



Department of Petroleum Engineering
and Applied Geophysics

Universal Temperature Profile in Pipe Flow

TPG 4515 Petroleum Production Specialization Course

Torbjørn Gjellesvik

Trondheim

December 1st, 2011

Identifying the problem

- The universal temperature profile encompasses temperature changes in pipe flow.
 - Formation of solids in pipelines depends on temperature (and pressure).
 - Knowledge about radial temperature change is extremely useful in order to know what to expect, taking appropriate measures to avoid formation of solids and awareness of pipeline conditions.
-

Agenda

- ▣ What is the Universal Temperature Profile
 - ▣ Petroleum Production Case Examples
 - ▣ Simple Sensitivity Analysis
 - ▣ Discussion
 - ▣ Comments on Used Method
 - ▣ Conclusion
-

The Universal Temperature Profile

- Temperature profile from pipe wall, through viscous sub-layer, buffer layer to the turbulent core.
 - Effect of outside cooling.
 - Pipeline wall heat transfer.
 - Effect of fluid and flow conditions.
 - Where, and by how much, does the change happen?
-

Methods Used

1st Step:

- Obtain inner pipe wall temperature, T_{vi} , through modification of Fourier's Law.

2nd Step:

- Construct radial pipeline temperature profile.
- Converts temperature (and distance) to dimensionless terms.

Viscous sub-layer:

$$T^+ = T_v^+ + \text{Pr } y^+$$

Buffer layer:

$$T^+ = T_v^+ + \left[5 \text{Pr} + 5 \ln(0,2 \text{Pr } y^+ + 1 - \text{Pr}) \right]$$

Turbulent core:

$$T^+ = T_v^+ + \left[5 \text{Pr} + 5 \ln(1 + 5 \text{Pr}) \right] + 2,5 \ln\left(\frac{y^+}{30}\right)$$

(J.S. Gudmundsson, 2011)

Case Examples

■ FLUIDS:

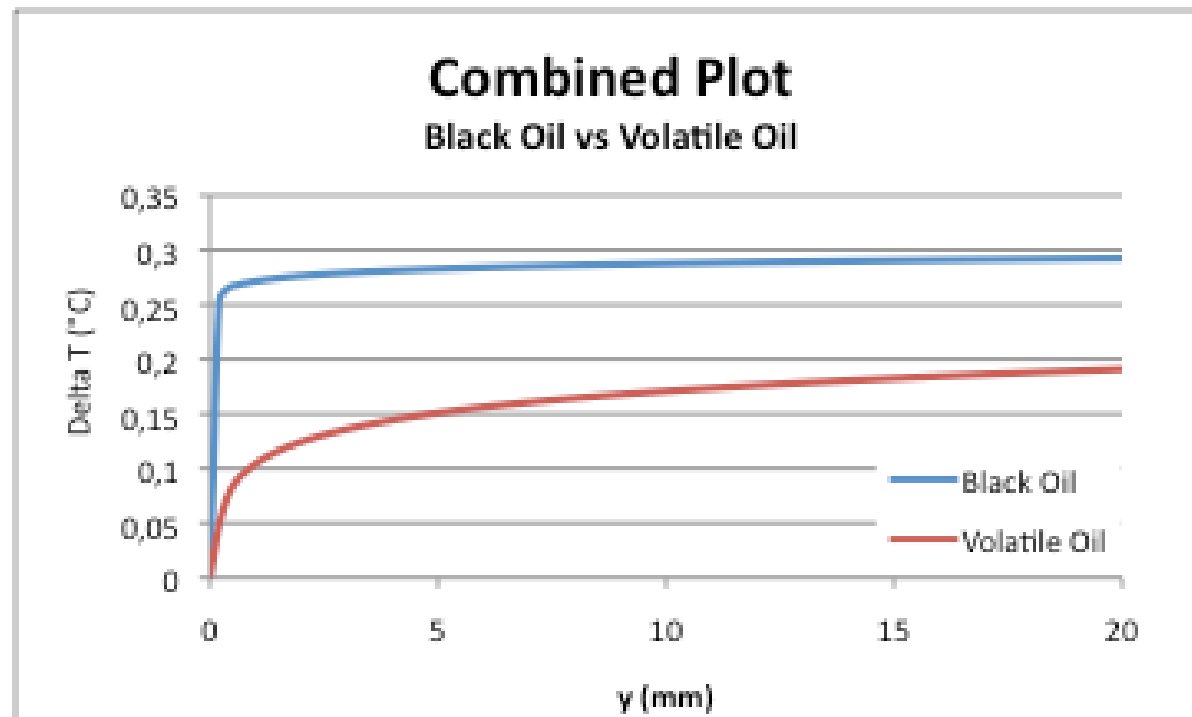
- Black Oil and Volatile Oil
(HYSYS compositions, TPG 4135 Processing of Petroleum, 2011)
- Shtokman Natural Gas
(Translang Tech., year unknown)
- Ormen Lange Natural Gas
(Heskestad, 2004)

