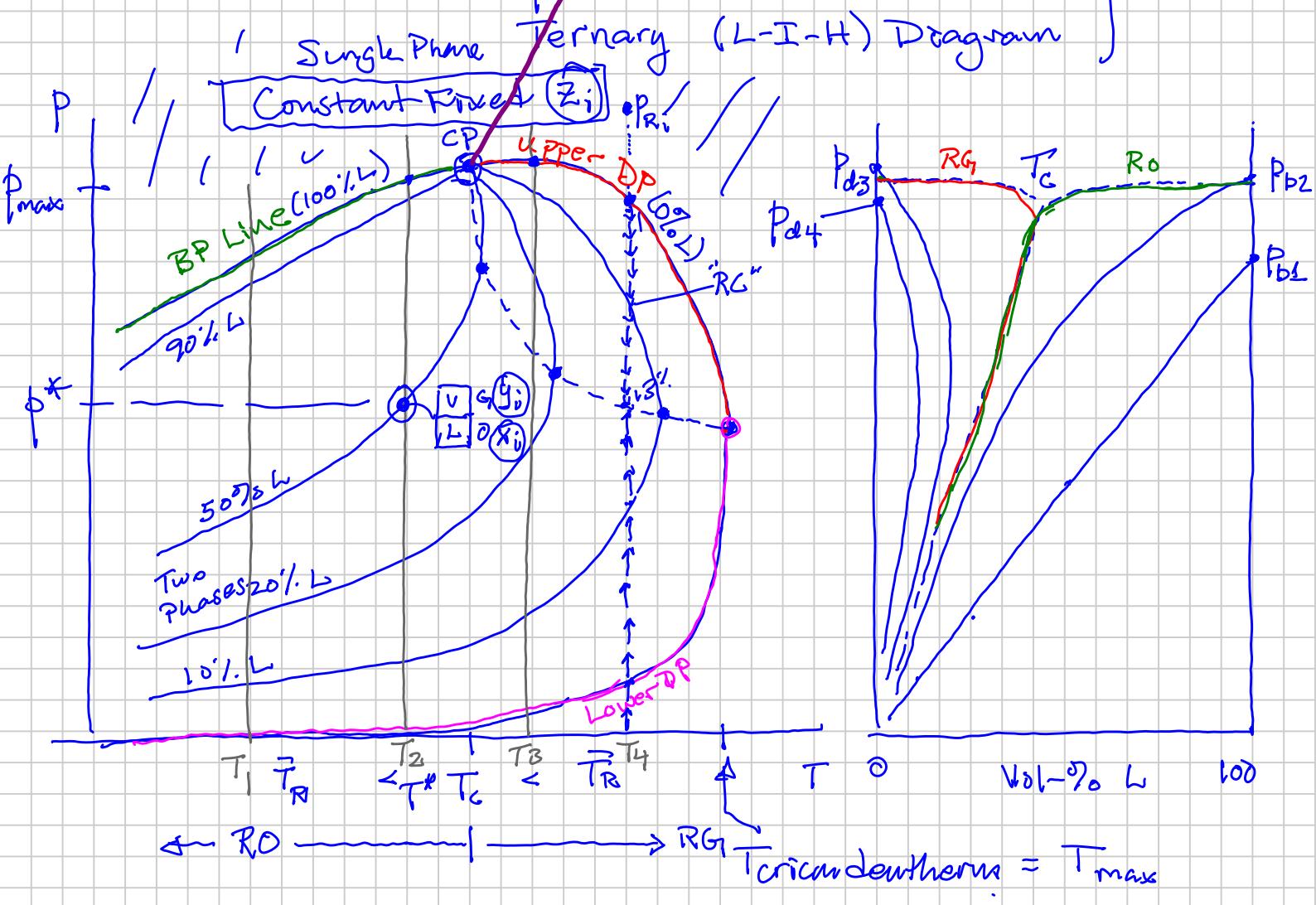


## Multi (>2) Component Phase Diagrams

Naturally-occurring petroleum reservoir fluids

$$\begin{aligned} P-T & \quad \beta = \beta_0 \\ P-V & \quad (P - V_{ro}) \\ P-Z_i & \end{aligned}$$

} Orientation about  $Z_i$



$$CP, P_b(T), P_d(T) : f(Z_i)$$

$$P_{\text{max}} = \text{Criticodenbar}$$

Condensation: Appearance of a liquid phase from a gas phase

Retrograde Condensation: Increasing liquid volume as pressure decreases

Revolatilization: below the --- (Retrograde Cond) where liquid volume decreases as P decreases

