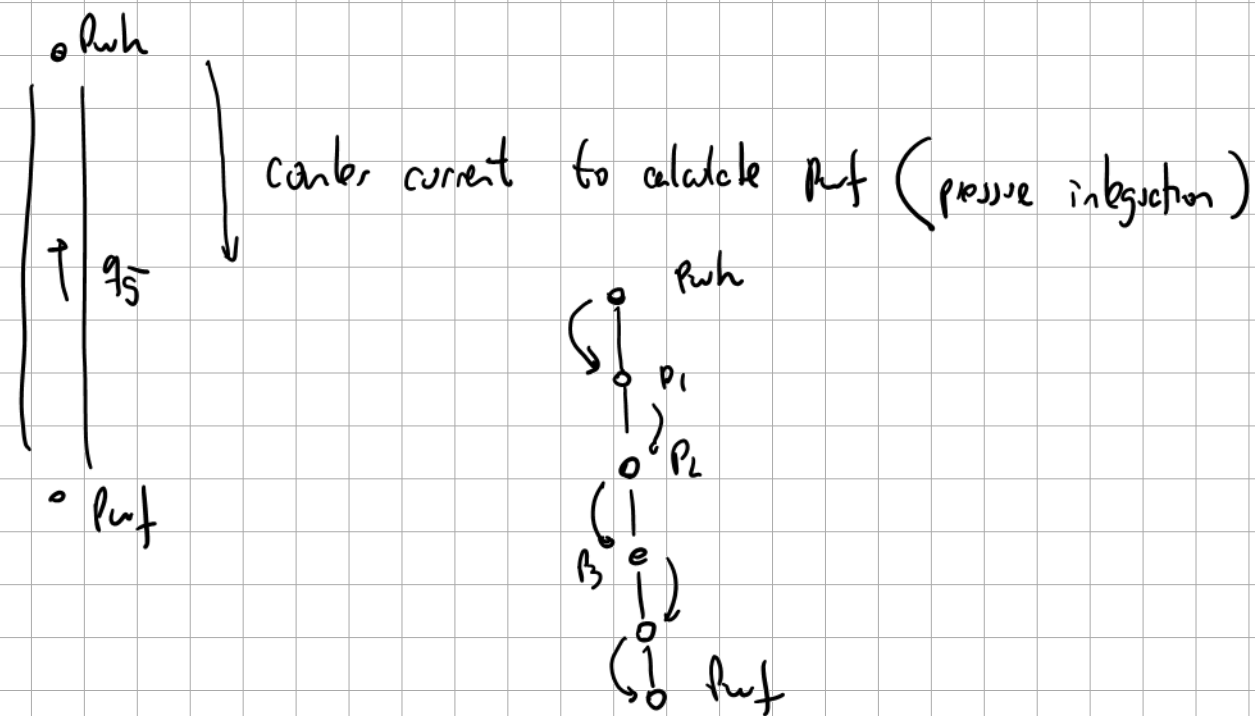
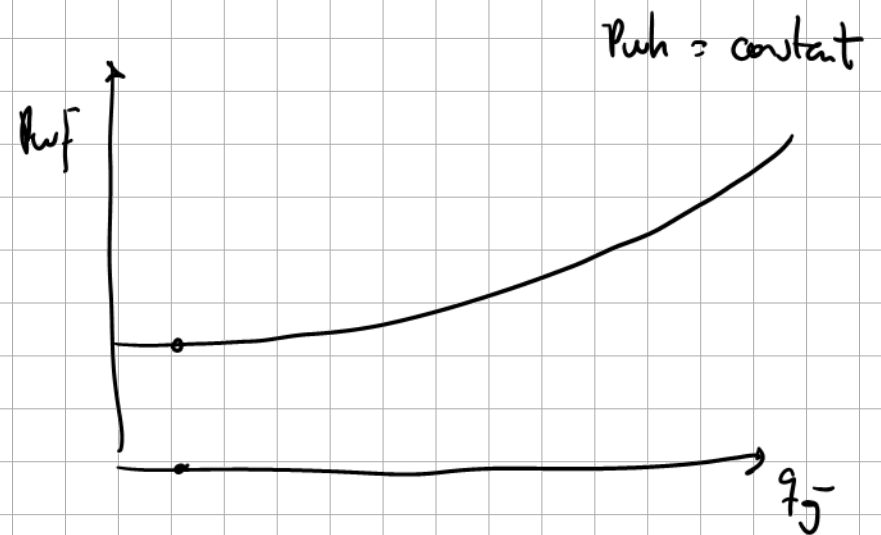
