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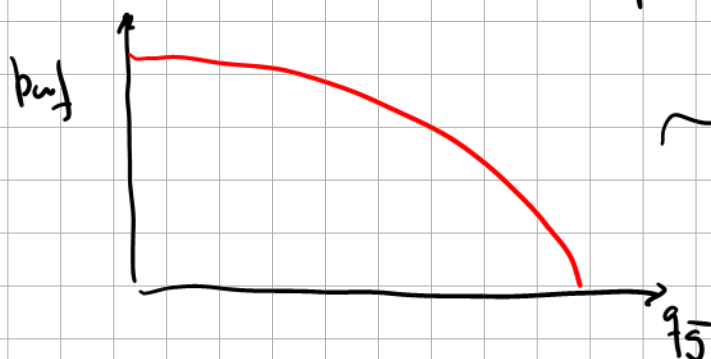
(1935)

Monograph 7

Back-Pressure Data on Natural-Gas Wells and Their Application to Production Practices

By
E. L. RAWLINS AND M. A. SCHELLHARDT

Back-pressure equation



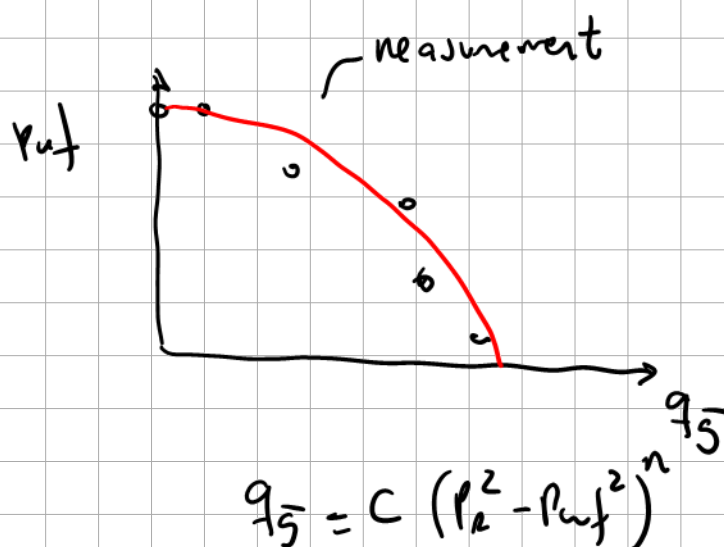
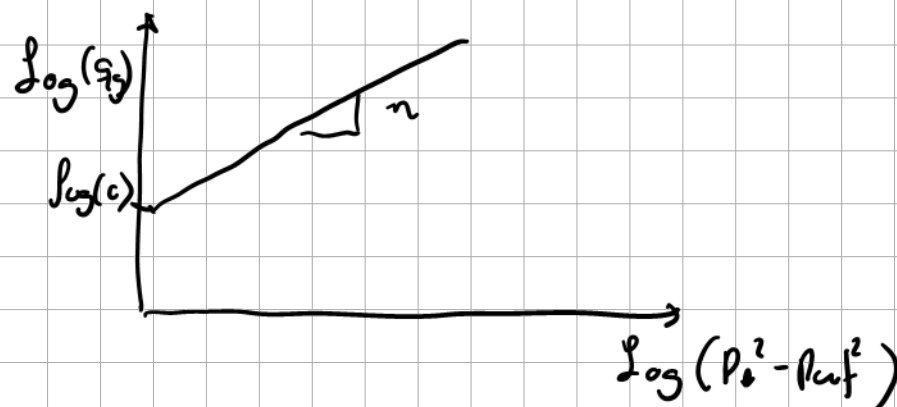
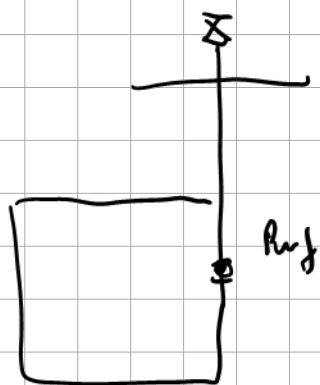
$$q_g \sim C (P_R^2 - P_{wf}^2)^n \quad \text{empirically, measured in the field} \quad 0.5 \leq n \leq 1$$