- Fluid properties are obtained from HYSYS under assumed reasonable pressure and temperature conditions.
-

General Assumptions

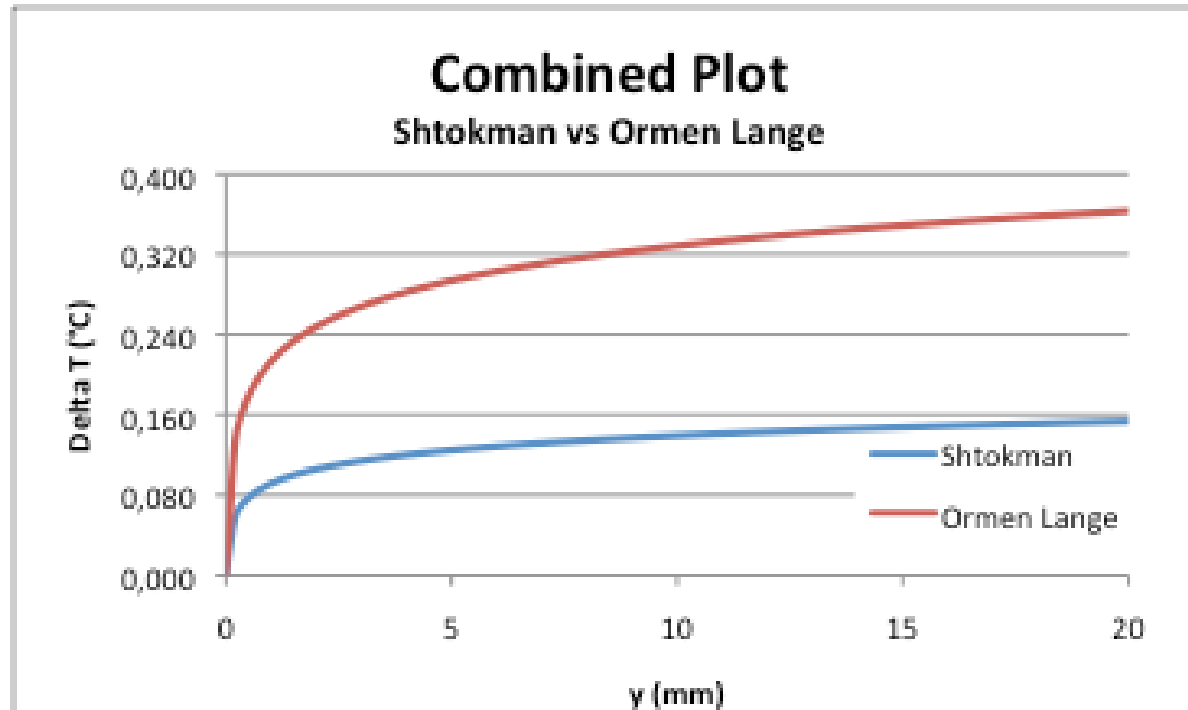
- STEADY STATE.
- PIPE:
 - Dimensions (12" ID)
 - Heat Transfer Coefficient, U (20 W/m² K)
 - Thermal Conductivity, k_{pipe} (40 W/m K)
- For not insulated carbon steel pipe.
 - Pipe Roughness (35,1 μm)
- CONDITIONS:
 - Ambient and Inlet Temperature ($^{\circ}\text{C}$)
 - Pressure (Pa)
- BULK:
 - Velocity (2 m/s for oils, 30m/s for gas)