# Ternary Diagram (Typically Only used Inj-Gas cut to R0)

$Z_i \Rightarrow 3$  "Pseudo" Components

L (light)

C<sub>1</sub> N<sub>2</sub>

I (intermediate)

CO<sub>2</sub> C<sub>2</sub>-C<sub>5</sub>

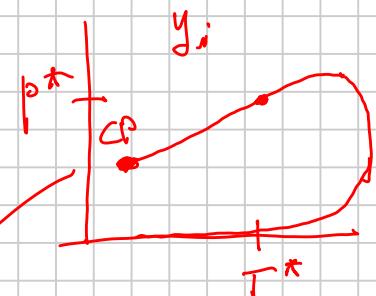
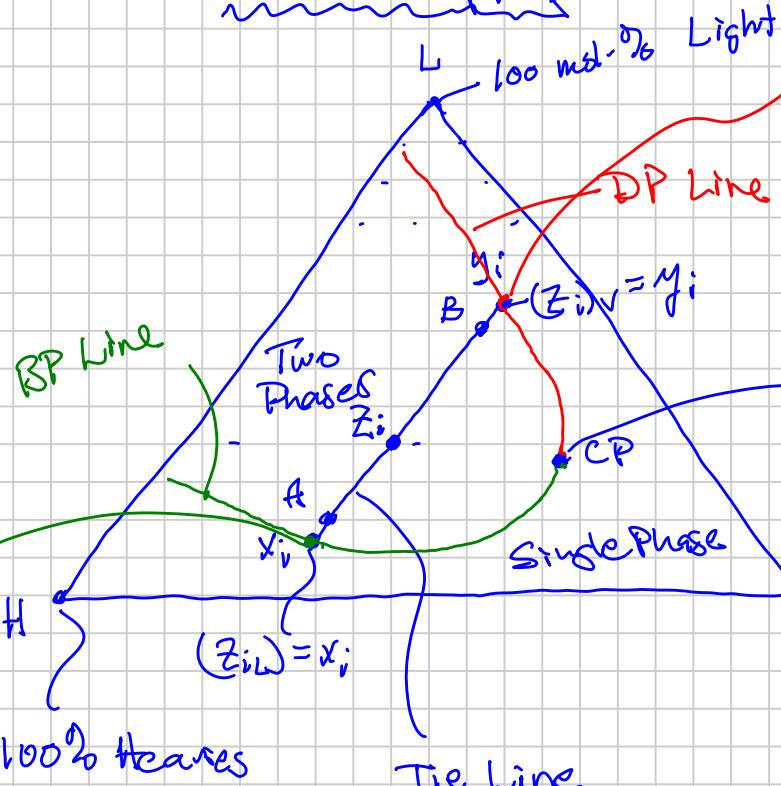
H (heavy)

C<sub>6+</sub>

Applies At a Fixed  $(P^*, T^*)$

$$Z_i = X_i$$

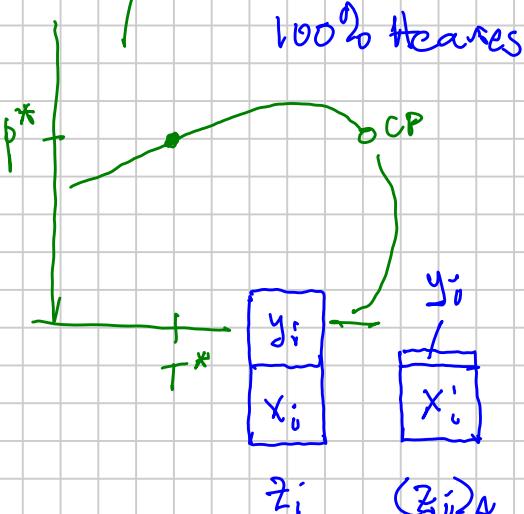
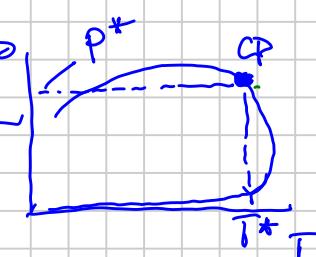
$$Z_i = Y_i$$



$$Z_L \sim 30 \text{ mol\%}$$

$$Z_I \sim 25 \text{ mol\%}$$

$$Z_H \sim 45 \text{ mol\%}$$



Since  $G(y_i) \neq G(x_i) \neq G(Z_i)$

$$P = P_d \\ \text{On Red Line}$$

$$P = P_b \\ \text{On Green Line}$$

Identical  
Chemical Energy  
 $M_t$  and  $M_{iL} = M_{iH}$

$$f_V : 0.4 \quad 0.05 \quad 0.95 \quad 1-e \quad e$$

$$\boxed{Z_i = f_V \cdot y_i + (1-f_V) x_i}$$

$$\frac{n_V}{n}$$

$$\frac{n_L}{n}$$

Tie Line (Lever's Rule) ?