$$\frac{q_g}{C} = (P_R^2 - P_{wf}^2)^n \quad \text{Log}$$

$$\text{Log}\left(\frac{q_g}{C}\right) = \text{Log}\left((P_R^2 - P_{wf}^2)^n\right)$$

$$\text{Log}(q_g) - \text{Log}(C) = n \cdot \text{Log}(P_R^2 - P_{wf}^2)$$

$$\text{Log}(q_g) = \text{Log}(C) + n \cdot \text{Log}(P_R^2 - P_{wf}^2)$$



in Excel change C, n to match data

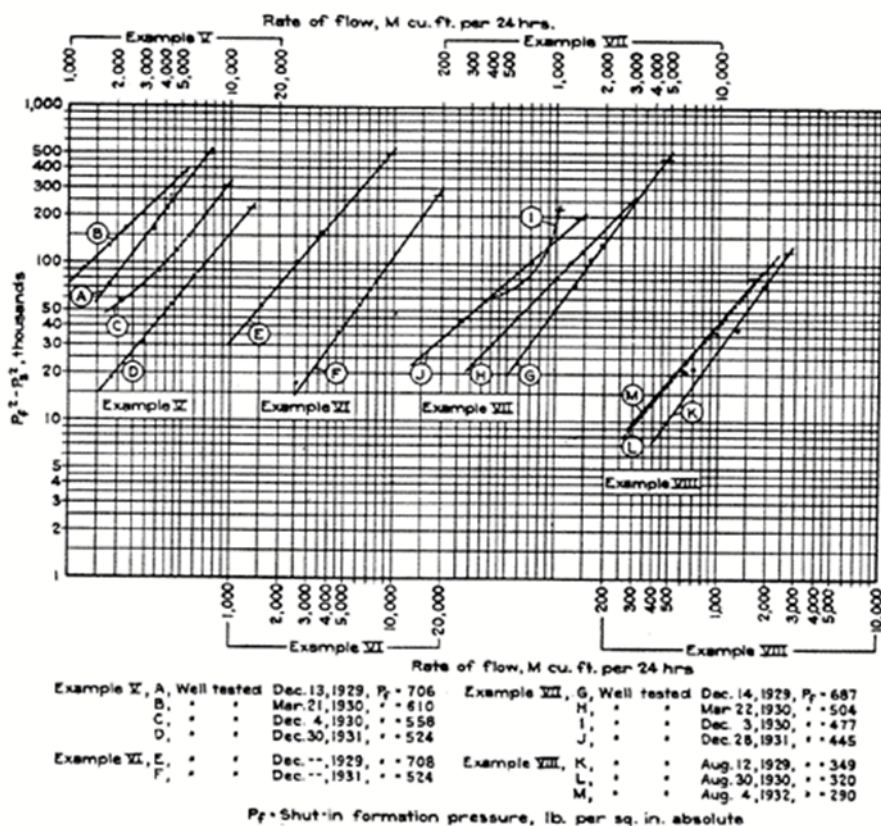


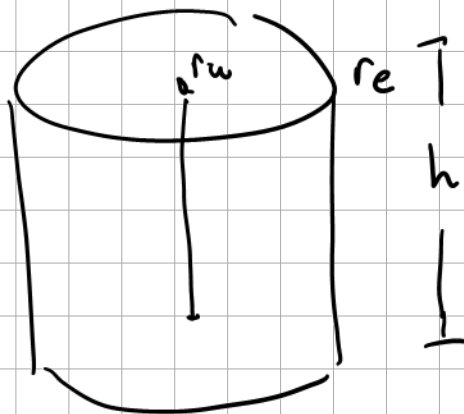
FIGURE 24.—Variation in delivery capacities of gas wells at different times in their productive lives, examples V, VI, VII, and VIII

