+07	1.85E+11	1.38778E-17
52.25	1.85E+07	1.85E+11	1.38778E-17
52.5	1.85E+07	1.85E+11	1.38778E-17
52.75	1.85E+07	1.85E+11	1.38778E-17
53.0	1.85E+07	1.85E+11	1.38778E-17
53.25	1.85E+07	1.85E+11	1.38778E-17
53.5	1.85E+07	1.85E+11	1.38778E-17
53.75	1.85E+07	1.85E+11	1.38778E-17
54.0	1.85E+07	1.85E+11	1.38778E-17
54.25	1.85E+07	1.85E+11	1.38778E-17
54.5	1.85E+07	1.85E+11	1.38778E-17
54.75	1.85E+07	1.85E+11	1.38778E-17
55.0	1.85E+07	1.85E+11	1.38778E-17
55.25	1.85E+07	1.85E+11	1.38778E-17
55.5	1.85E+07	1.85E+11	1.38778E-17
55.75	1.85E+07	1.85E+11	1.38778E-17
56.0	1.85E+07	1.85E+11	1.38778E-17
56.25	1.85E+07	1.85E+11	1.38778E-17
56.5	1.85E+07	1.85E+11	1.38778E-17
56.75	1.85E+07	1.85E+11	1.38778E-17
57.0	1.85E+07	1.85E+11	1.38778E-17
57.25	1.85E+07	1.85E+11	1.38778E-17
57.5	1.85E+07	1.85E+11	1.38778E-17
57.75	1.85E+07	1.85E+11	1.38778E-17
58.0	1.85E+07	1.85E+11	1.38778E-17
58.25	1.85E+07	1.85E+11	1.38778E-17
58.5	1.85E+07	1.85E+11	1.38778E-17
58.75	1.85E+07	1.85E+11	1.38778E-17
59.0	1.85E+07	1.85E+11	1.38778E-17
59.25	1.85E+07	1.85E+11	1.38778E-17
59.5	1.85E+07	1.85E+11	1.38778E-17
59.75	1.85E+07	1.85E+11	1.38778E-17
60.0	1.85E+07	1.85E+11	1.38778E-17
60.25	1.85E+07	1.85E+11	1.38778E-17
60.5	1.85E+07	1.85E+11	1.38778E-17
60.75	1.85E+07	1.85E+11	1.38778E-17
61.0	1.85E+07	1.85E+11	1.38778E-17
61.25	1.85E+07	1.85E+11	1.38778E-17
61.5	1.85E+07	1.85E+11	1.38778E-17
61.75	1.85E+07	1.85E+11	1.38778E-17
62.0	1.85E+07	1.85E+11	1.38778E-17
62.25	1.85E+07	1.85E+11	1.38778E-17
62.5	1.85E+07	1.85E+11	1.38778E-17
62.75	1.85E+07	1.85E+11	1.38778E-17
63.0	1.85E+07	1.85E+11	1.38778E-17
63.25	1.85E+07	1.85E+11	1.38778E-17
63.5	1.85E+07	1.85E+11	1.38778E-17
63.75	1.85E+07	1.85E+11	1.38778E-17
64.0	1.85E+07	1.85E+11	1.38778E-17
64.25	1.85E+07	1.85E+11	1.38778E-17
64.5	1.85E+07	1.85E+11	1.38778E-17
64.75	1.85E+07	1.85E+11	1.38778E-17
65.0	1.85E+07	1.85E+11	1.38778E-17
65.25	1.85E+07	1.85E+11	1.38778E-17
65.5	1.85E+07	1.85E+11	1.387

- Calculation of the production profile: sequential

- choose a timestep

- • decide how I want to produce $\left\{ \begin{array}{l} \text{mode a} \\ \text{mode b} \end{array} \right.$

- for current $G_p^i \rightarrow q_{pp}$ $\left\{ \begin{array}{l} \text{if mode a } q_{pp} > q_{pla} \\ \text{if mode b } q_f = q_{pp} \end{array} \right.$

linear interpolation

- rectangle method: constant production G_p^{i+1}

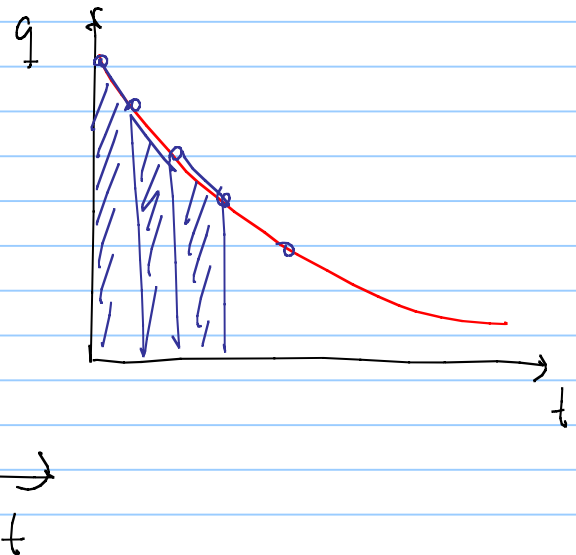
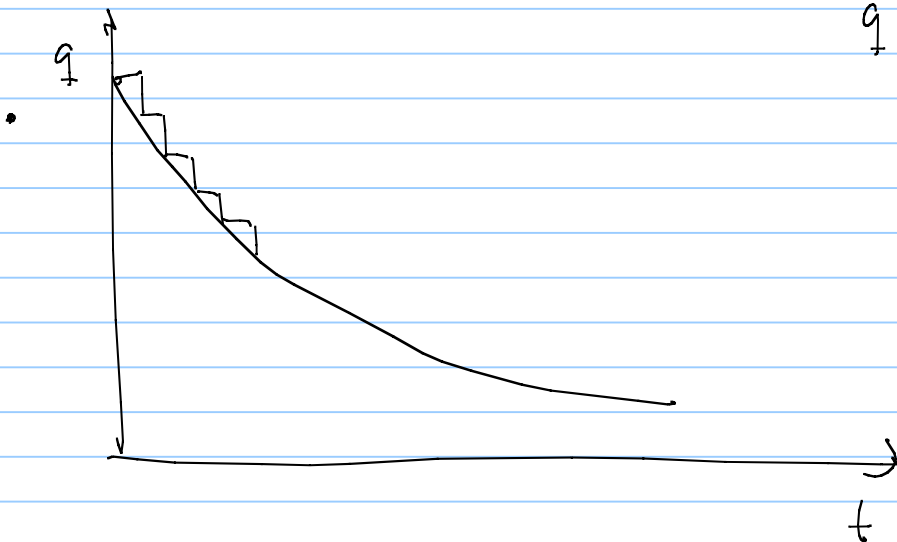
- Two examples: open choice, plateau mode.

//

- Calculation of production profile

- Exercise 1- clarification

- Architecture of the production system



Producing with open choke, calculate q vs. t using sequential calculations and trapezoidal integration

• Name of variable, symbol, units

Red: input (user given input)

Blue: result of a calculation

Violet: constant

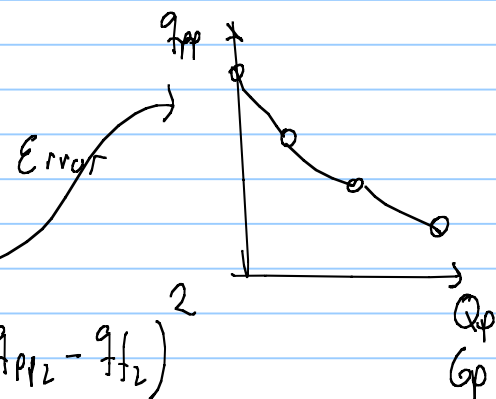
• plots: font size big enough 16-18, Bold
thickness of line

excel etiquette

Using the trapezoidal method to calculate cumulative production

time [y]	$q_f [m^3/d]$	$G_p [m^3]$	$q_{fp} [m^3/d]$
t_1 0	q_{fp1}	0	q_{fp1}
t_2 0.5	$q_{fp2} = 0.9$	$\frac{(q_{f1} + q_{f2})(t_2 - t_1)}{2} \cdot \frac{Ndc}{year}$	q_{fp2}
1			
1.5			
2			
2.5			
1			
1			
1			