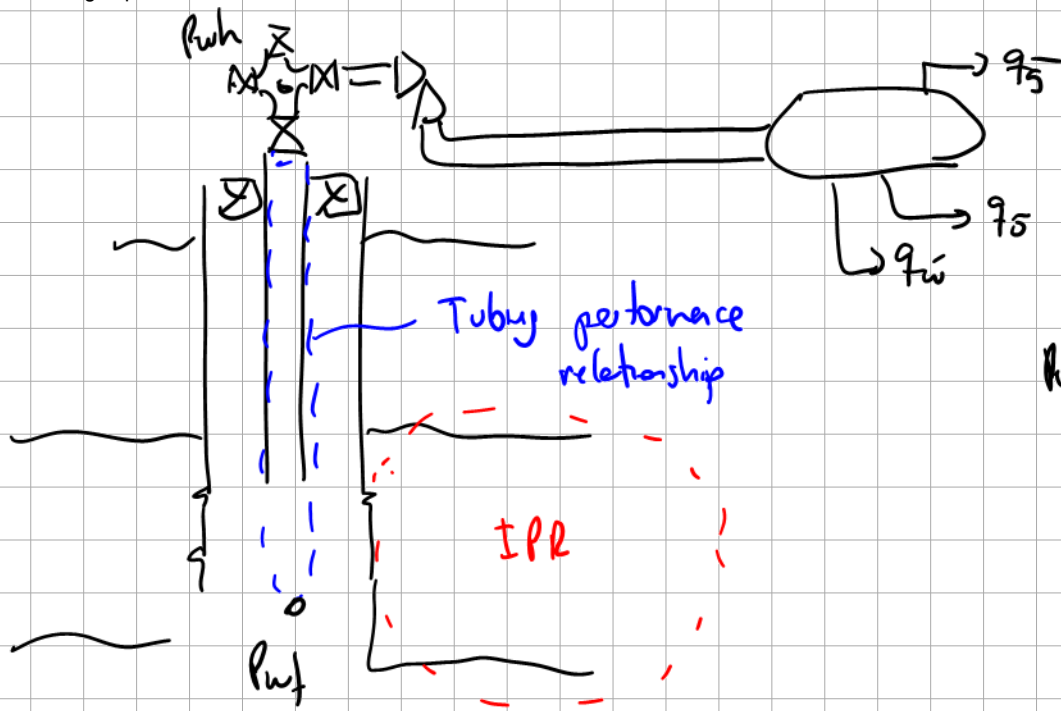




