

# Temperature Effects on Wave Velocities and Compaction of Shales

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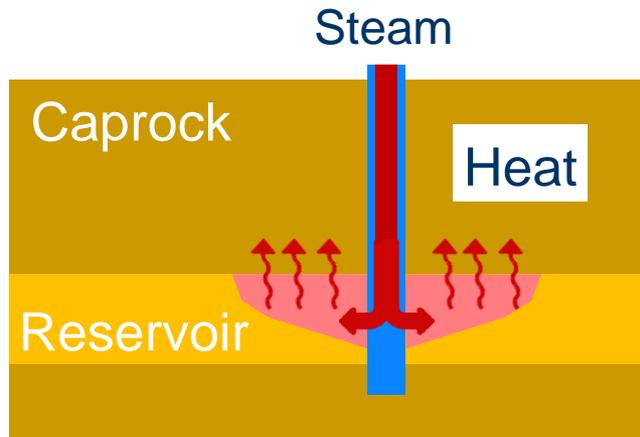


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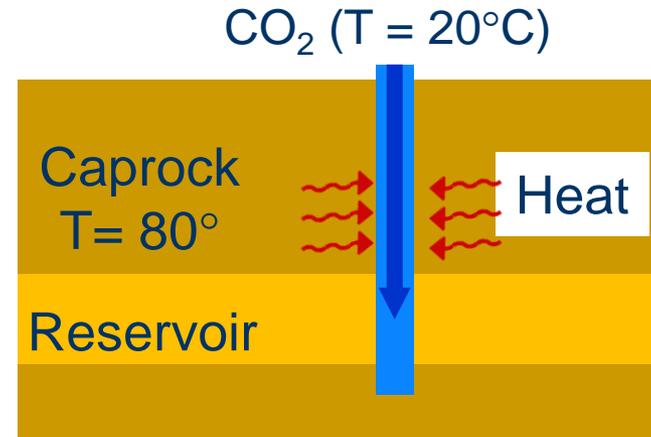
# Why are temperature effects important?

## Thermal EOR



- ⇒ Heating of reservoir
- ⇒ Heat diffusion into caprock
- ⇒ Thermally induced stress (and pore-pressure) changes
- ⇒ Possible risks: fault reactivation, leakage, interface slip

## Fluid injection (e.g. CO<sub>2</sub>)



- ⇒ Temperature difference between injected CO<sub>2</sub> and surrounding formation
- ⇒ Thermally induced pore-pressure and stress changes around injector wells may result in rock failure and leakage of CO<sub>2</sub>

# Why are temperature effects important?

Heating induces:

- **Elastic rock expansion and thermal stresses**

↪ understood; expansion coefficients should be measured with core material

- **Pore pressure increase in low-permeability rocks**

↪ in shales, heat diffusion is faster than pore-pressure diffusion; thermo-poroelasticity established but measurement of coupling coefficients recommended (A. Bauer et al., 2012)

- **Irreversible rock compaction**

↪ Not well understood for shales

← This study

- **Velocity changes**

↪ Not well understood for shales

↪ Understanding important for quantitative interpretation of timelapse seismic

← This study

# Temperature dependence of ultrasonic velocities

- For the temperatures range of interest ( $T < 200^{\circ}\text{C}$ ), the stiffness of rock minerals (quartz) changes only slightly
- If the dry rock does not show any significant temperature dependence the temperature dependence of the saturated-rock stiffness (low-frequency limit) may be described by the Gassmann model:

$$K_{sat} = K_{dry} + \frac{\left(1 - \frac{K_{dry}}{K_{gr}}\right)^2}{\frac{\phi}{K_{fl}(T)} + \frac{(1-\phi)}{K_{gr}} - \frac{K_{dry}}{K_{gr}^2}} ; G_{sat} = G_{dry}$$