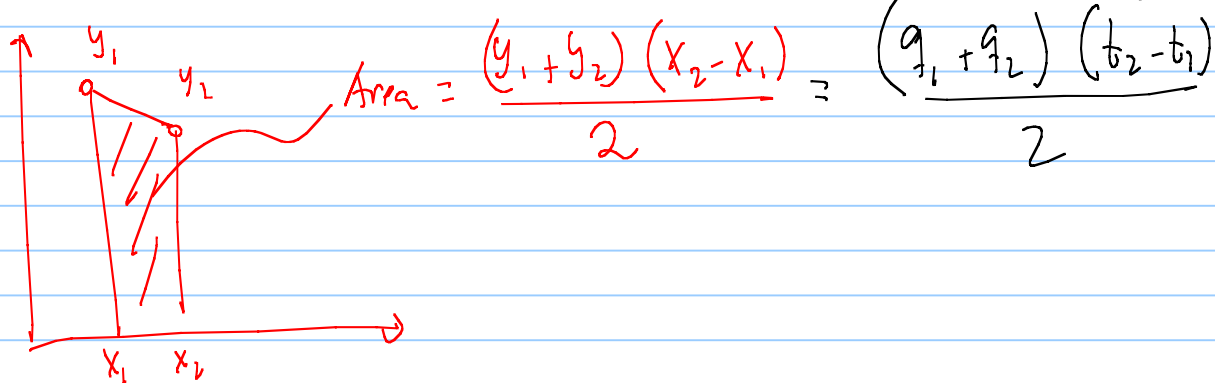
open choke rate

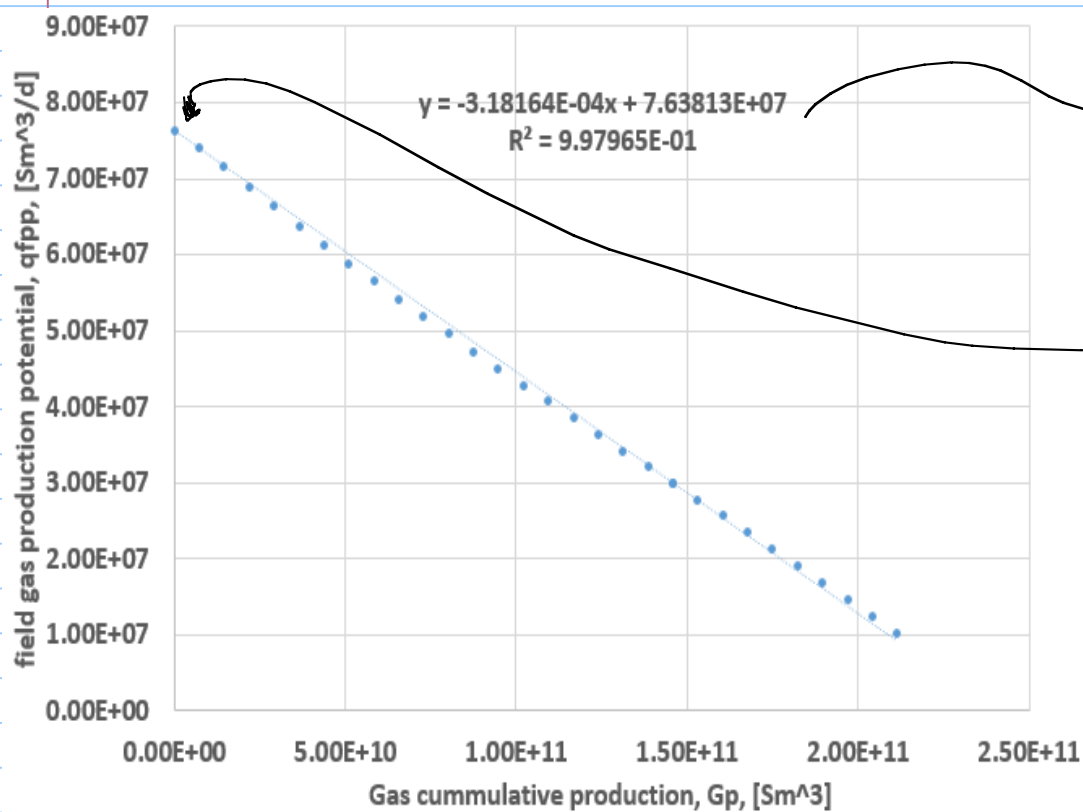


$$(q_{fp2} - q_{f2})^2$$

Assume $q_{f2} = q_{fp1} = 0.9$

$$m^3/d \left(\frac{365d}{1year} \right) \text{ years}$$



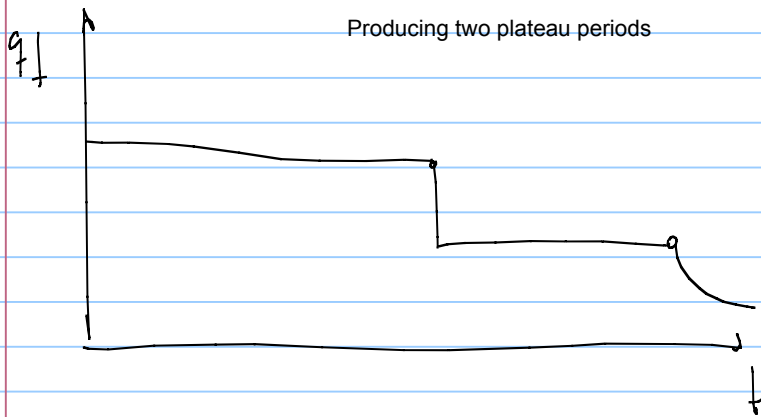


$$q_{fpp} = -m \cdot G_p + q_{fpp0}$$

```
Sub test()
  For i = 8 To 69
    SolverReset
    OBJSTRING = "$J$" & (i)
    VARSTRING = "$H$" & (i)
    SolverOk SetCell:=Range(OBJSTRING), MaxMinVal:=3, valueof:="1e-10", ByChange:=VARSTRING
    SolverSolve UserFinish:=True
  Next
  'Reading Results
End Sub
```

Handwritten annotations: "value of" points to the "valueof" parameter in the SolverOk line. "set of instructions" points to the entire Sub procedure. "Reading Results" is highlighted in green.

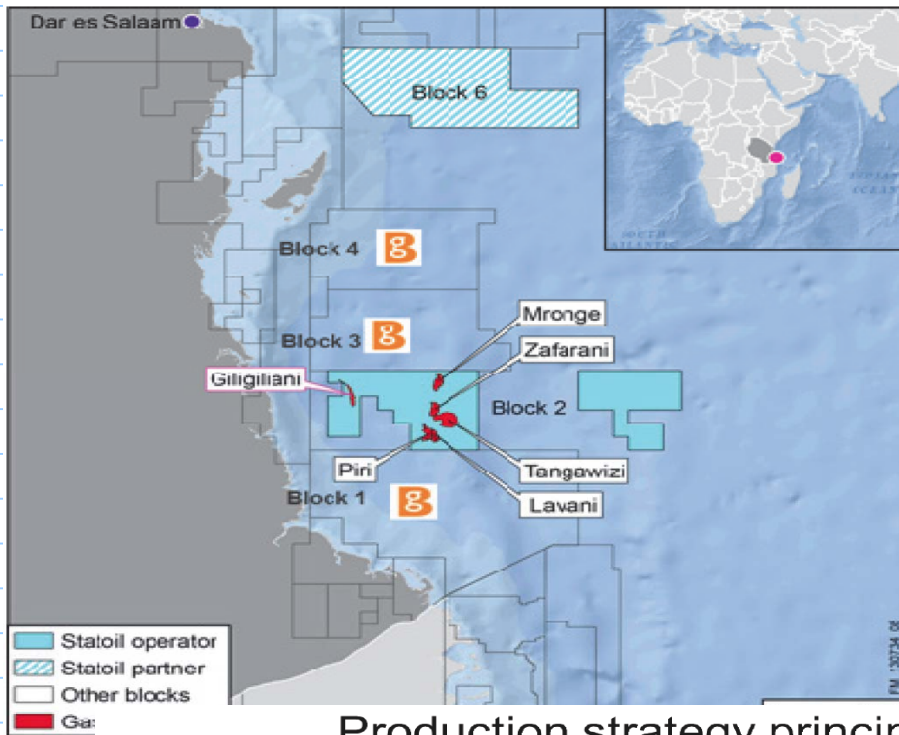
time	qf	Gp	qfpp	error
[year]	[Sm ³ /d]	[Sm ³]	[Sm ³ /d]	
0.0	7.64E+07	0	7.64E+07	
0.5	7.22E+07	1.32E+10	7.22E+07	0
1.0	6.82E+07	2.56E+10	6.82E+07	0
1.5	6.45E+07	3.74E+10	6.45E+07	0
2.0	6.09E+07	4.86E+10	6.09E+07	0
2.5	5.76E+07	5.91E+10	5.76E+07	0
3.0	5.44E+07	6.90E+10	5.44E+07	5.55112E-17
3.5	5.14E+07	7.84E+10	5.14E+07	0
4.0	4.86E+07	8.73E+10	4.86E+07	0
4.5	4.59E+07	9.57E+10	4.59E+07	5.55112E-17
5.0	4.34E+07	1.04E+11	4.34E+07	0
5.5	4.10E+07	1.11E+11	4.10E+07	0
6.0	3.88E+07	1.18E+11	3.88E+07	5.55112E-17
6.5	3.66E+07	1.25E+11	3.66E+07	0