so far:

	II	III
$z_i$		
$C_1$	72 mol-%	$C_2$ 8 mol-%
$N_2$	8	$i$
		$m-C_5$ 1.5
$y_i$		
$C_1$	95	
$N_2$	5	
$x_i$		
$C_1$	1/6	
$N_2$	3	

Violating  
that  
the 3  
(pseudo)  
components  
are  
not the  
same  
 $\downarrow$

Ternary diagram can be very misleading if used Quantitatively.

(Concept of Developed Miscibility)

1986 Arrow Zick

High near 100% recovery  
of oil by an  
Injection Gas

# Pressure-Composition Diagram "( $p-x$ or $p-z$ )"

Used in understanding gas injection effect on oil recovery (Enhanced Oil Recovery, EOR)

$\Rightarrow N_2$

$\Rightarrow CO_2$

$C_1 (+ C_2-C_4)$

$\Rightarrow$  Lean HC gas

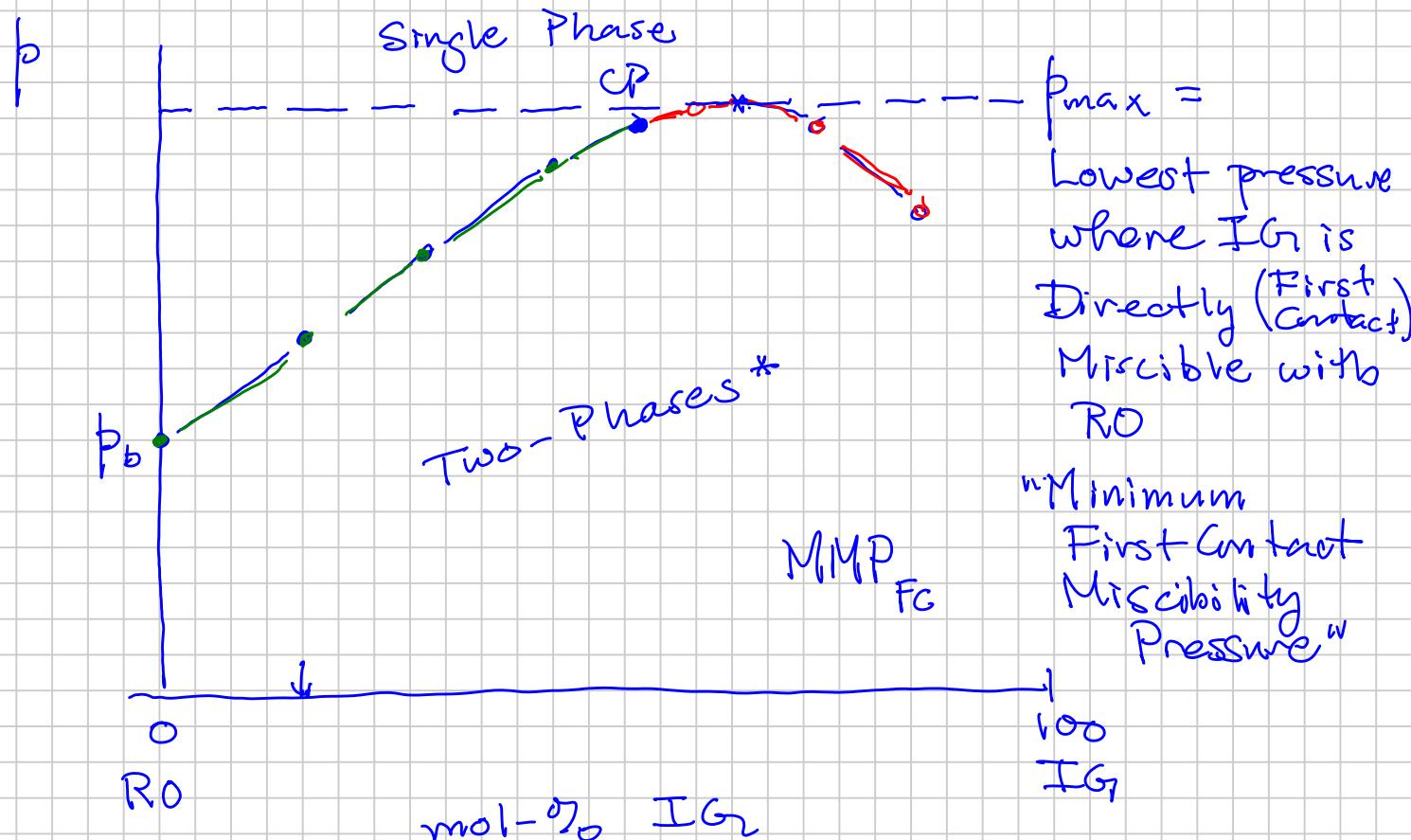
$C_1 (+ C_2-C_4)$

$\Rightarrow$  Separator Gas  
adds

$(C_2-C_4)$

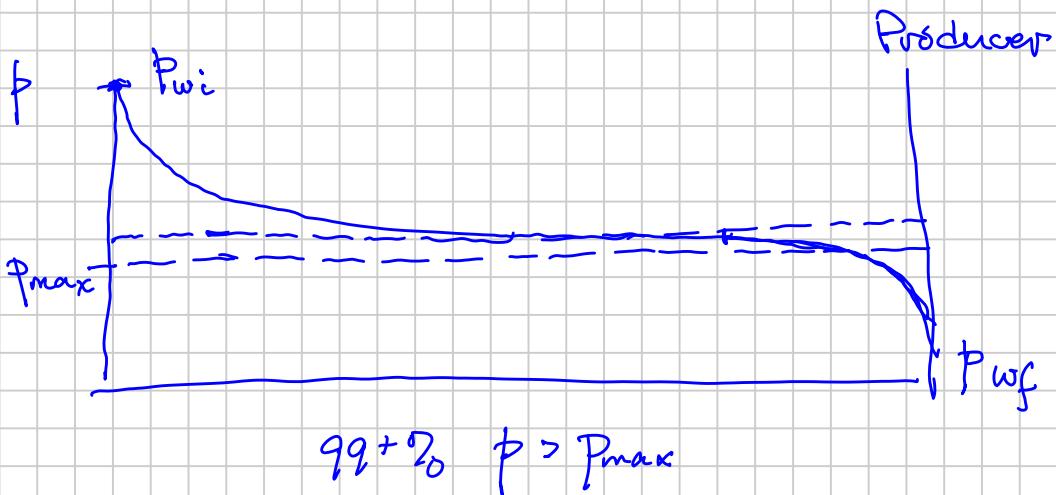
$\Rightarrow$  Enriched Gas

$T_R = \text{const}$



\* Some "local" regions with 3 phases e.g.





Why (how) does nature decide if  $Z_i @ P, T$  is single phase or two (more) phases?

- ① Nature always tries to minimize the system energy.

Chemical energy (Gibbs)  $\mu_i(Z, P, T, v)$