analytical derivation of Dry gas IPR

$$q_g$$

$$v = \frac{k}{\mu_g} \frac{dp}{dr}$$

$$\frac{q_g}{2\pi r h} = \frac{k}{\mu_g} \frac{dp}{dr}$$



$$q_g = f(q_g)$$

$$B_g = \frac{q_g}{q_g}$$

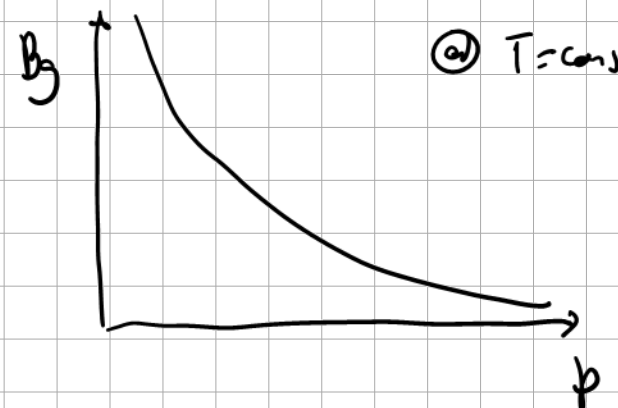
$$q_g = q_g \cdot B_g$$

$$\int_{r_w}^{r_{@pR}} \frac{q_g}{r} = \int_{p_wf}^{p_R} \frac{2\pi k h}{B_g \mu_g} \frac{dp}{dr}$$

for PSS

$$q_g = \frac{2\pi k h}{(\ln(\frac{r_e}{r_w}) - 0.75)}$$

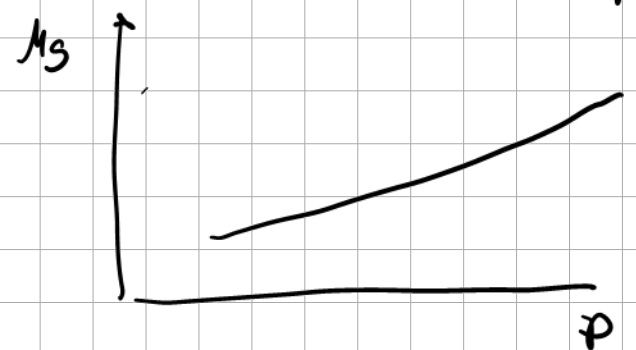
$$\int_{p_wf}^{p_R} \frac{1}{B_g \mu_g} dp$$



mass conservation

$$q_g \cdot \rho_g = q_g \cdot \rho_g$$

$$B_g = \frac{q_g}{q_g} = \frac{\rho_g}{\rho_g}$$



Real gas equation

$$\frac{p}{\rho} = z R T$$

$$R = \frac{R_u}{M_w}$$

gas deviation factor

$$z = \frac{p}{z R T}$$

deviation from ideal gas

Bovle (Enqlish)



Hooke (Enqlish)



Charles (French)



Gay-Lussac (French)



Avogadro (Italian)

