

# MULTI-POINT WELL TEST FOR GAS WELLS

Note Title

2014-11-06

$$q_g = \frac{kh (P_{PR} - P_{pwf})}{TR \left[ \underbrace{\left( \ln \frac{r_e}{r_w} - \frac{3}{4} \right)}_{7-10} + \underbrace{s + Dq_g}_{\text{Total Skin}} \right]}$$

$$\underbrace{B q_g^2}_{\text{Unknown}} + A q_g - (P_{PR} - P_{pwf}) = 0$$

B (D ; β) :

$$Re = \frac{\rho v d}{\mu} \approx 1 \Rightarrow B$$

r, v, μ

$$v \propto \frac{1}{r}$$

Radial flow  
near the  
wellbore

$$D q_g \sim 1 - 100$$

BUT

need "high"

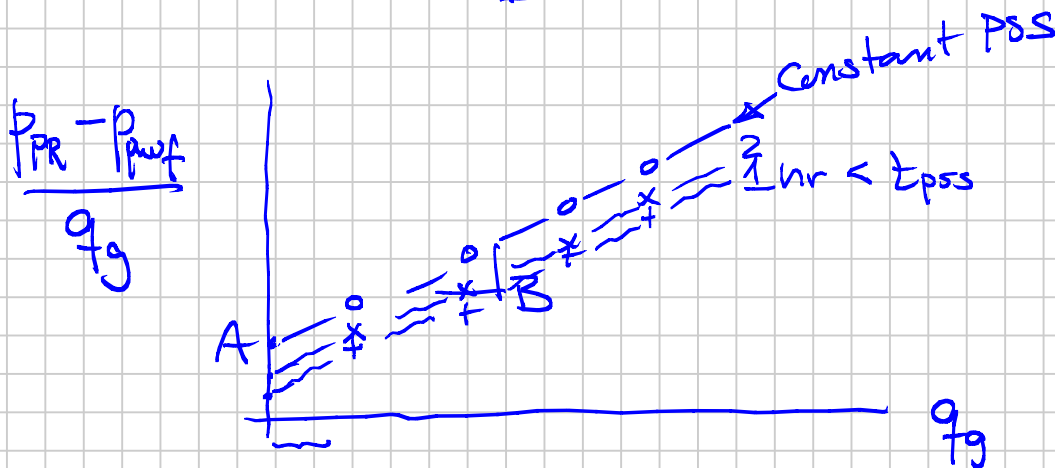
$$q_g = 5 - 50 \text{ MMscf/d}$$

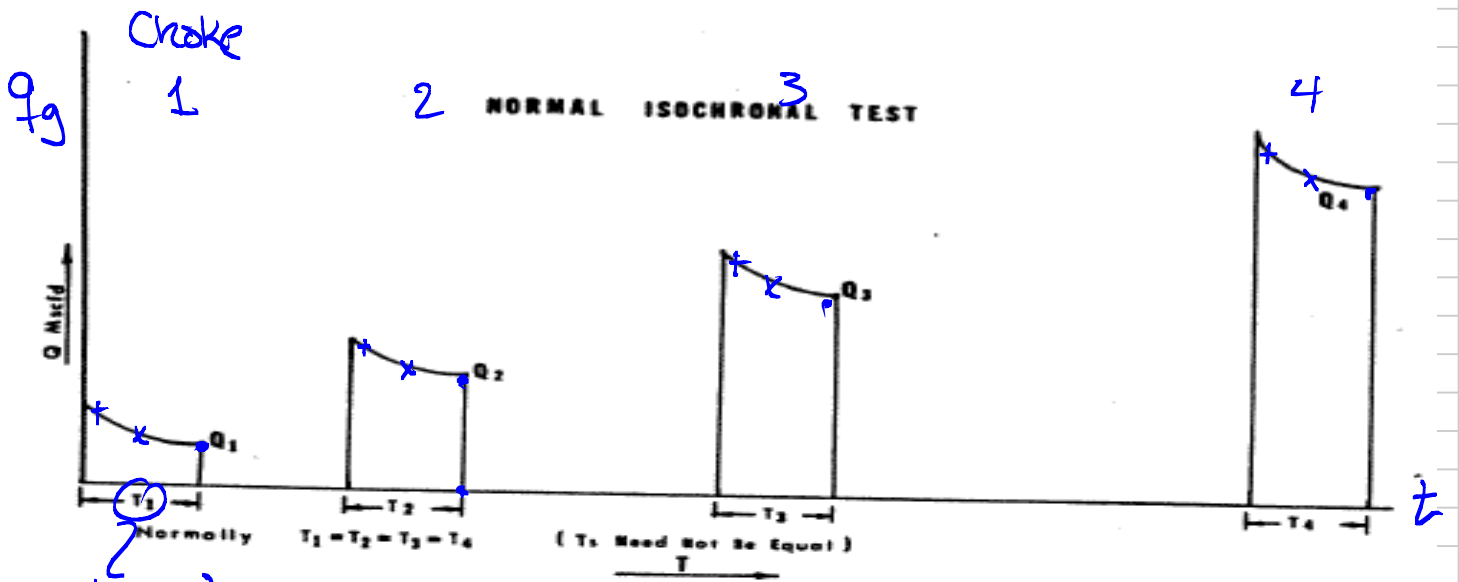
$$\approx 0.1 - 1 \cdot 10^6$$

$$\text{Sm}^3/\text{d}$$

$$v = \frac{q_g \cdot B_g}{A_L}$$

$$A_L = 2\pi r h$$





$\Delta t_g > t_{pss}$

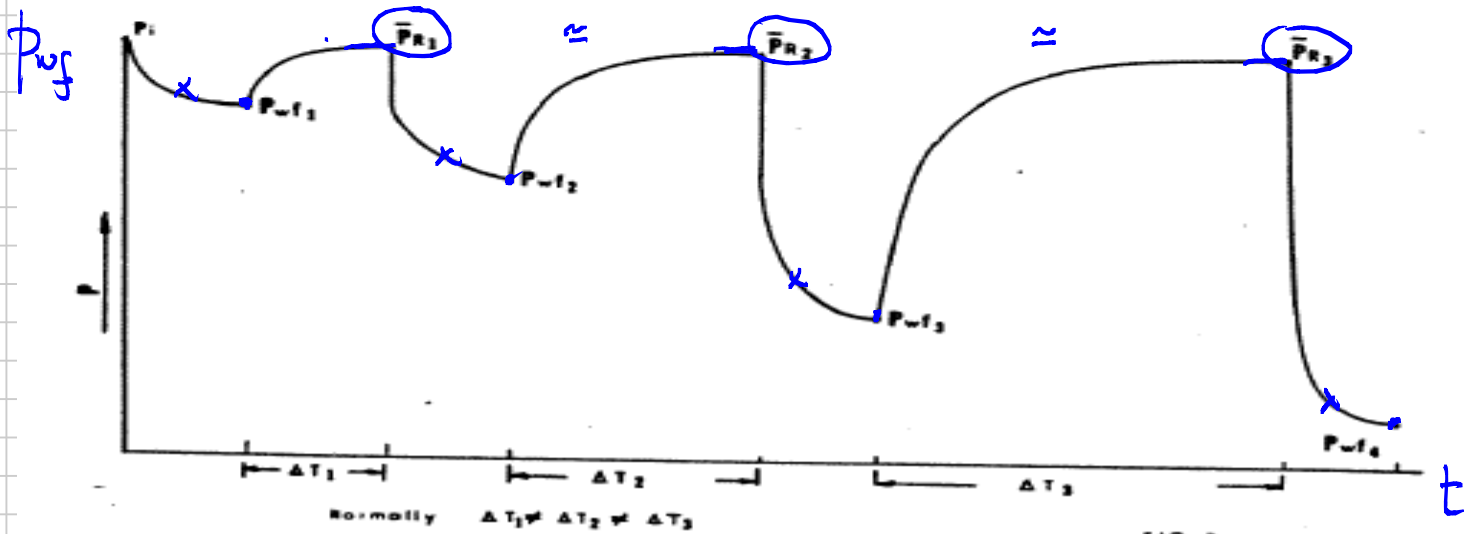
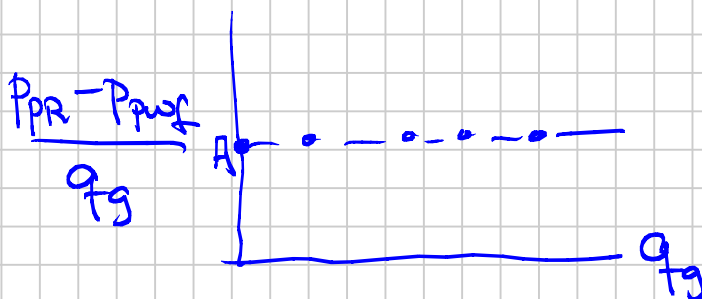