Single Phase :  $\mu_{t1} = \sum n_i \mu_i = n \sum z_i \mu_i(z)$

Two Phases :  $\mu_{t2} = \underline{n_v} \cdot \sum y_i \mu_{iV}(y) + \underline{n_L} \cdot \sum x_i \mu_{iL}(x)$

$\mu_{iV} = \mu_{iL} \quad \left. \right\}$   
 $n = n_V + n_L$

Problem : so many combinations  
 $n_V, n_L, y_i, x_i$

$$\mu_{t1} < \mu_{t2} \Rightarrow \text{Single Phase}$$

$$\mu_{t2} < \mu_{t1} \Rightarrow \text{Two (more) Phases}$$

Gibbs : Simplified method only to identify if single phase or 2(+) phases

$\{ u_i = \text{composition} \}$

$$\mu_t^* = \epsilon \cdot \sum u_i \cdot \mu_i(u) + (1-\epsilon) \sum z_i \cdot \mu_i(z)$$

$$\mu_t^*(u) < \mu_t(z) \Rightarrow 2(t) \text{ phases}$$

$$\mu_i(u) \propto \mu_i(z)$$

$$\frac{\mu_i(u)}{\mu_i(z)} = \text{constant} \quad \text{all } i$$

Challenge to look in a large composition space  
for  $u_i$

### Ch. 3 Calculation of Saturation Pressure (BP, DP)

#### Calculation of Two-Phase Equilibrium

$$z_i @ P, T = n_r n_L y_i x_i$$

All

3.6 : K-values

only  
4.3.1 : Two-Phase Flash

4.5 : Saturation Pressure

Eqs. 4.74-4.75 Only