Tanzania gas development – flow assurance challenges

H Holm

Statoil ASA, Norway



Production strategy principles

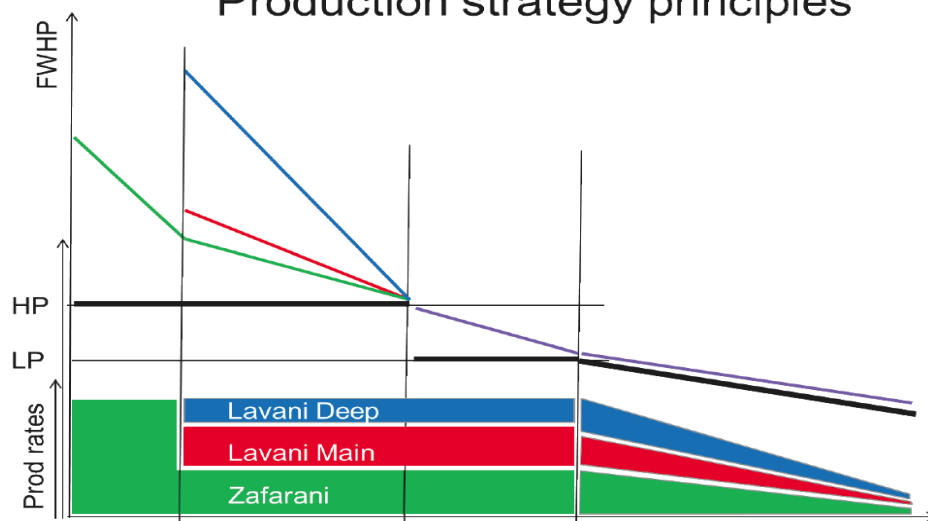
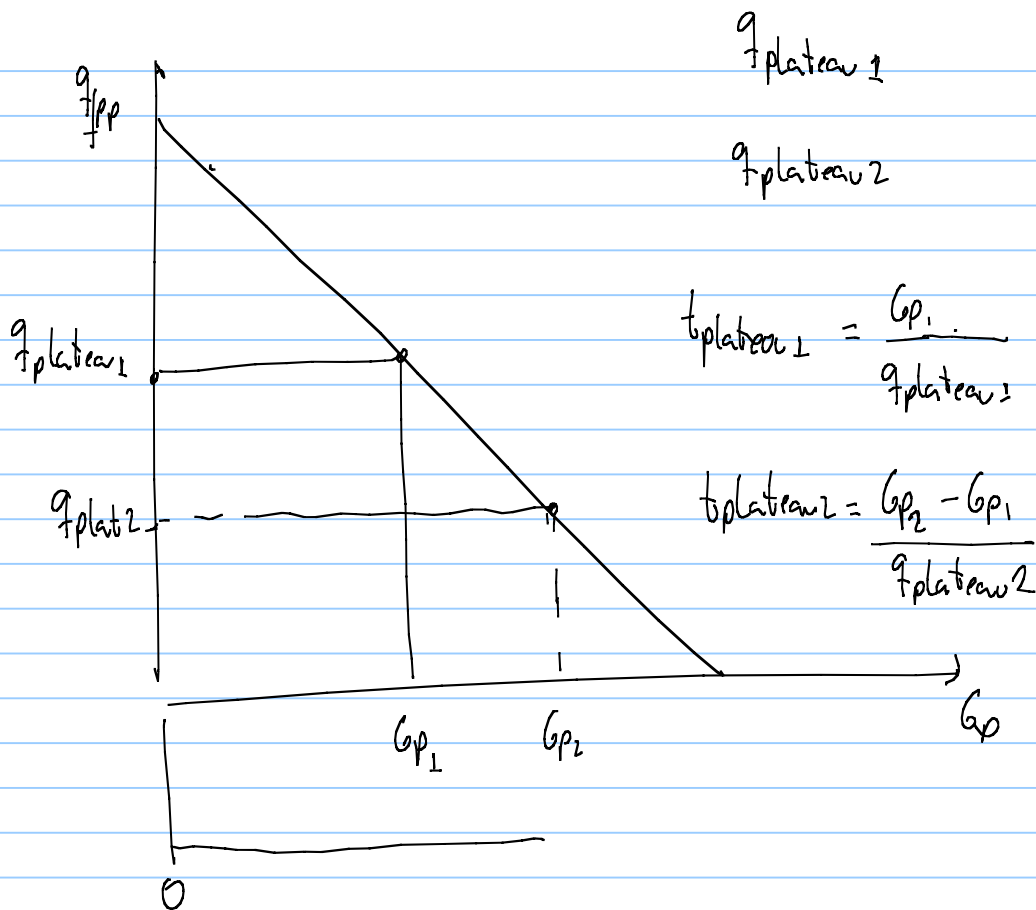


Figure 9 Production strategy inhomogeneous reservoirs



Calculating production profile analytically

$$Q_p(t) = \int_0^t q \, dt$$

producing all the time at open choke.
 $q = q_{pp}$

$$Q_p(t) = \int_0^t q_{pp} \, dt$$

$$\frac{q_{ppo} - q_{pp}}{m} = \int_0^t q_{pp} \, dt$$

$$q_{ppo} - q_{pp} = \int_0^t m q_{pp} \, dt \quad \frac{d}{dt}$$

$$-\frac{d q_{pp}}{dt} = m q_{pp}$$

$$q_{pp} = -m G_p + q_{ppo}$$

production potential at initial conditions

$$G_p = \frac{-q_{pp} + q_{ppo}}{m}$$

Snowdrift example

It might actually look different for other cases

$$\int_{q_{ppo}}^{q_{pp}(t)} \frac{dq_{pp}}{q_{pp}} = \int_0^t -m dt$$

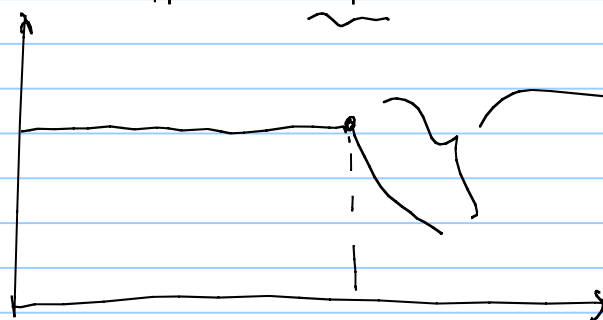
$$\ln \left(\frac{q_{pp}(t)}{q_{ppo}} \right) = -m(t-0)$$

$$\ln \left(\frac{q_{pp}(t)}{q_{ppo}} \right) = -m(t-0)$$

$$-m(t-0)$$

$$G_p = 0$$

$$q_{pp}(t) = q_{ppo} \cdot e$$



for this period, we $q_{pp}(t) = q_{ppo} e^{-m(t-t^*)}$

with * values at plateau end.

G_p @ end of the plateau

Decline curve analysis ~

$$q(t) = q_i / e^{\left\{ D_i \left[1 - \left(p_{wf} / \bar{p}_R \right) \right] \right\} t}$$

TABLE 1—SUMMARY OF PRODUCTION DECLINE EQUATIONS

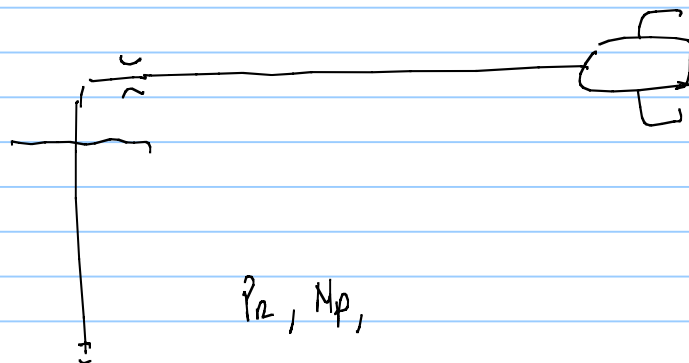
Decline Type	Hyperbolic	Exponential	Harmonic
Rate-Time	$q(t) = q_i / (1 + b D_i t)^{1/b}$	$q(t) = q_i / e^{D_i t}$	$q(t) = q_i / (1 + D_i t)$

DECLINE CURVE ANALYSIS USING TYPE CURVES

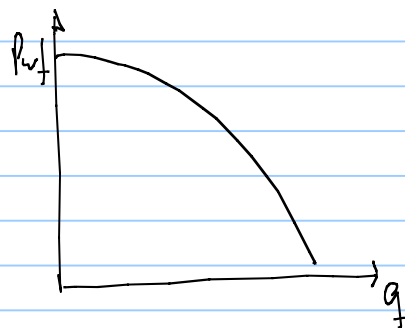
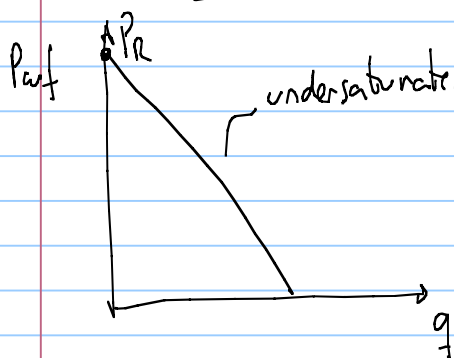
by

M. J. Fetkovich
SPE, Phillips Petroleum Co.

How do we calculate the production potential

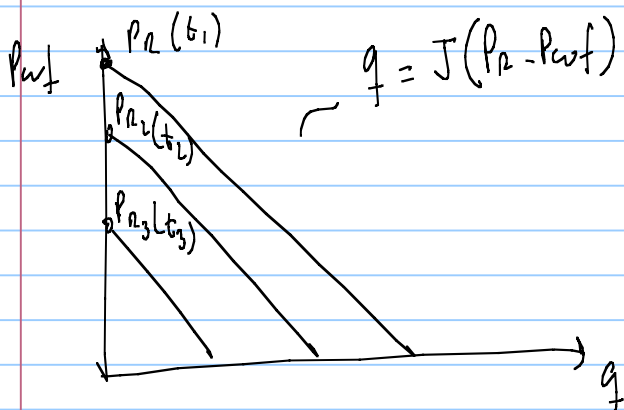


→ hydraulic equilibrium in the production system with open choke. calculate the rate.