FIG. 3

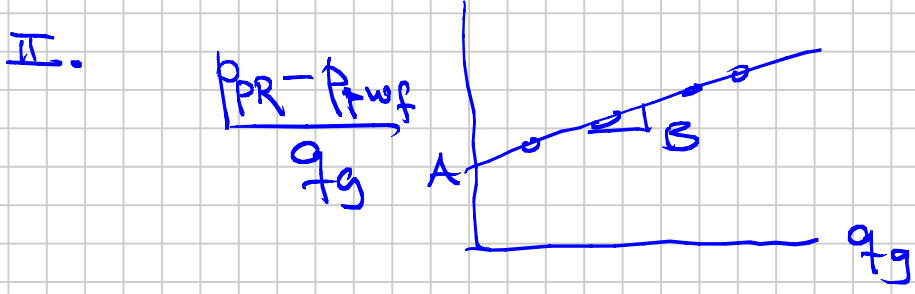
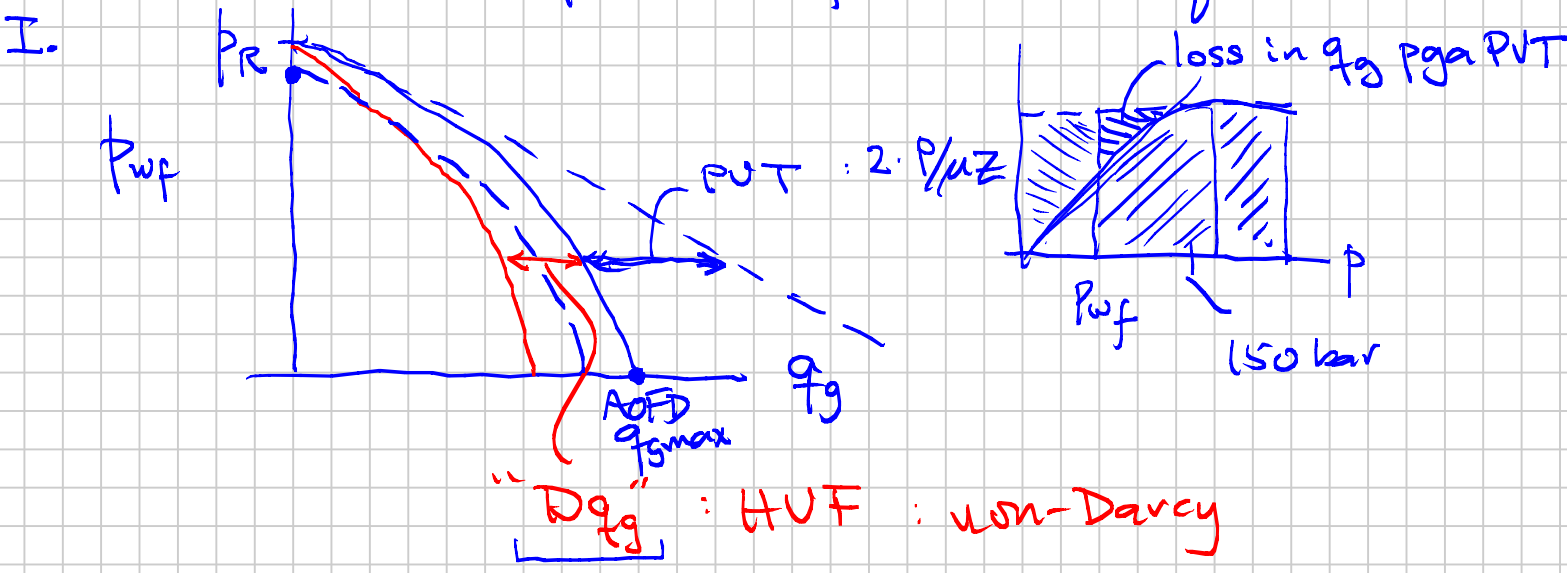
$$A(t) = \frac{T_R}{Kh} \left[ \underbrace{p_D(t_0)} + s \right] \quad t < t_{pss}$$