Black Oil vs. Volatile Oil



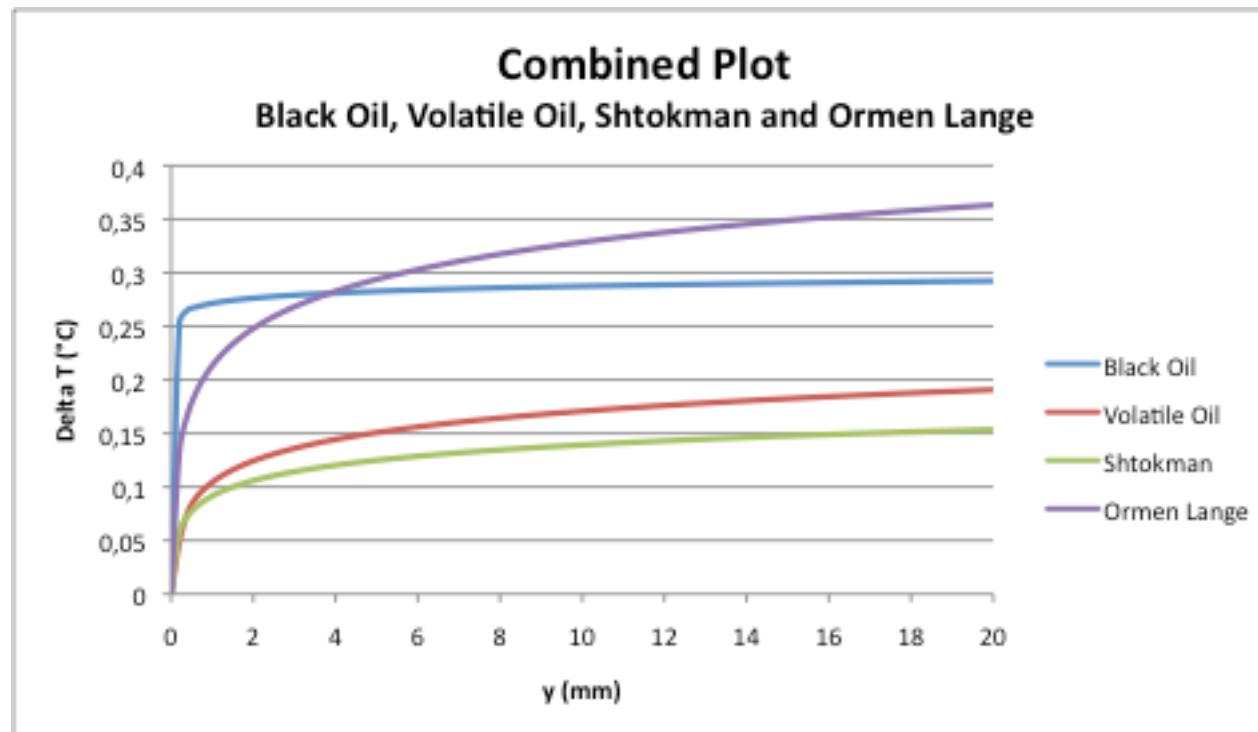
- Conditions: 20°C & 80 bara.
- Thicker boundary layer for black oil.
- Noticeable temperature change in turbulent core. Even more so for volatile oil. 82% and 25% change in the viscous sub-layer for black- and volatile oil, respectively.

Shtokman vs. Ormen Lange



- Shtokman: 40°C & 100 bara.
Ormen Lange: 80°C & 100 bara.
- Extremely thin sub- and buffer layer.
- Temperature change within these two layers is still 36% and 35% for Shtokman and Ormen Lange, respectively.