Lead $\rightarrow h_1 = h_2$ (no energy losses)

$$h = z + \frac{p}{\rho \cdot g} + \frac{v^2}{2g}$$

incompressible

$$h_1 = h_2 + \Delta h_{\text{losses}}$$

$$\Delta h_{\text{losses}} = \underbrace{\Delta h_{\text{expansion}}}_{\text{values restrictions}} + \Delta h_{\text{friction}}$$

$$\Delta h_{\text{friction}} = f \frac{L}{D} \frac{v^2}{2g}$$

Moody friction factor

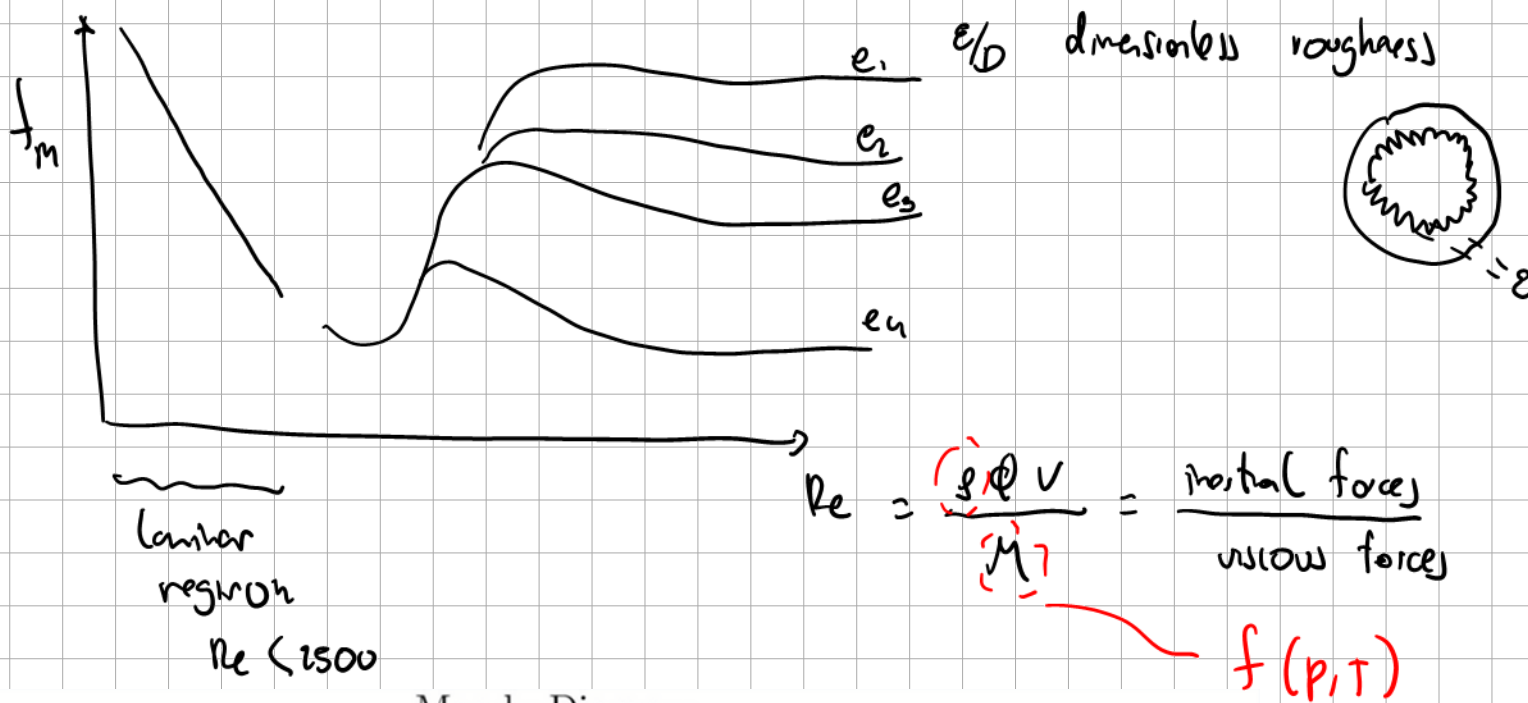
$$h_1 = z_1 + \frac{p_1}{\rho \cdot g} + \frac{v_1^2}{2g} = z_2 + \frac{p_2}{\rho \cdot g} + \frac{v_2^2}{2g} + f \frac{L}{D} \frac{v^2}{2g}$$