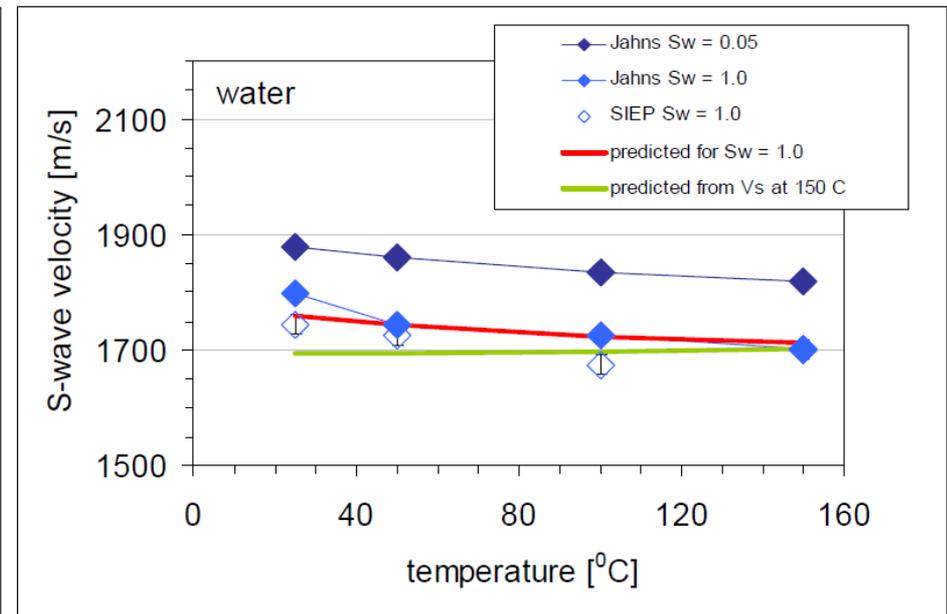
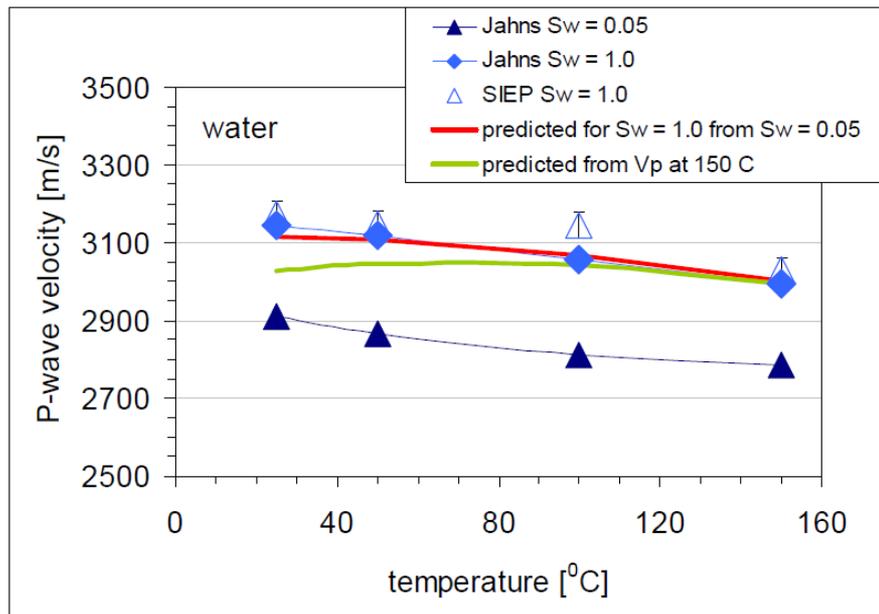
$K_{sat}$ : Bulk modulus of saturated rock  
 $K_{dry}$ : Bulk modulus of rock frame  
 $K_{gr}$ : Bulk modulus of grains  
 $K_{fl}$ : Fluid modulus  
 $G_{sat}$ : Shear modulus of saturated rock  
 $G_{dry}$ : Shear modulus of rock frame  
 $\phi$ : Porosity  
 $\rho$ : Density of saturated rock

- Velocities are given by:

$$V_p(T) = \sqrt{\frac{K_{sat}(T) + \frac{4}{3}G_{sat}(T)}{\rho(T)}} ; V_s(T) = \sqrt{\frac{G_{sat}(T)}{\rho(T)}}$$

# Temperature dependence of ultrasonic velocities

- For many rocks, deviations from the Gassmann model were observed for both  $V_p$  and  $V_s$ .
- For water-saturated Castlegate sandstone, it was shown the Gassmann model provides a good description if the temperature dependence of the dynamic rock stiffness for a small but non-vanishing water saturation is taken as "dry-rock" stiffness (drained-rock stiffness)