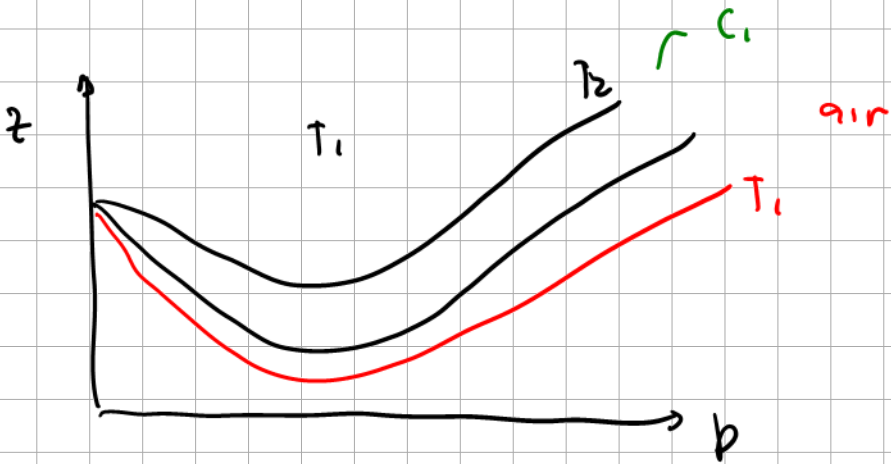


$z \sim$

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(INCORPORATED)

Density of Natural Gases

BY MARSHALL B. STANDING* AND DONALD L. KATZ,* MEMBER A.I.M.E.
(New York Meeting, February 1941)



Marshall B. Standing



Donald L. Katz

$$T_r = \frac{T}{T_c}$$

$$P_r = \frac{p}{p_c}$$

$$T_c, p_c$$

$$T_c, p_c = f(\text{MW})$$

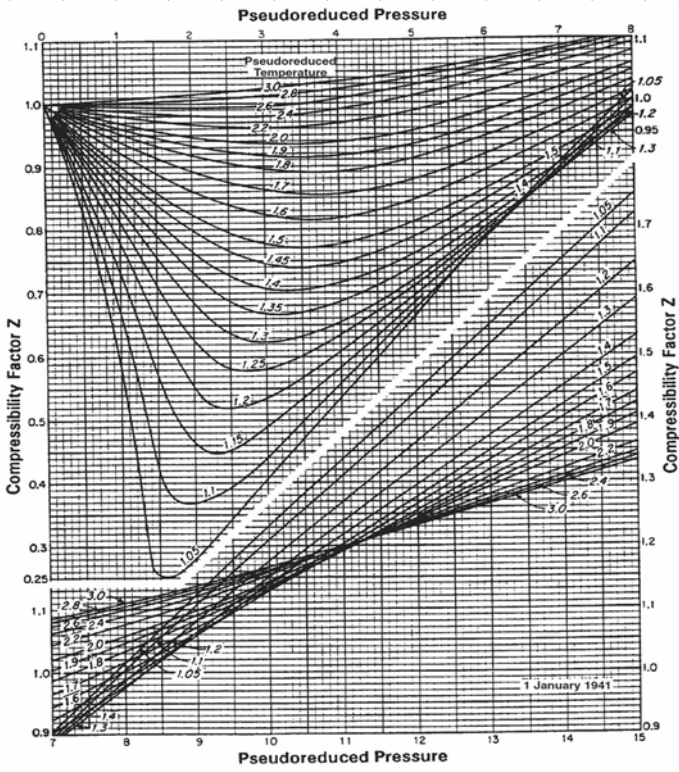
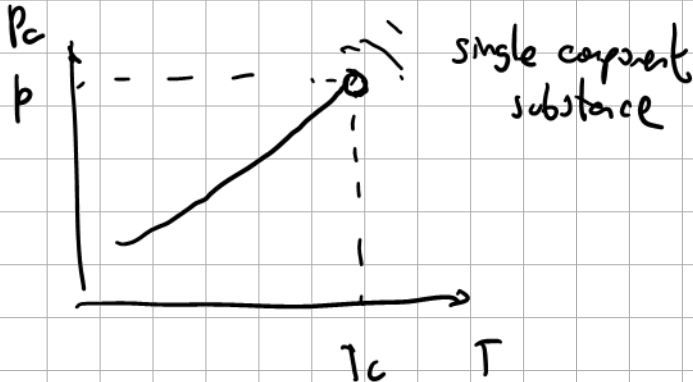


Fig. 3.6—Standing-Katz⁴ Z-factor chart.