Oil vs. Natural Gas



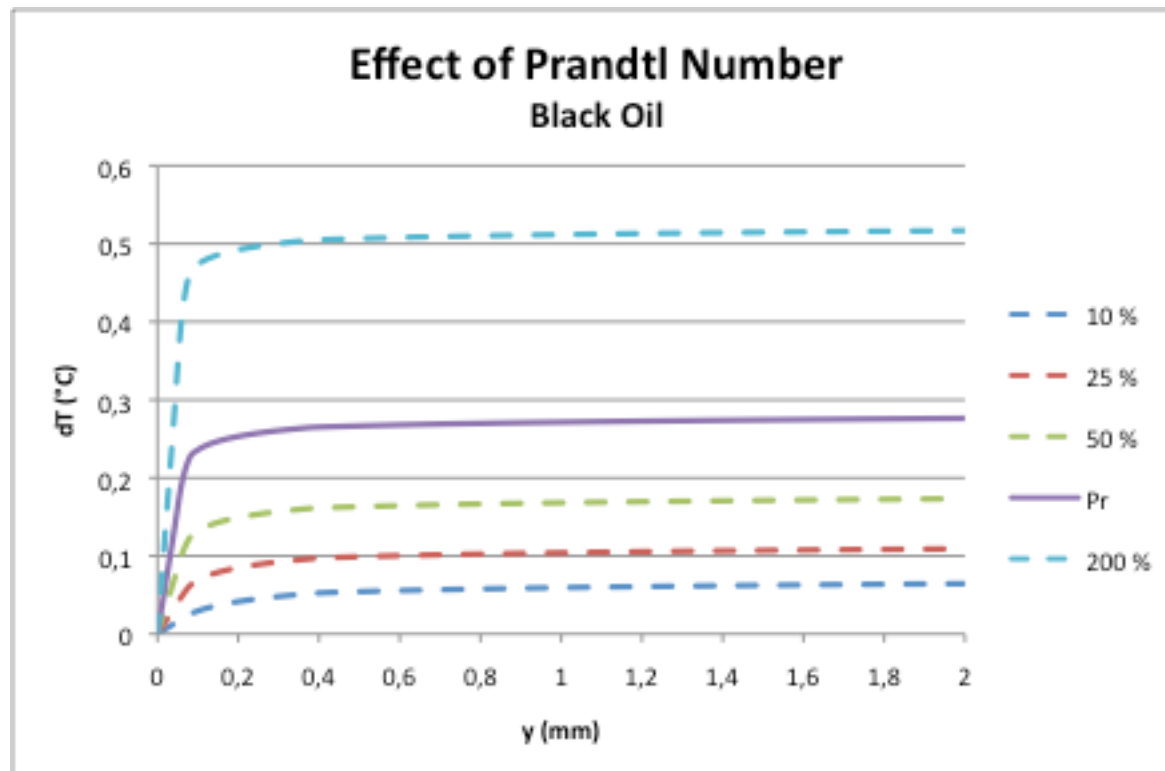
- Shape of curve is very dependent on Pr number.
- Black oil has very high Pr number, giving it a distinct shape compared to the other fluids. $Pr_{BO} \gg PR_{VO,G}$

Simple Sensitivity Analysis

- Investigate the sensitivity of certain parameters and their effect on the radial temperature profile.
- Pr number shown to have significant effect.
 - Heat capacity and viscosity varies most between the fluids.
- Unchangeable parameters:
 - Heat Capacity
 - Viscosity
 - Thermal conductivity of fluid.
- Changeable parameters:
 - Heat Transfer Coefficient
 - Fluid Velocity