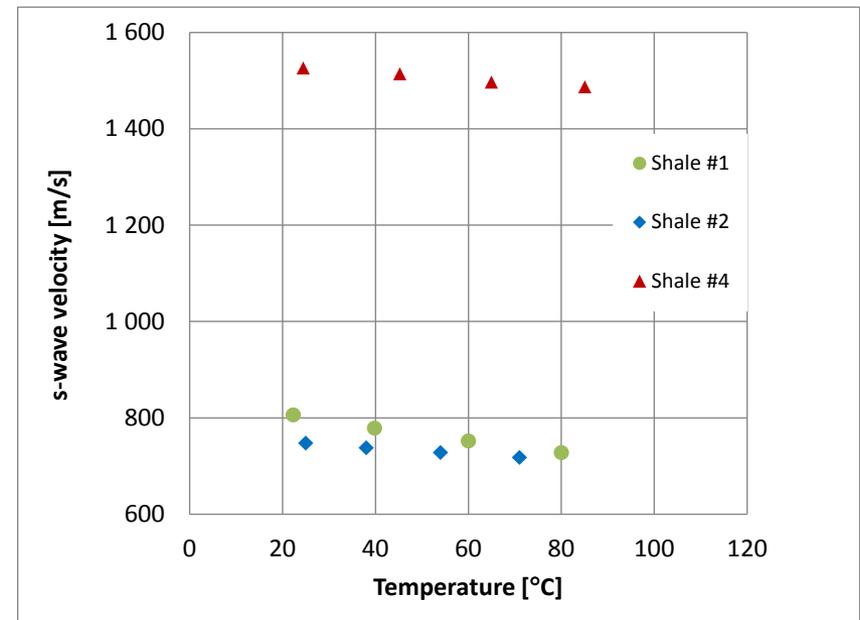
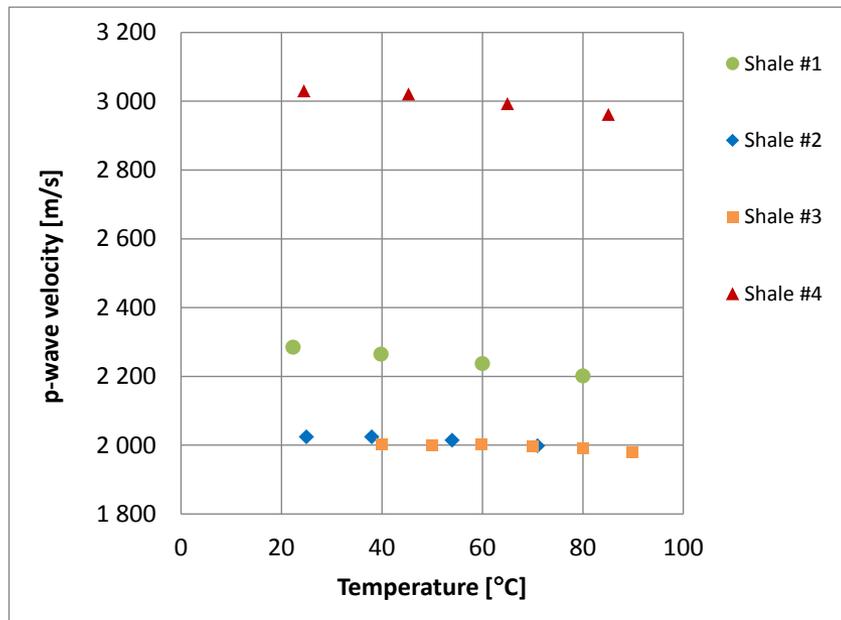


Bauer et al., Euroconference 2011

# Temperature dependence of ultrasonic velocities in shales

Core-plug measurements with subsurface shales covering a wide range of depths, porosity, and clay content:

Shale	Age	Depth [mTVD]	Porosity [%]	Clay cont. [wt%]
#1	Paleocene	2620	32	84
#2	Upper Miocene	1730	40	42
#3	Miocene	1750	53	40
#4	Upper Jurrasic	2390	12	73