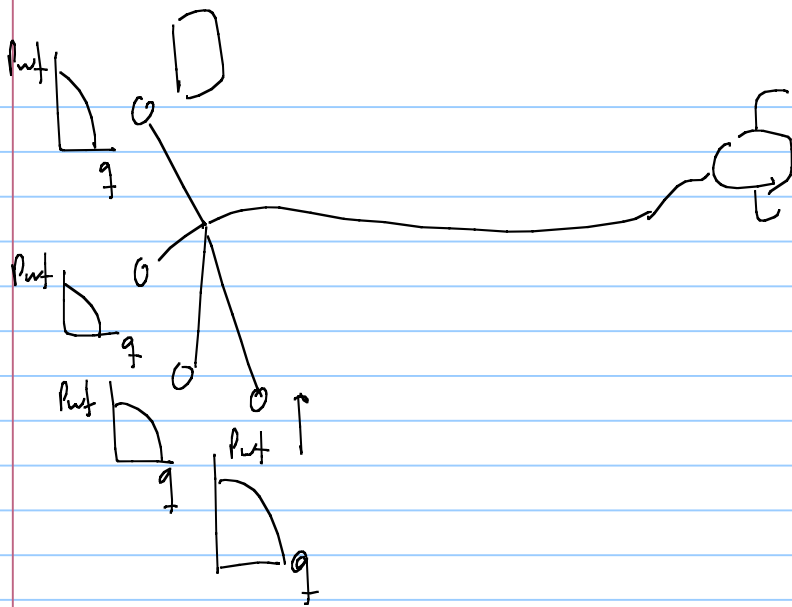


production simulators
- Pipesim
- GAP

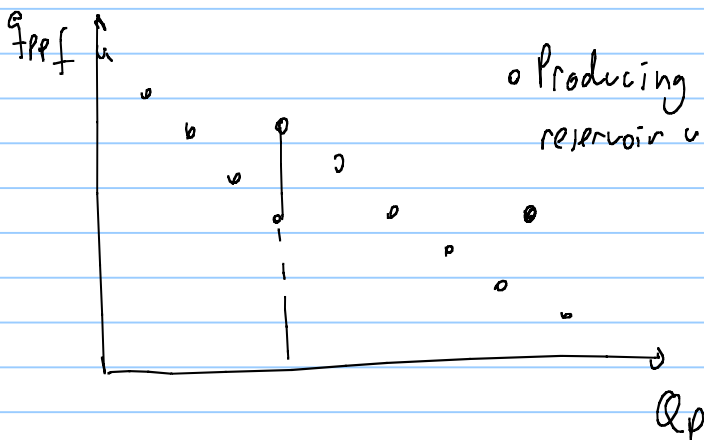
$$q = f(P_R - P_{wf})$$



IPR: pseudo-steady state representation of the deliverability of the reservoir at a given $P_R, M_P,$



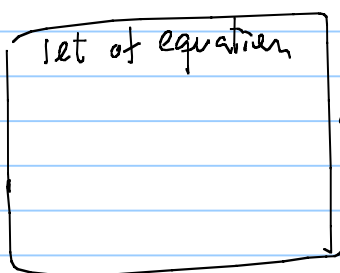
- Some complexities to calculate the production potential
 - IPR changes with depletion
 - GOR, WC of each well changes with depletion
 - Changes in the production system
 - adding new wells
 - add boosters
 - add Artificial lift
 - Producing from different reservoir units



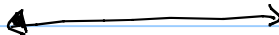
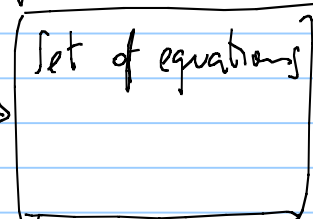
Usually, for calculating field performance we use:

- Coupled models reservoir + production system
implicit coupling

Reservoir simulation

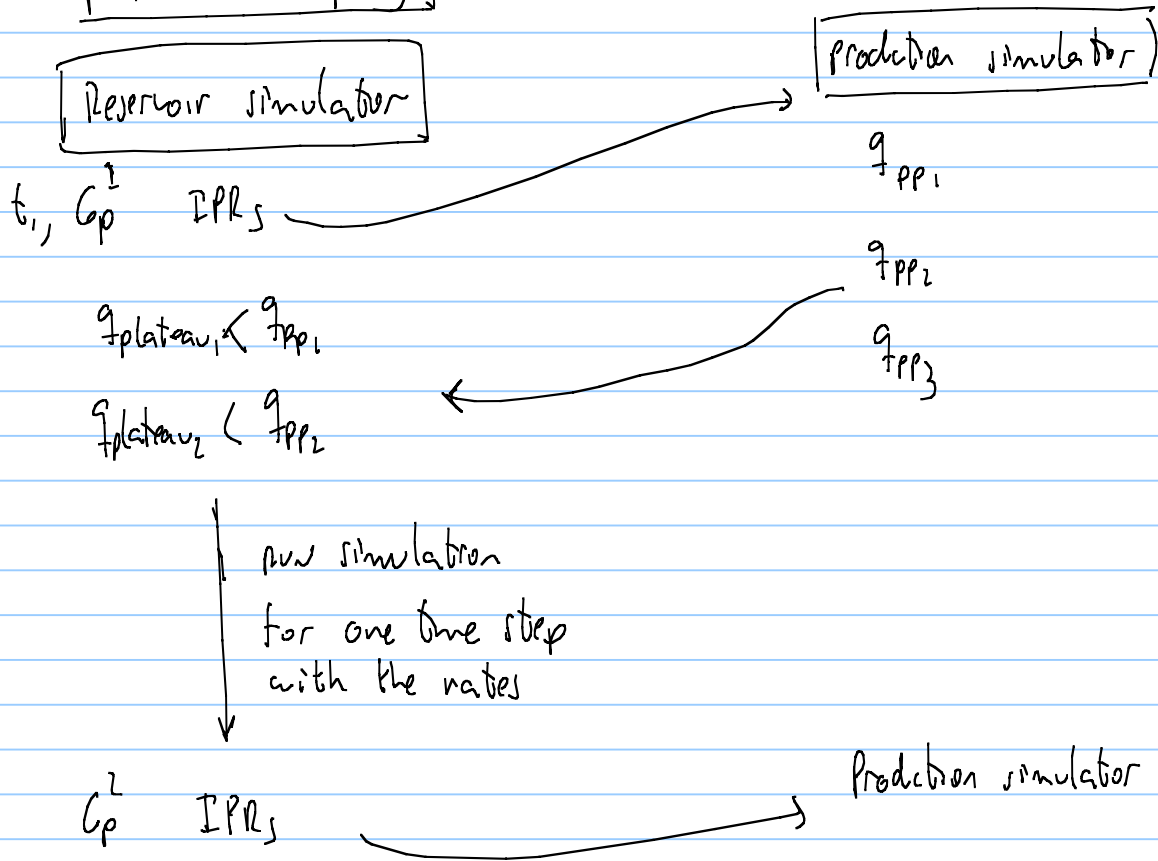


production simulator

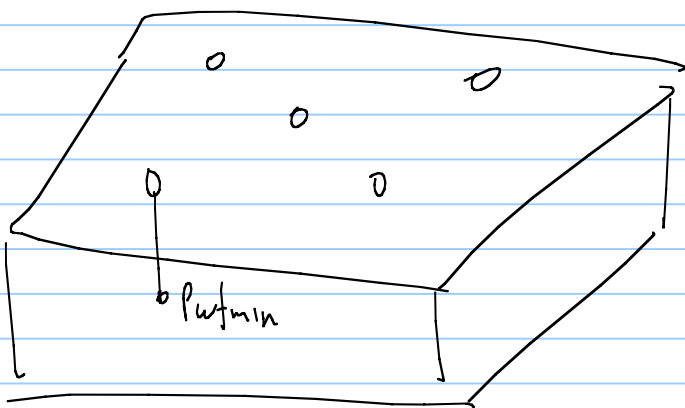


solve all equations simultaneously, time consuming, not very practical

explicit coupling to compute field performance.