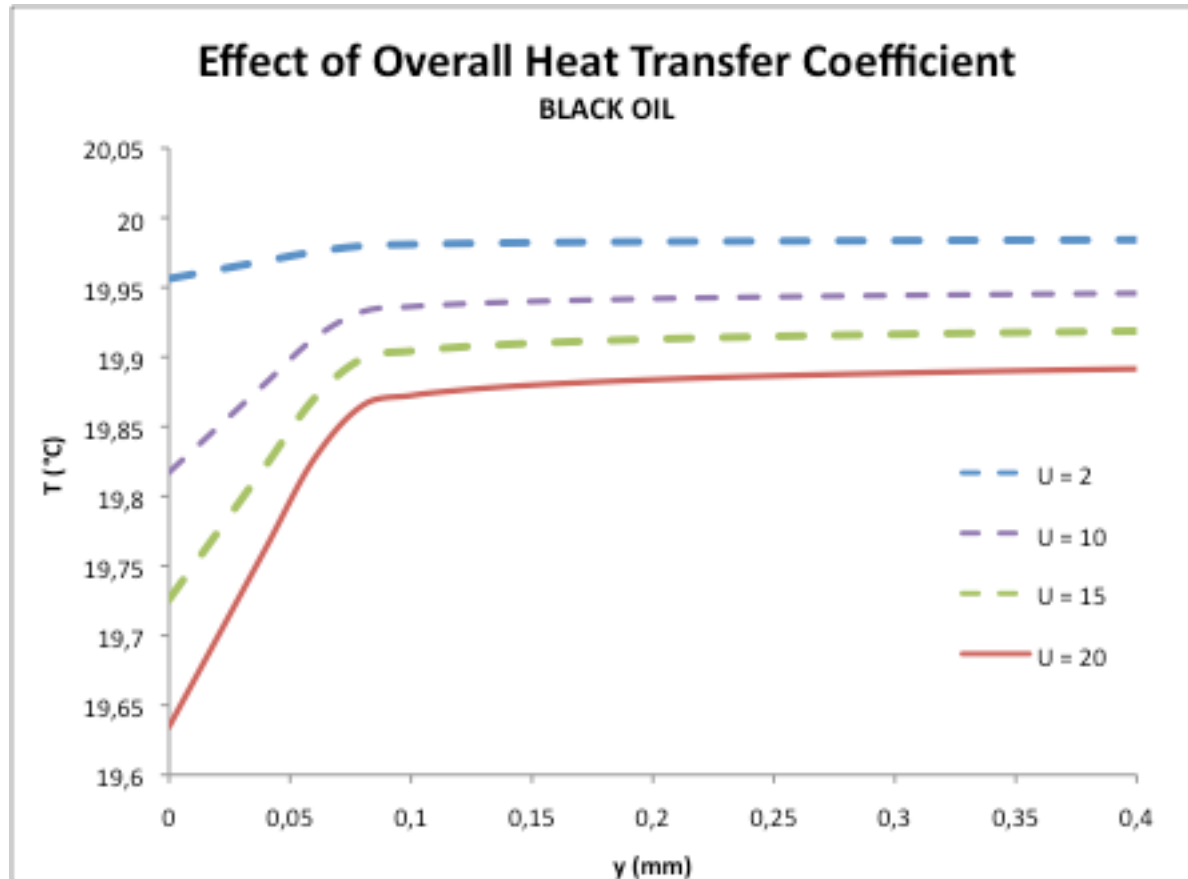
$$\text{Pr} = \frac{C_p \mu}{k}$$

Simple Sensitivity Analysis



- Sharper transition into turbulent core. Higher dT as Pr decreases.

Simple Sensitivity Analysis



- The more insulation, the less temperature drop at the wall.
- Insulated pipelines have low heat transfer coefficients.

Discussion

- The calculations have been performed using a combination of real data, simulated data and assumed data.
 - Actual numbers may not be reliable because they are subject to a high degree of uncertainty.
 - Shape of profile, trends and the sensitive parameters is perhaps the most valuable and reliable information that can be extracted from this work.

- Helpful in identifying solid deposition “danger-zones”.
 - Wax, hydrates are more likely to start forming at the wall as the issues arise as temperature drops.

- Based on available data and model requirements the results are thought to be reasonable, keeping the uncertainties in mind.
 - Variations imposed by considering different fluids seem valid.

- Method used corresponds to what is described in “Fluid Mechanics & Transfer Processes” by Kay & Nedderman (1985), although from different reference points.
 - Kay & Nedderman → From turbulent core to pipe wall.
 - J.S. Gudmundsson → From pipe wall to turbulent core.
 - Model as described by Sippola is similar, but not closely considered in this work.

Conclusion

- Shape of temperature profile very much dependent on Prandtl number.

- Heat Capacity
- Viscosity
- Fluid Thermal Conductivity

$$\text{Pr} = \frac{C_p \mu}{k}$$

- Boundary layer is thicker for more viscous fluids.
- Relative radial temperature change is generally small.
- Most of the temperature change happens within the first few millimetres (oil) and centimetres (gas).
- Probability of solid formation is greater at the wall due to lower temperature.

References

- “Pipeline Wall Heat Transfer”, J.S. Gudmundsson, “Flow Assurance” Manuscript, NTNU, 2011.
- “Boundary Layer Temperature Profile”, J.S. Gudmundsson, “Flow Assurance” Manuscript, NTNU, 2011.
- “Fluid Mechanics and Transfer Processes”, J.M. Kay & R.M. Nedderman, 1985.
- “Particle Deposition in Ventilation Ducts”, M.R. Sippola, UC Berkeley, 2002.
- Black Oil, HYSYS Stream file, Pedersen et al, 1989.
- Volatile Oil, HYSYS Stream file, Pedersen et al, 1989.
- Shtokman gas composition, PowerPoint presentation, Translang Tech., year unknown.
- Ormen Lange as composition, Deposits Detection Using Pressure Pulse Technology, K.L. Heskestad, NTNU, 2004.