Gas composition

Component	mole fraction
C_1	z_{c1}
C_2	z_{c2}
C_3	z_{c3}
\vdots	

$$\sum_{i=1}^N z_{ci} = 1$$

$$MW_{mix} = \sum_1^N MW_i z_i$$

$$T_c, p_c = f(MW_{mix}) \rightarrow \text{Sutton}$$

$$B_g = \frac{p_g}{p_g}$$

$$p_g = \frac{p_{sc}}{z_{sc} R T_{sc}}$$

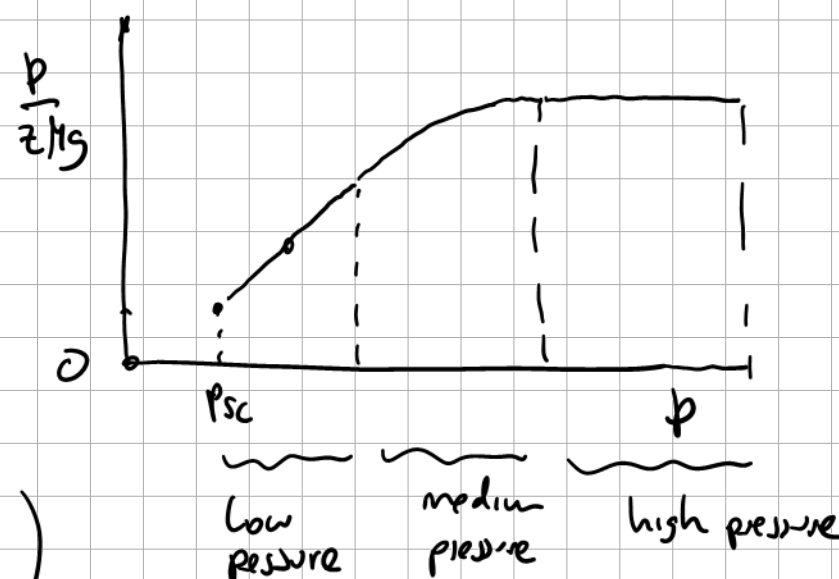
$$p_g = \frac{p}{z R T}$$

$$B_g = \frac{p_{sc}}{T_{sc}} \cdot \frac{z T}{p}$$

$p_{sc} = 1.01325 \text{ bara}$
 $T_{sc} = 15.56^\circ \text{C}$

$$q_g = \frac{2\pi k h}{(\ln(r_e/r_w) - 0.75)} \int_{p_{wf}}^{p_r} \frac{1}{M_g B_g} dp$$

$$q_g = \frac{2\pi k h}{\ln(r_e/r_w) - 0.75} \frac{T_{sc}}{p_{sc} T_r} \int_{p_{wf}}^{p_r} \frac{p}{z M_g} dp$$



low pressure (p_{wf}, p_r)

$$q_g = \frac{2\pi k h}{(\ln(r_e/r_w) - 0.75)} \frac{T_{sc}}{p_{sc} T_r} 0.5 \left(p_r^2 - p_{wf}^2 \right) \left(\frac{1}{z M_g} \right)_{@ p_r}$$

in the low pressure region $\left(\frac{1}{M_g z} \right) = \text{const}$

$$q_g = C (p_r^2 - p_{wf}^2)^n \quad \text{if } n=1 \quad \text{it's a match!}$$

high pressure

$$q_g = \frac{2\pi k h}{(\ln(r_e/r_w) - 0.75)} \frac{T_{sc}}{p_{sc} T_r} \left(\frac{p}{M_g z} \right)_{@ p_r} \int_{p_{wf}}^{p_r} dp = \frac{2\pi k h}{(\ln(r_e/r_w) - 0.75)} \frac{T_{sc}}{p_{sc} T_r} \frac{p_r}{M_g z} (p_r - p_{wf})$$

any pressure constant

similar to undersaturated oil IPR

doesn't resemble $q_g = C (p_r^2 - p_{wf}^2)^n$

$$q_o = J (p_r - p_{wf})$$