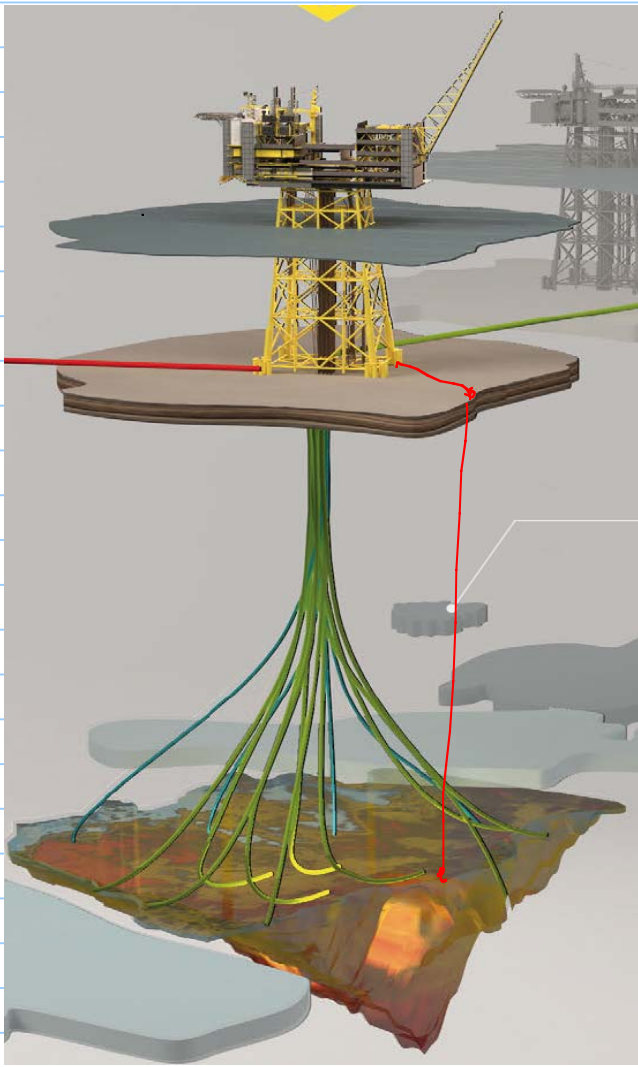
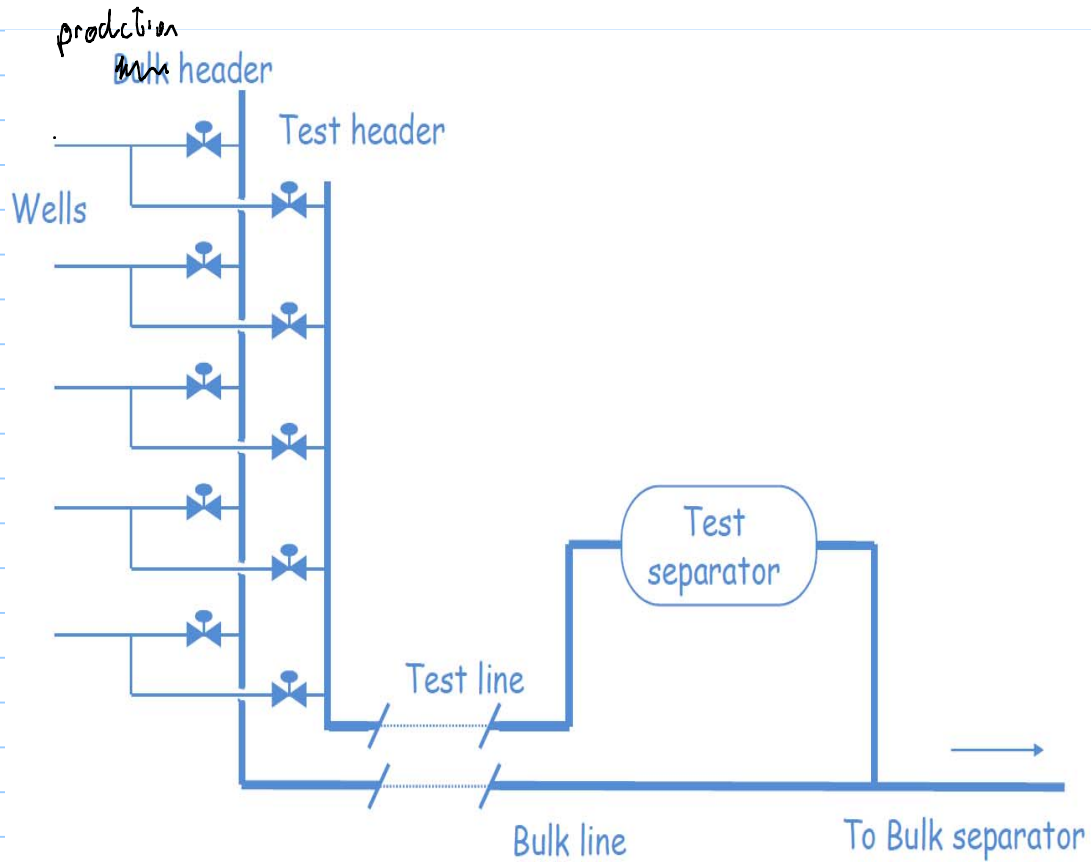


Very often the reservoir simulator is used standalone, with a minimum flowing bottomhole pressure to represent network backpressure

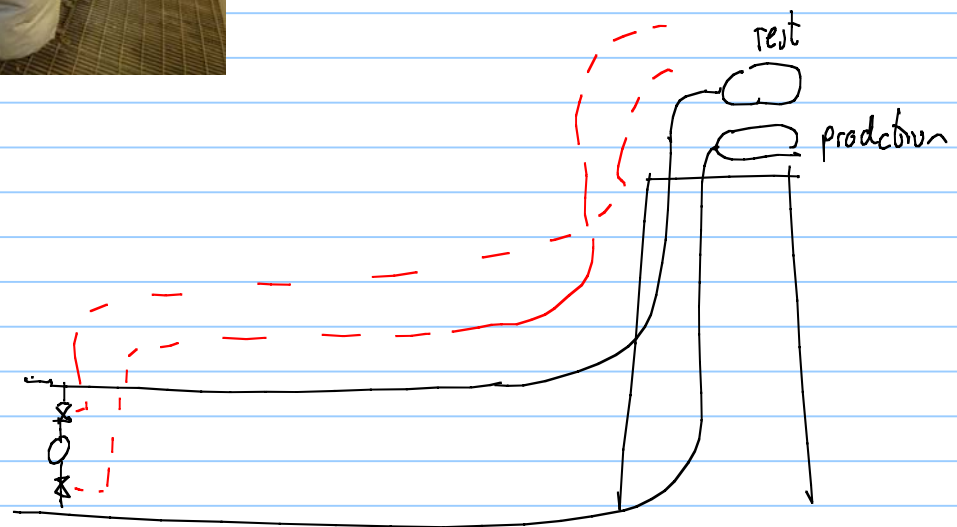


this is not always an accurate representation of the production system (well, pipeline, flowline, sep).