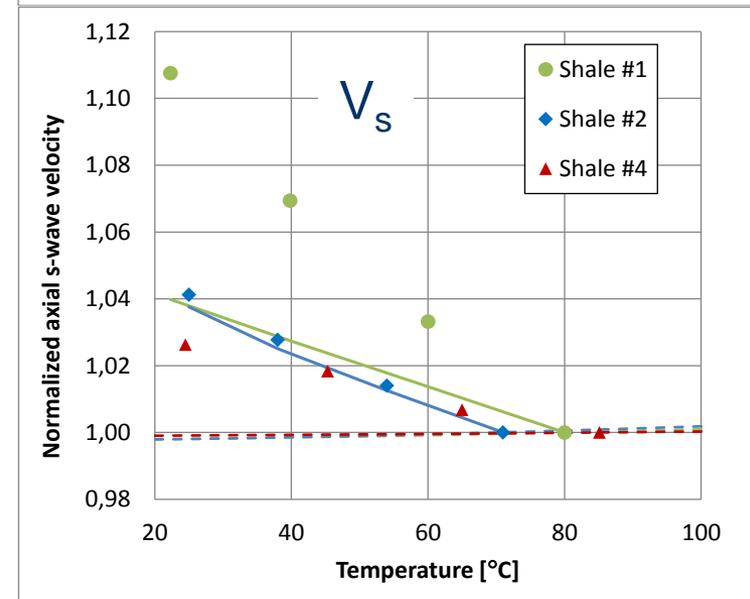
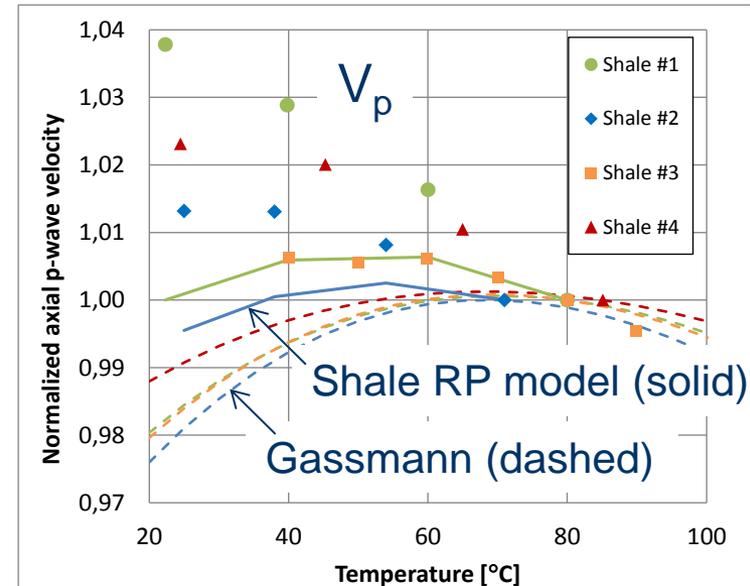
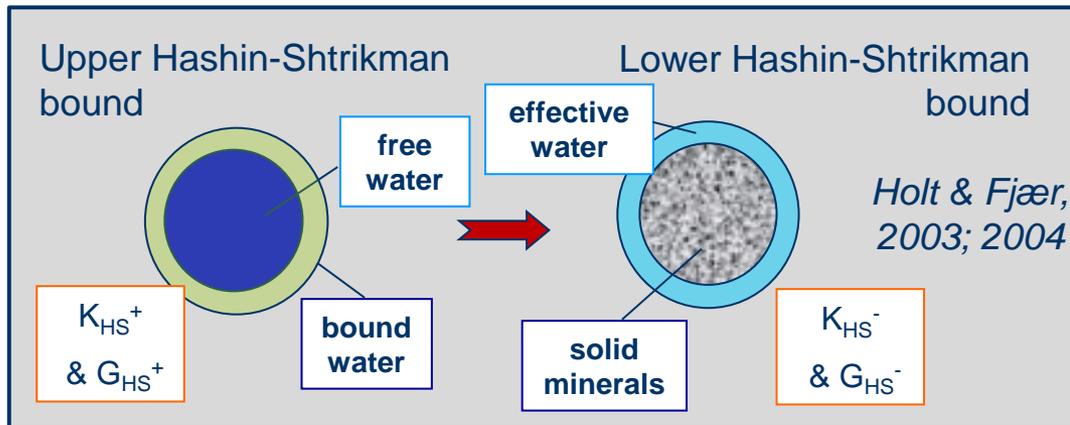


# Temperature dependence of ultrasonic velocities in shales

Gassmann model with temperature-independent dry-rock moduli:

- ↪ Strong deviation from experimental data
- ↪ Gassmann model does not take bound water into account

SINTEF's Shale rock physics (RP) model accounts for bound water. Temperature sensitivity of the bound-water stiffness is not known; assume same sensitivity as that of ice ⇒ trend in the right direction, still strong deviations