its incompressible, so $v_1 = v_2 = v$
 $Q = \text{constant}$

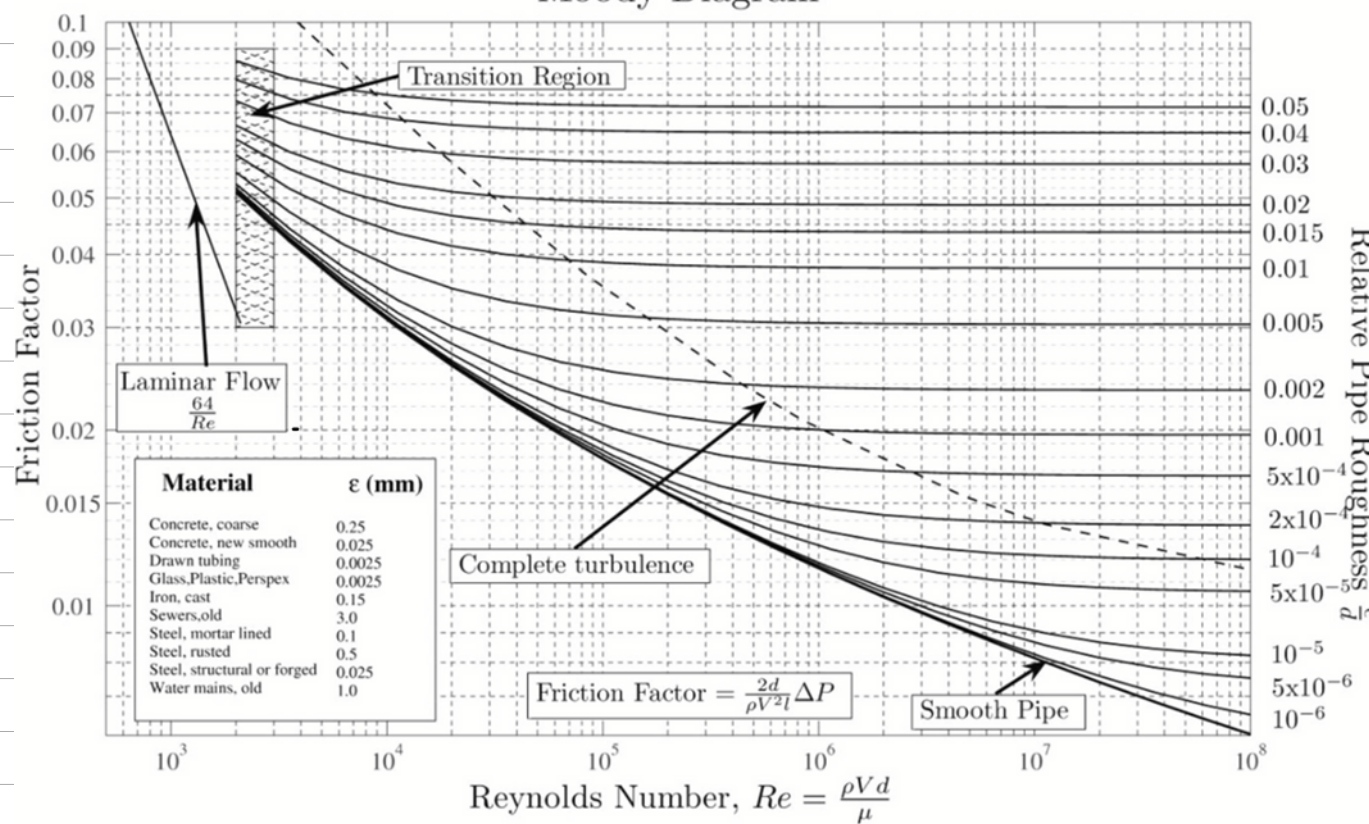
$$\Delta p = (p_1 - p_2) = \rho \cdot g \cdot (z_2 - z_1) + f \frac{L}{D} \frac{\rho \cdot g}{2} v^2$$

$$(p_1 - p_2) = \underbrace{\Delta z \cdot \rho \cdot g}_{\text{hydrostatic}} + \underbrace{f \frac{L}{D} \rho \frac{v^2}{2}}_{\text{friction}}$$

for gas $f = f(p, T)$



Moody Diagram



$$\begin{matrix} 1 & 0 & P_1, T_1 \\ 2 & 0 & P_2, T_2 \\ 3 & 0 & \\ & \vdots & \\ & 0 & P_N, T_N \\ & \vdots & \\ & 0 & P_N, T_N \end{matrix}$$

$N \rightarrow N-1$, gas properties don't change much

valid if ΔL is small

$$\frac{\Delta T}{\Delta p} \text{ is small}$$

$$\tilde{v}_g = \frac{q_g}{A} = \frac{q_g B_g(p, T)}{A}$$



$$B_g = \frac{q_g}{q_{gs}}$$

$$q_{gs} \cdot L_s = q_g \cdot L_s$$

$$B_g = \frac{q_g}{q_{gs}} = \frac{p_{gs}}{p_g} = \frac{z T}{p} \left(\frac{p_{sc}}{T_{sc}} \right)$$

$$p_{gs} = \frac{p_{sc}}{R z_{sc} T_{sc}}$$

$$p_g = \frac{p}{z R T}$$

$$\frac{m^3}{d} \quad \frac{1 d}{24 h} \quad \frac{1 h}{3600 s}$$

qg [Sm ³ /d]	2.85E+06
Gas gravity	0.7
Tubing ID [m]	0.157
Tubing cross section area [m ²]	0.019
Tubing roughness [m]	1.50E-06