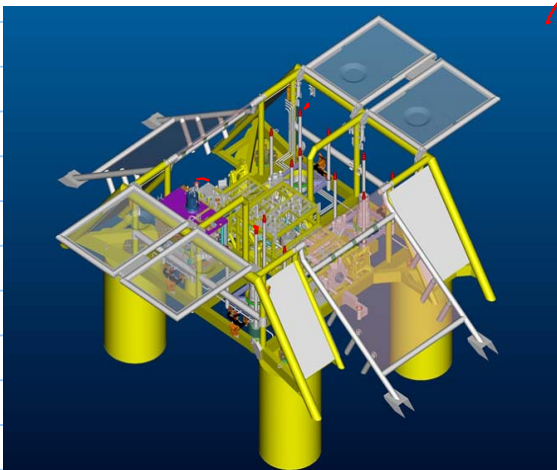
architecture of production systems



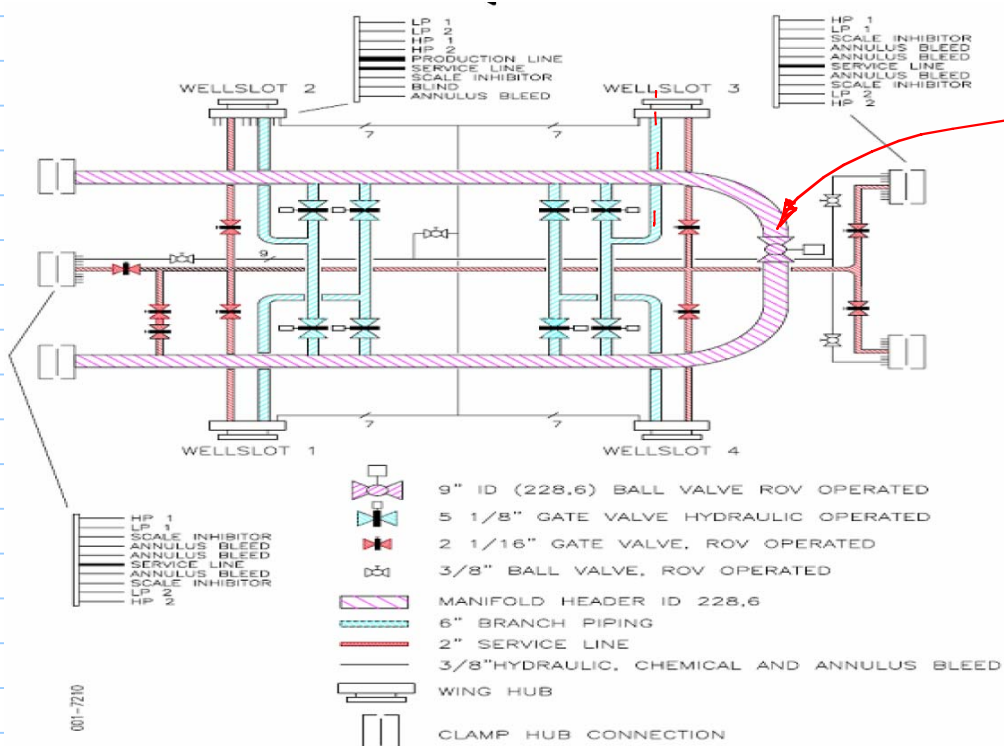
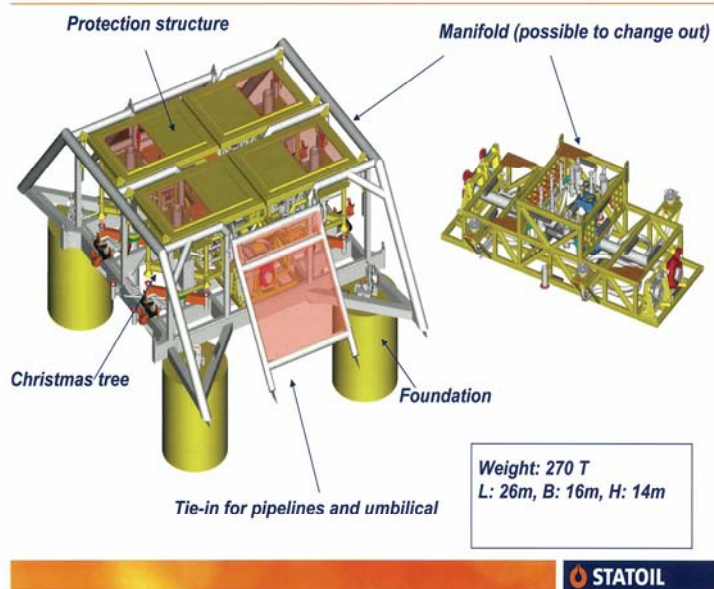




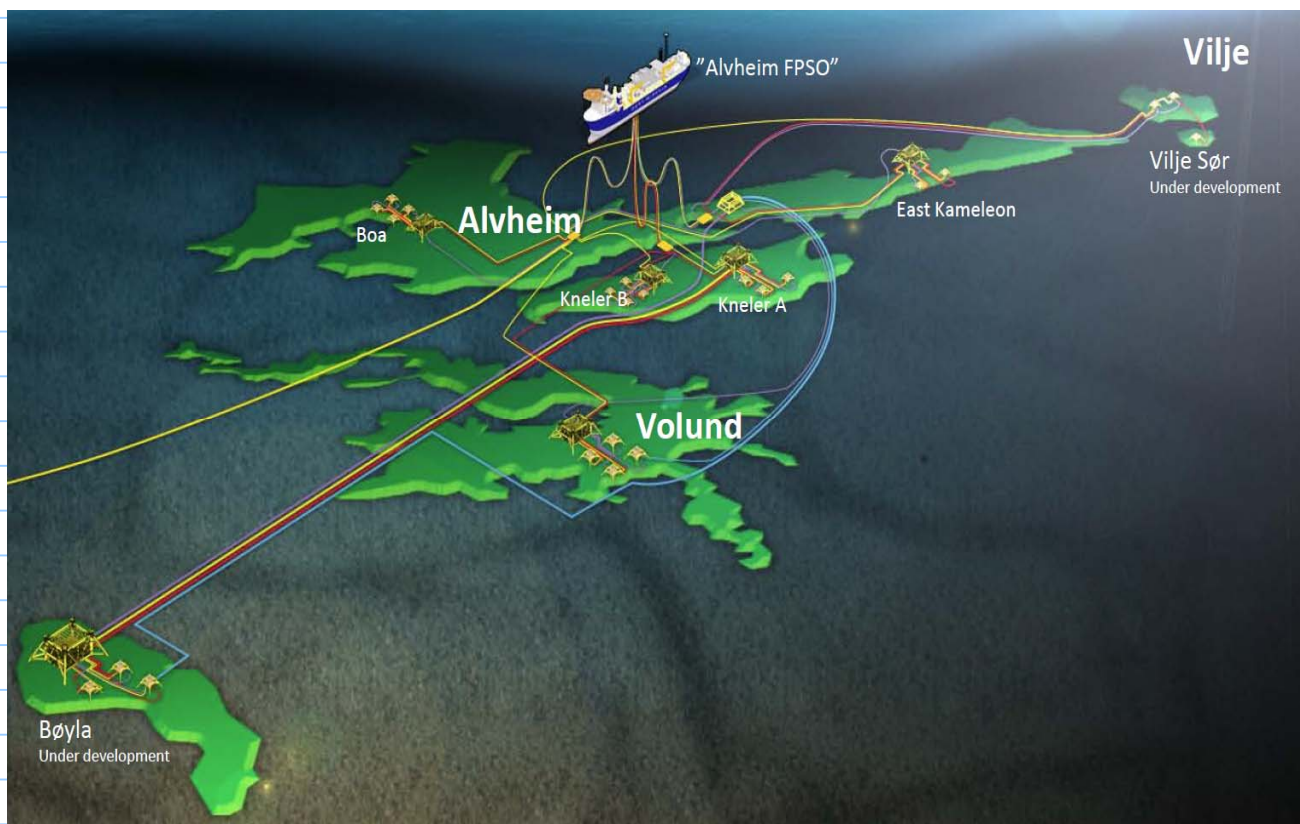
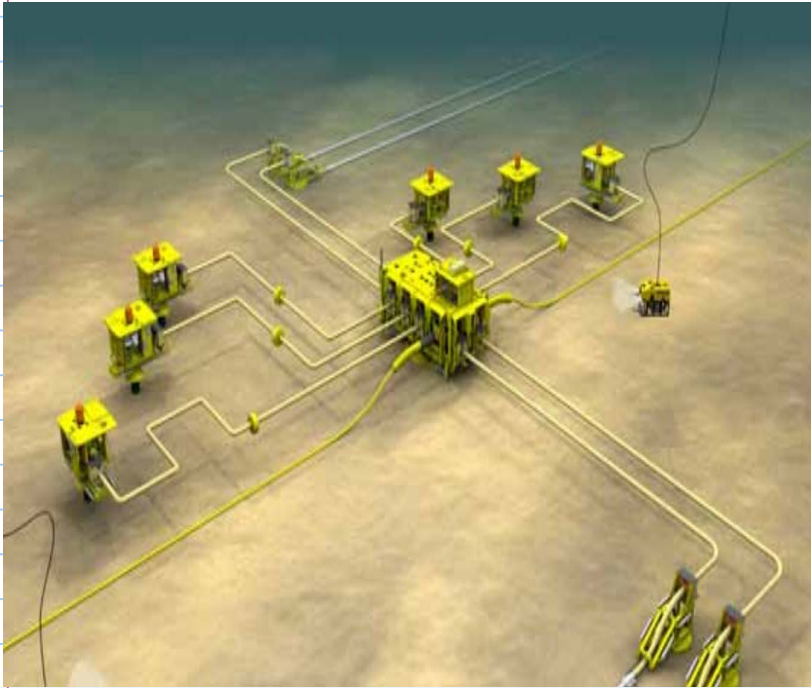
template



→ stabil 3/4

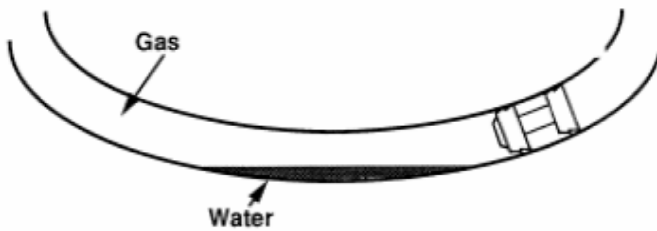


satellite wells



function of test and production line : for pigging operations.