# Temperature dependence of ultrasonic velocities in shales

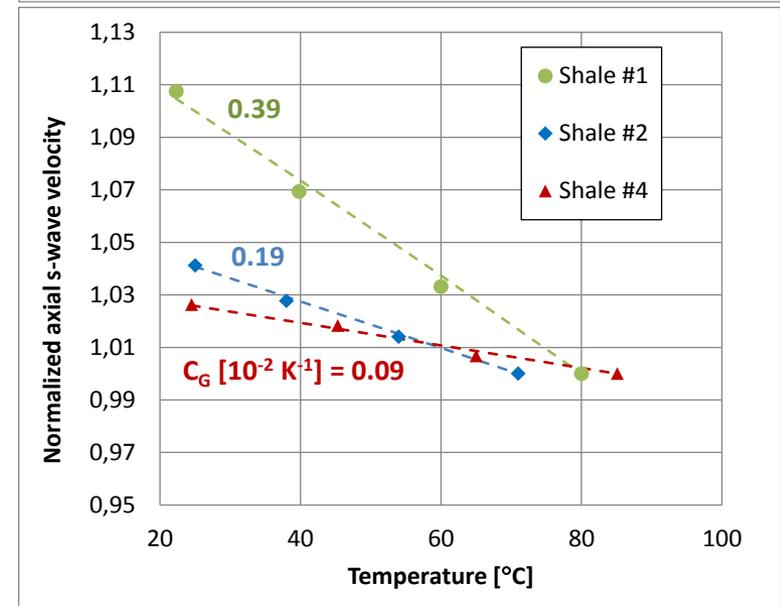
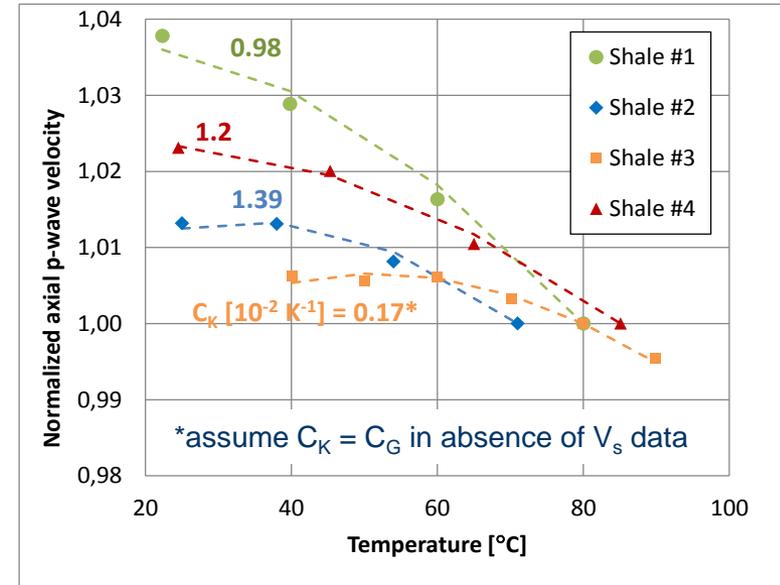
## Emperical approach:

Apply Gassmann model and assume linear temperature dependences of drained-rock moduli:

$$K_{dry} = K_{dry,0} (1 - C_K \cdot \Delta T)$$

$$G_{dry} = G_{dry,0} (1 - C_G \cdot \Delta T)$$

- ↪ Good fit of experimental data for  $C_K \approx 1.0 - 1.4 \cdot 10^{-2} \text{ K}^{-1}$ , and  $C_G \approx 0.1 - 0.4 \cdot 10^{-2} \text{ K}^{-1}$ .
- ↪ Bound-water effects, fluid-rock interaction, etc. included in drained-rock modulus.