TVD [m]	p [bara]	T [C]	Z [-]	deng [kg/m ³]	Bg [m ³ /Sm ³]	viscg [cp]	qg [m ³ /d]	vg [m/s]	p-calc [bara]
0	40	87	0.948	28.6	3.00E-02	1.36E-02	8.54E+04	51.03	
284	46	89	0.942	32.9	2.60E-02	1.38E-02	7.41E+04	44.28	
567	51	90	0.938	36.8	2.32E-02	1.39E-02	6.63E+04	39.61	
851	56	92	0.934	40.4	2.12E-02	1.41E-02	6.04E+04	36.14	
1135	61	94	0.930	43.6	1.96E-02	1.43E-02	5.59E+04	33.43	
1418	66	96	0.928	46.7	1.83E-02	1.45E-02	5.23E+04	31.25	
1702	70	98	0.926	49.5	1.73E-02	1.46E-02	4.92E+04	29.44	
1986	74	99	0.924	52.2	1.64E-02	1.48E-02	4.67E+04	27.92	
2269	78	101	0.922	54.8	1.56E-02	1.49E-02	4.45E+04	26.61	
2553	81	103	0.921	57.3	1.49E-02	1.51E-02	4.26E+04	25.47	
2837	85	105	0.920	59.6	1.44E-02	1.52E-02	4.09E+04	24.46	

2837 - 2553

$$P_{w-1} = P_{wf} \quad \text{?}$$

$$P_{w-1} = P_{wf} - \rho \cdot g \cdot \Delta z - \int \frac{L}{Q} \rho \frac{v^2}{2}$$

using conditions at P_{wf} !

Function Pout(qt1, ID, den, viscg, Length, teta, pin, roughness)

'Function that give pressure available at the outlet of a pipe with a flow qt and inlet pressure pressure pin

'Calculation made for liquid single phase flow

'Takes in data in SI

'qt flow [m³/d]

'ID inner diameter of pipe [m]

'den density of fluid, [kg/m³]

'viscg viscosity of fluid, [Pa s]

'Length, pipe length, [m]

'teta inclination angle of pipe with respect to horizontal [°]

'pin, discharge pressure required, [bara]

'roughness of pipe [m]

'Gravitational acceleration g, [m/s²]

g = 9.81

'Pi number

Pi = 4 * Atn(1)

qt = qt1 / (3600# * 24#) '[m³/s]

'Calculating area and velocity

Area = Pi * (ID ^ 2) / 4

v = qt / Area

Pressscalcl = pin - (Length * Sin(teta * Pi / 180) * den * g / 100000#) - ((factor(den, viscg, ID, roughness, v) * Length * (v ^ 2) * den / (ID * 200000#))

Pout = Pressscalcl

End Function

change for m³/d to m³/s

dividing by 1e5 to take from Pa to bara

TVD [m]	p [bara]	T [C]	Z [-]	deng [kg/m ³]	Bg [m ³ /Sm ³]	viscg [cp]	qg [m ³ /d]	vg [m/s]	p-calc [bara]
0	40	87	0.948	28.6	3.00E-02	1.36E-02	8.54E+04	51.03	35.55
284	46	89	0.942	32.9	2.60E-02	1.38E-02	7.41E+04	44.28	41.50
567	51	90	0.938	36.8	2.32E-02	1.39E-02	6.63E+04	39.61	47.03
851	56	92	0.934	40.4	2.12E-02	1.41E-02	6.04E+04	36.14	52.27
1135	61	94	0.930	43.6	1.96E-02	1.43E-02	5.59E+04	33.43	57.29
1418	66	96	0.928	46.7	1.83E-02	1.45E-02	5.23E+04	31.25	62.15
1702	70	98	0.926	49.5	1.73E-02	1.46E-02	4.92E+04	29.44	66.88
1986	74	99	0.924	52.2	1.64E-02	1.48E-02	4.67E+04	27.92	71.52
2269	78	101	0.922	54.8	1.56E-02	1.49E-02	4.45E+04	26.61	76.08
2553	81	103	0.921	57.3	1.49E-02	1.51E-02	4.26E+04	25.47	80.59
2837	85	105	0.920	59.6	1.44E-02	1.52E-02	4.09E+04	24.46	85.04

surprisingly close !