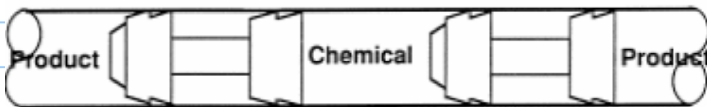
Removing water in a gas flow system



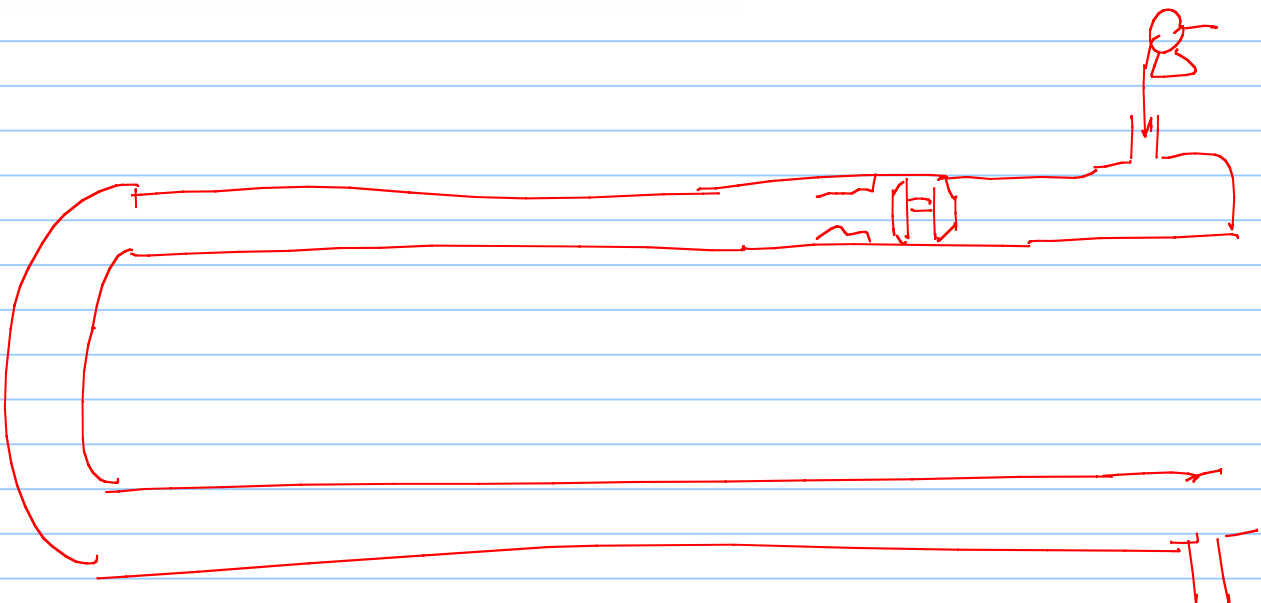
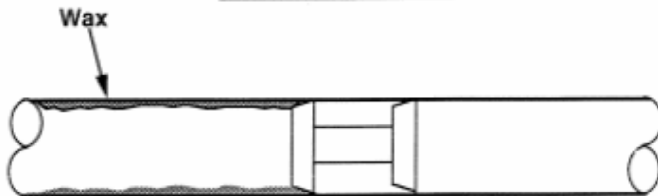
Removing water in a oil system