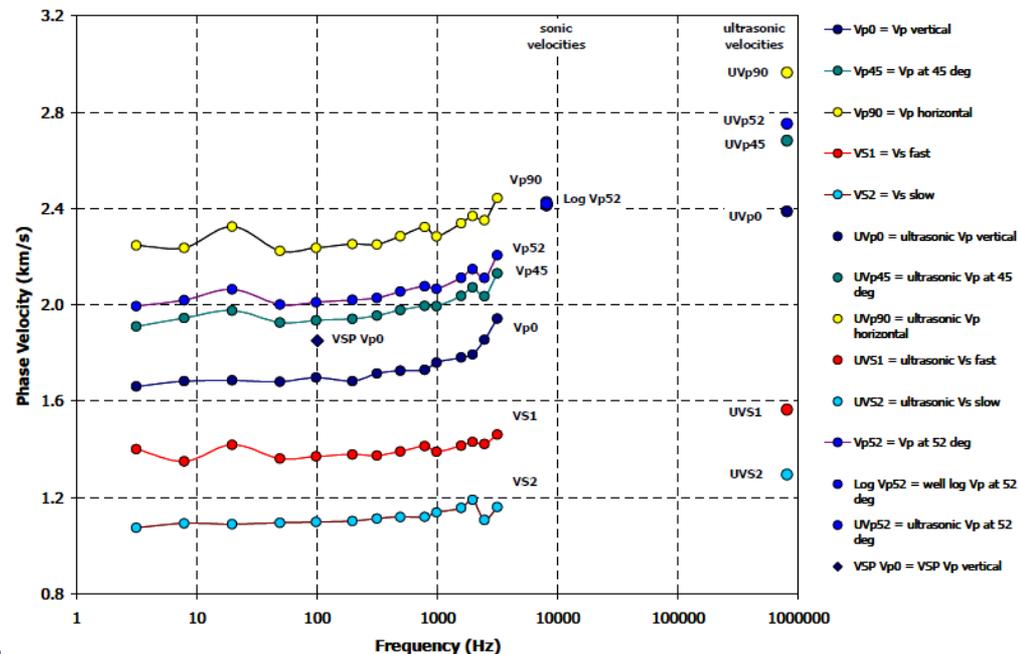
# Temperature dependence of shale velocities – Dispersion effects

Is the temperature dependence of ultrasonic velocities the same as that of sonic and seismic velocities?

↪ There is evidence for relatively large velocity dispersion in shales

↪ It is likely that velocity dispersion is temperature dependent (previous compaction tests have shown smaller temperature dependence of static stiffness as compared to dynamic drained-rock stiffness)

↪ **Need for temperature-dependent dispersion measurements**



Duranti, Ewy, Hofmann (2006)

# Thermally induced compaction of shales

Project work at NTNU Fall 2012 by Leni Marøyen

w/ assistance from Eyvind F Sønstebo, Olav-Magnar Nes, Liang Wang (SINTEF Energy),  
Andreas Bauer & Rune M Holt

## Motivation

- Significant contraction has been observed at elevated temperature (< 100°C) in previous shale experiments at SINTEF – artefact or reality?
- Thermally induced compaction could have significant impact on caprock integrity and wellbore stability

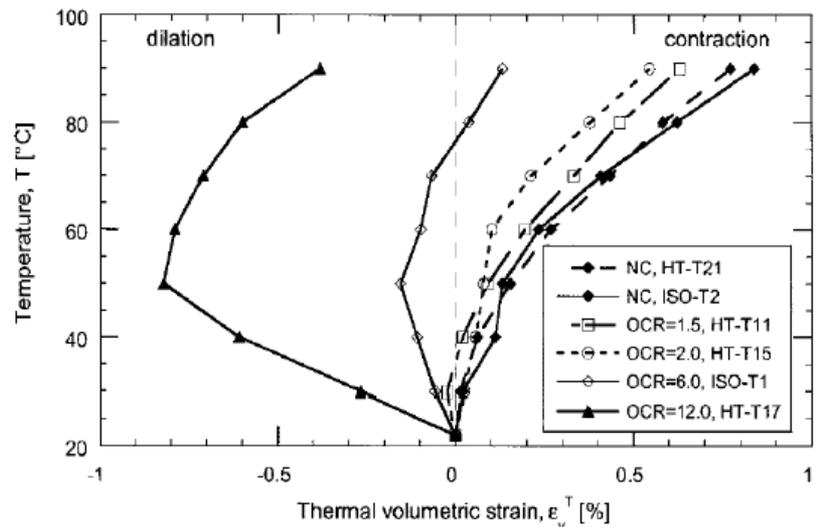
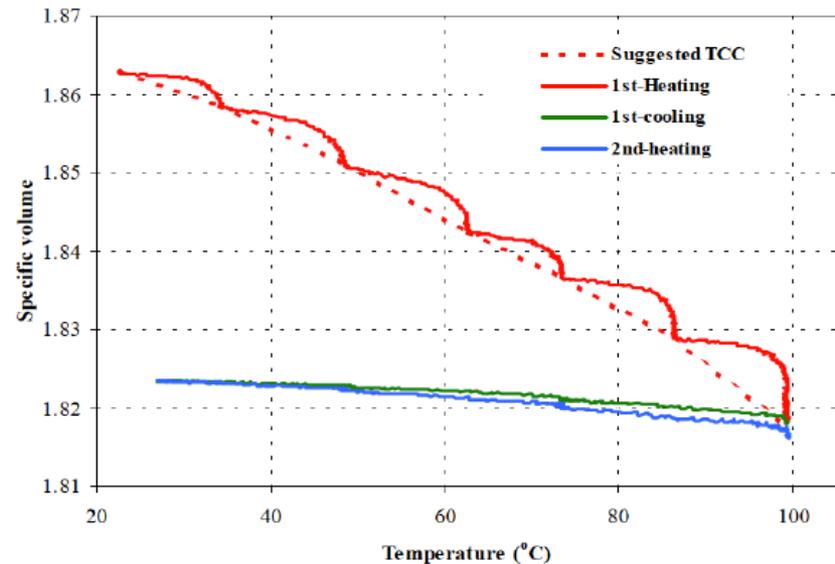
# Thermally induced compaction of shales