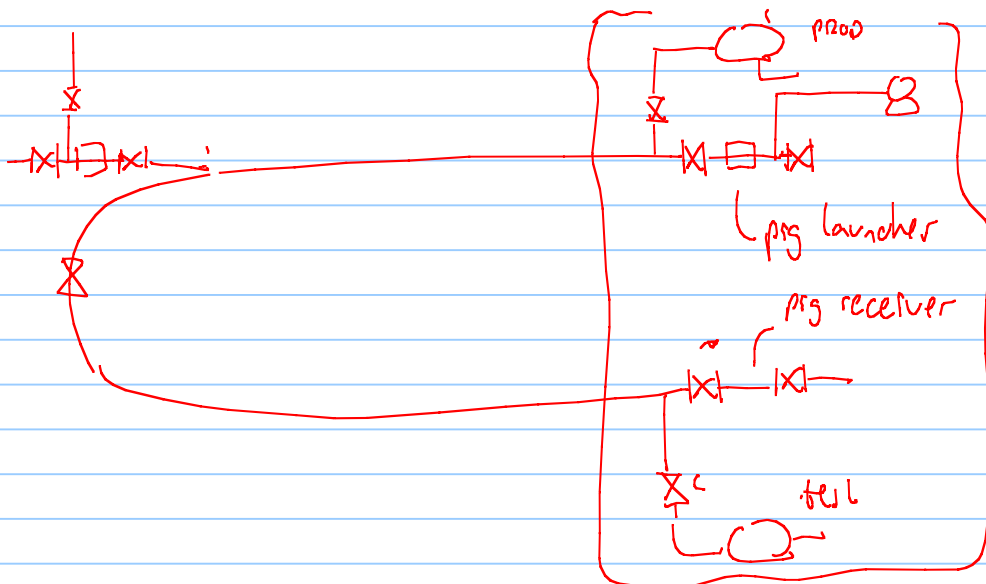


Treating by chemicals

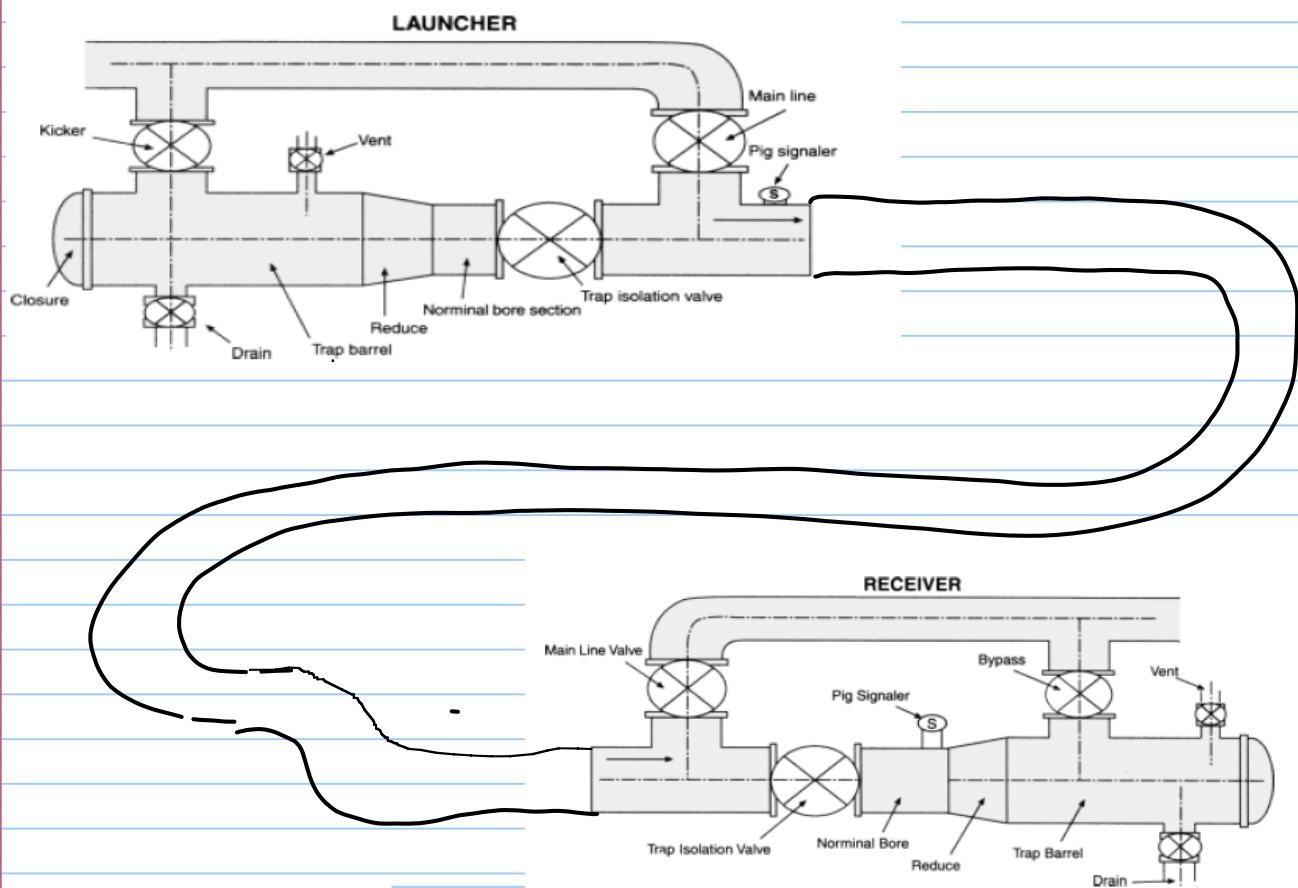


Removal of Wax





Pigging animation: <https://www.youtube.com/watch?v=CDHtL-J1Xxo>



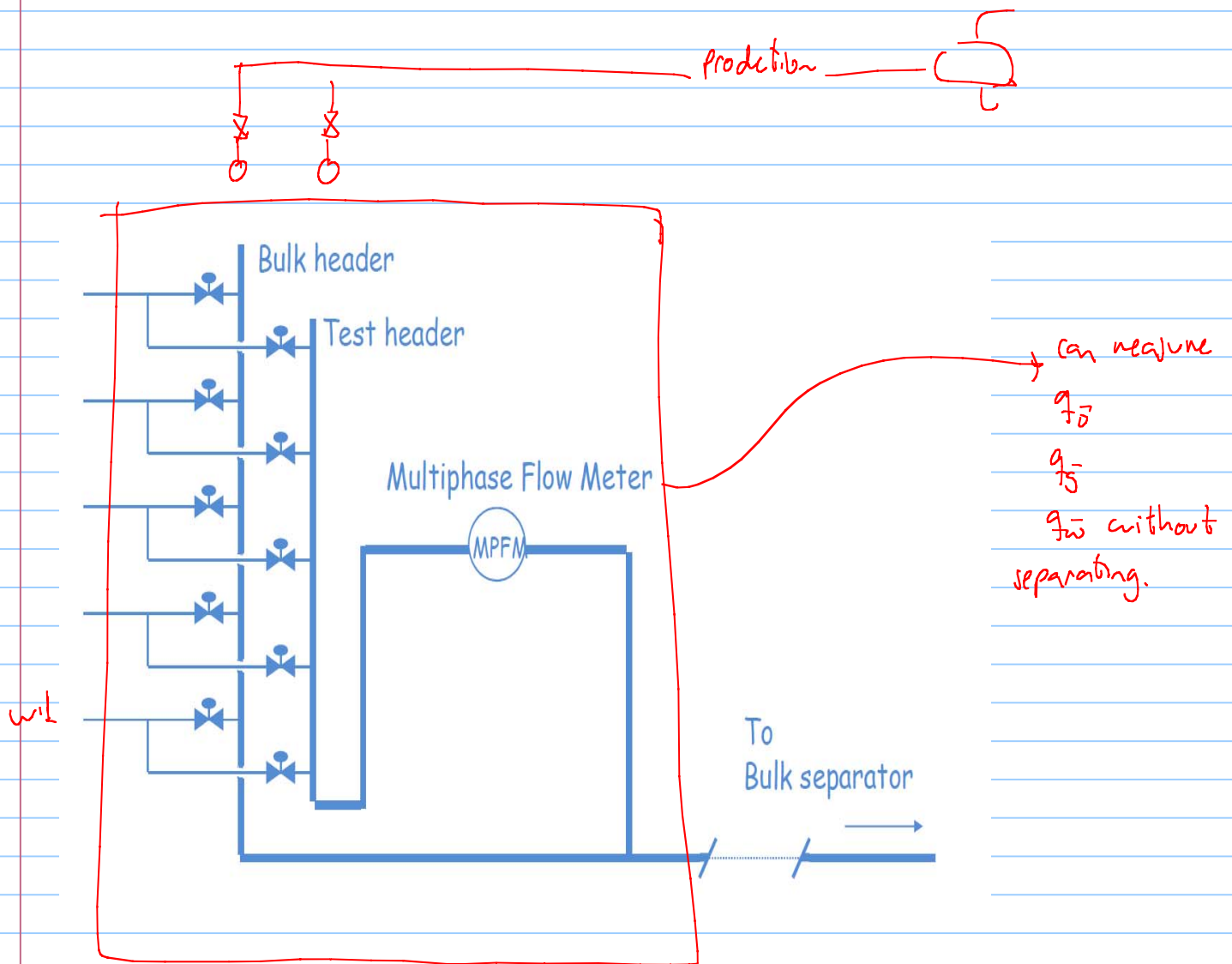
Wax plug-North Sea line pigging



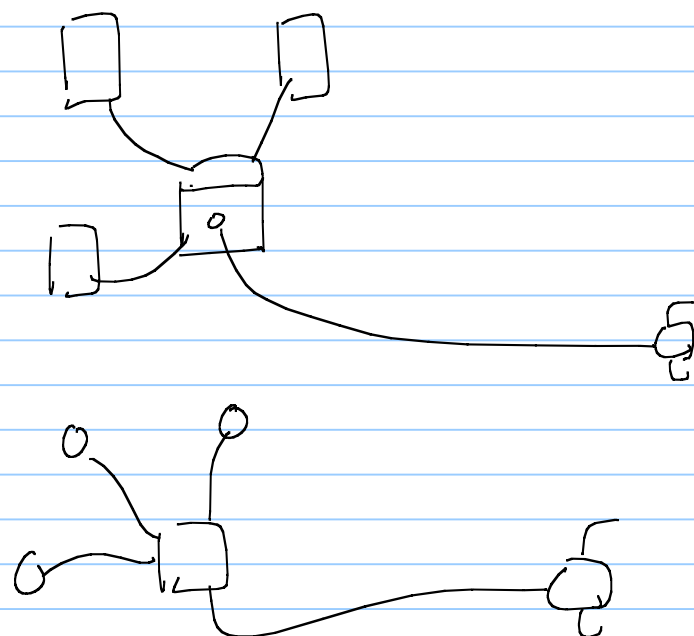
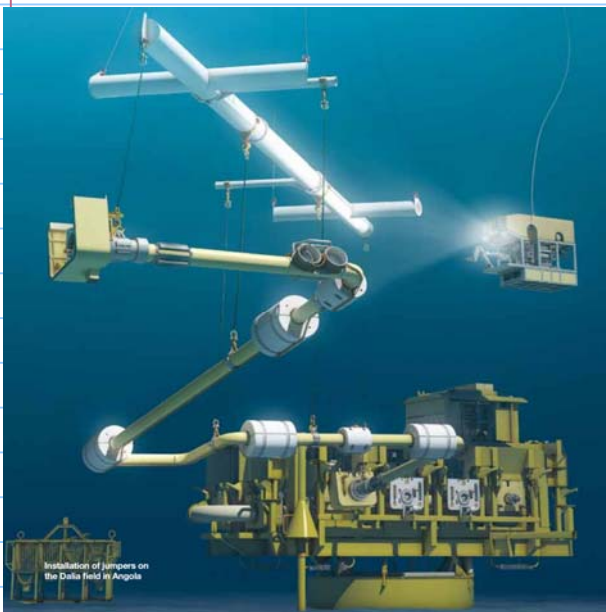
Various pig types



offshore pigging offshore pig launcher.

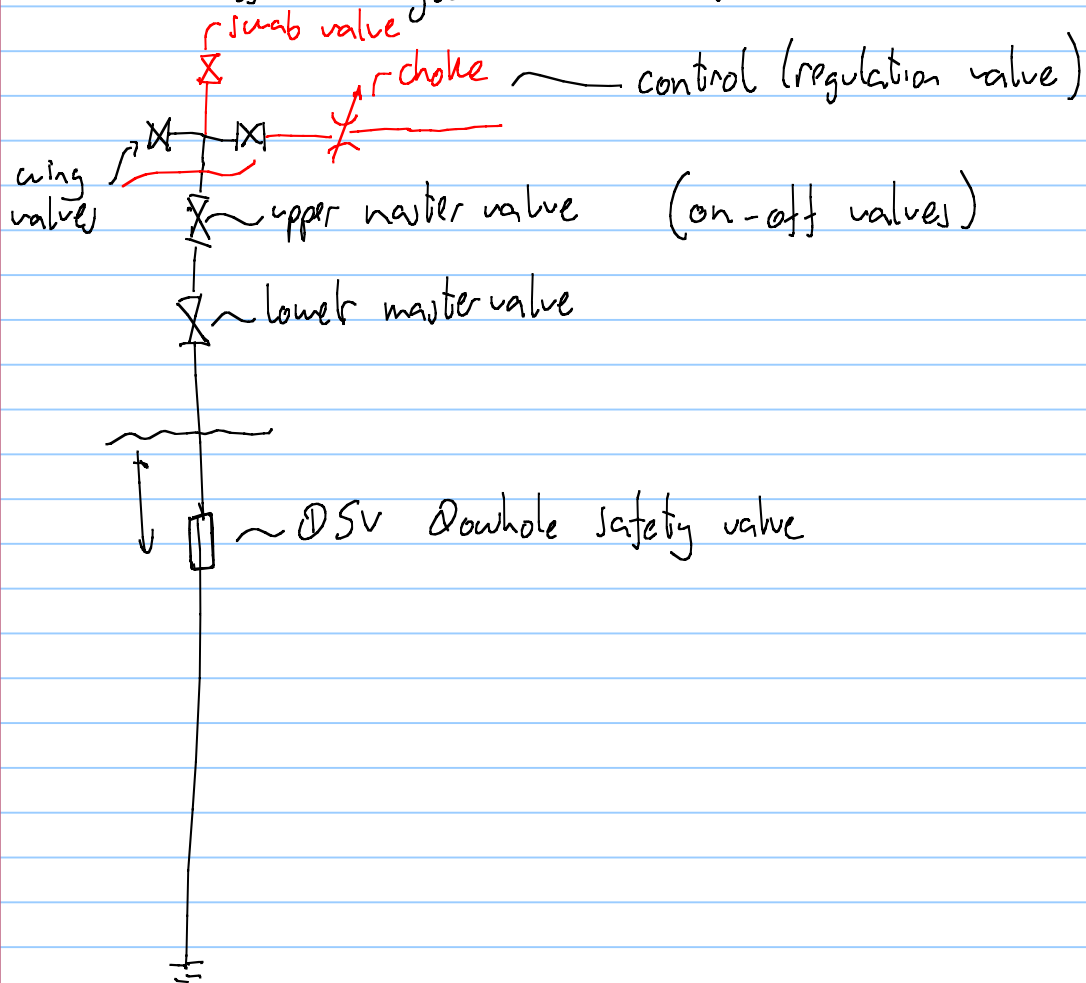


Connectors between well template, satellite well to manifold





main valves that you have in a well





SSSV subsurface safety
valve.