## Literature study

Thermal compaction of reconstituted clay (Ghahremannejad, 2003): Largely plastic behaviour during initial heating, elastic behaviour during cooling and reheating

Stress history dependent thermal behaviour of kaolin clay during heating; initial consolidation at 0.6 MPa (Cekerevac et al., 2004)

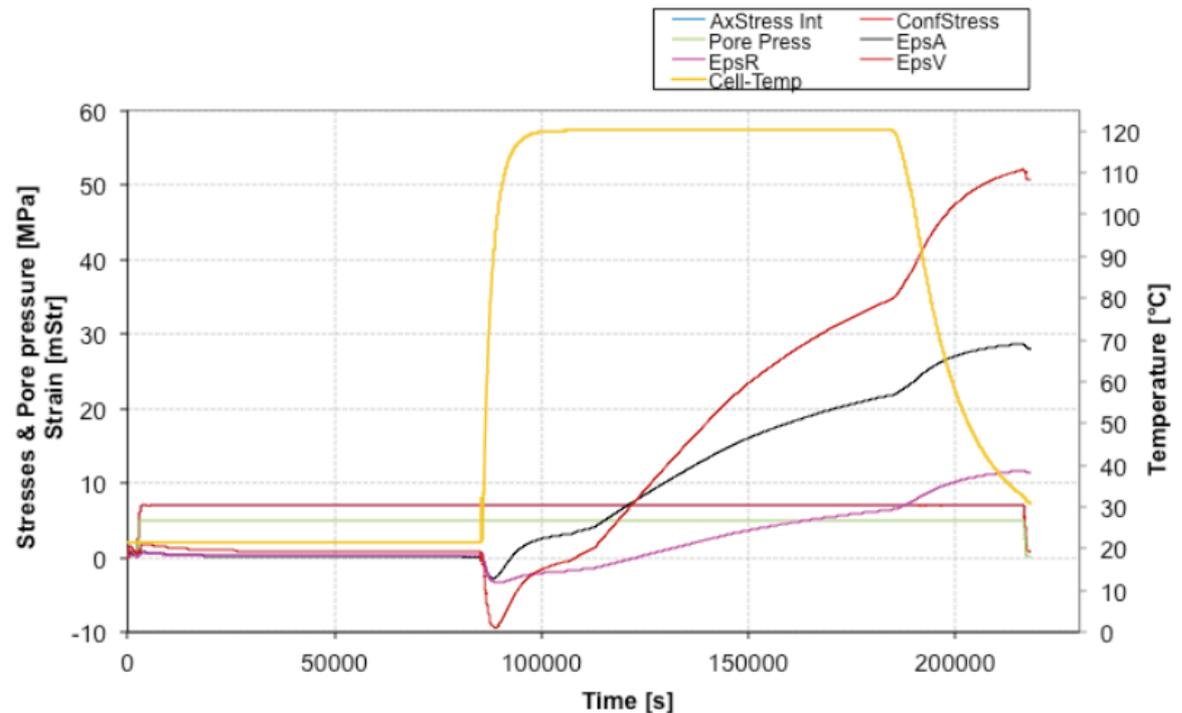
Normally consolidated samples show contraction; heavily overconsolidated samples show dilatancy.



# Thermally induced compaction of Pierre shale

## Experimental observations

Drained heating of Pierre Shale @ 7 MPa (isotropic) external stress & 5 MPa pore pressure within the SMASH apparatus

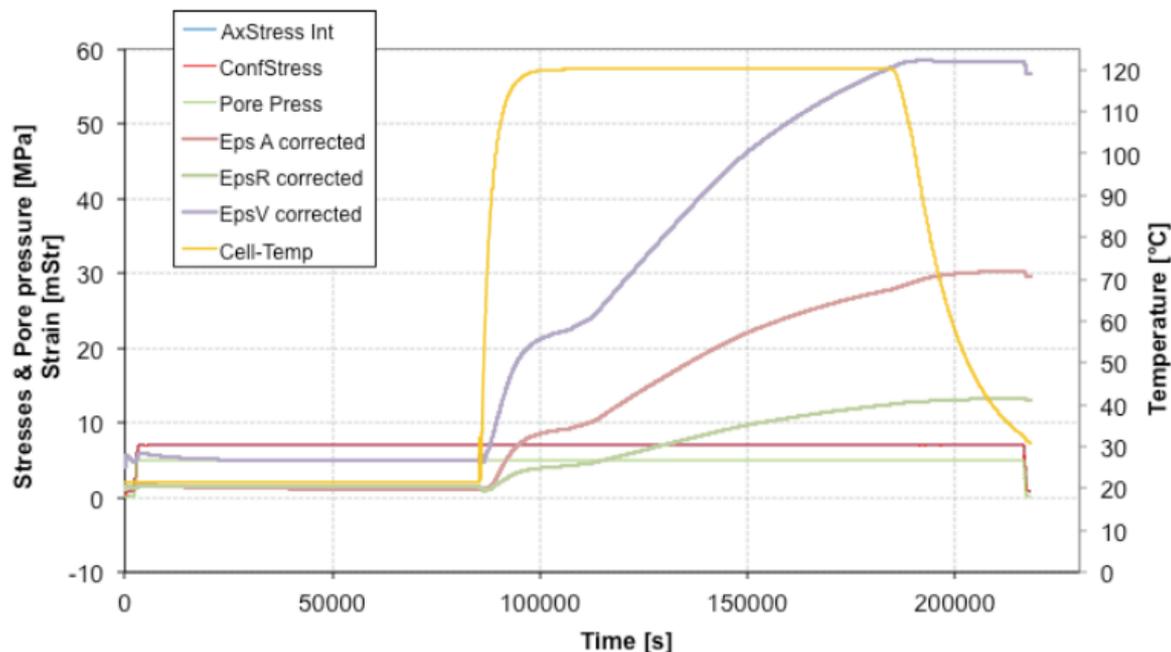


Upon heating, the sample expands, followed by time-dependent irreversible compaction

# Thermally induced compaction of Pierre shale

## Experimental observations

Strain data corrected with the thermal expansion coefficient, estimated from the cooling stages (when elastic behaviour can be assumed) ( $\alpha_{T,\text{vol}} = 19 \cdot 10^{-5} \text{ }^\circ\text{C}^{-1}$ )



Significant contraction takes place as non-elastic creep.

**The volumetric strain corresponds to porosity reduction from 19 to 14 %!**

# Thermally induced compaction of Pierre shale

## P-Wave Velocity

- Strong velocity increase associated with thermally induced compaction
- Velocity drops during initial heating
- Significant velocity decrease at 120 °C indicates loss of "cementation"



SINTEF's Shale Rock Physics model: Choosing  $K_{bw}=3$  &  $G_{bw} = 2.5$  GPa,  $v_p$  (at room temperature) is estimated to 2383 m/s ( $v_s=1024$  m/s) for 19 % porosity Pierre Shale  
Reducing porosity to 14 % (as at 120 °C),  $v_p$  increases to 2708 m/s (without changing  $K_{bw}$  &  $G_{bw}$ )

# Conclusions

## Thermal Rock Physics of Shales

- Relatively strong reduction of  $V_p$  and  $V_s$  with temperature (in the absence of thermally-induced compaction)
- Temperature dependence can be described by Gassmann theory by assuming a temperature-dependent drained-rock stiffness accounting for bound-water effects and rock-fluid interaction; better understanding needed
- Not clear if sonic and seismic velocity show same temperature dependence as ultrasonic velocities; need for velocity-dispersion measurements

## Thermally-induced compaction of shale

- Significant thermally-induced compaction observed during heating of shale core plugs
- Not clear to what degree thermally-induced compaction would occur in the subsurface; might have significant impact on caprock integrity and wellbore stability; better understanding and more systematic studies needed.