$$\frac{1}{2} [ln(t_0 + 0.809)]$$

If  $Bq_g \ll Aq_g$  : Darcy

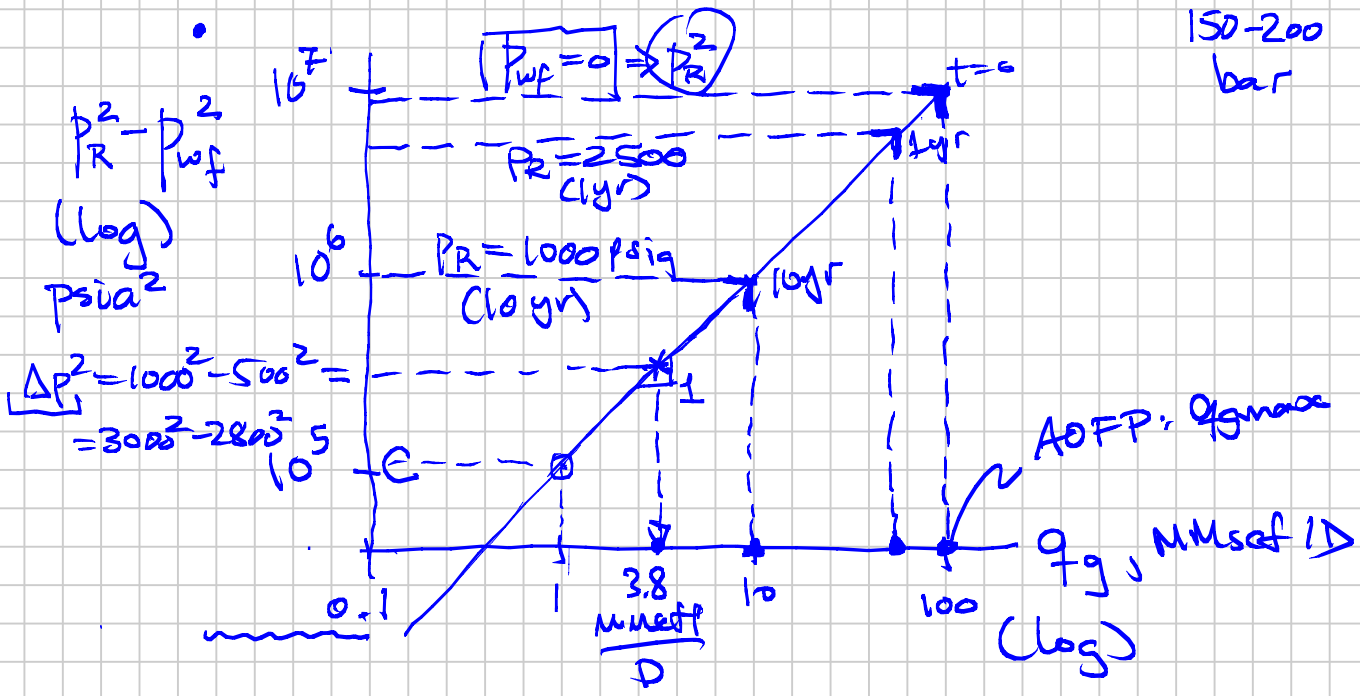
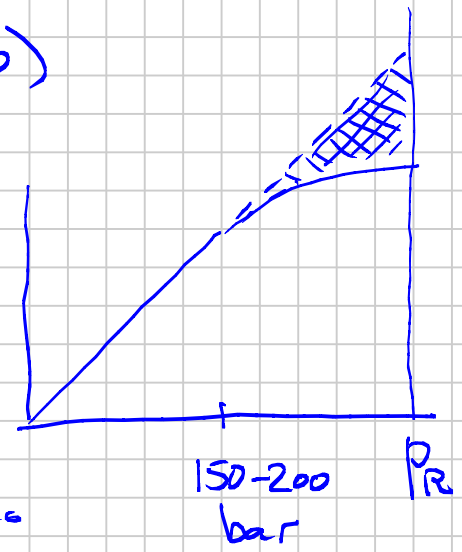


# Alternative Graphical Representation of IPR



III. 1940s → (Fetkovich +++ before 1990)  
 (Log-Log)  
 Backpressure Plot

- $p_p : p^2 ; P_R \approx 200 \text{ bar}$



Darcy:  $q_g = \frac{kh}{T_a \left[ \ln \frac{r_e}{r_w} + s \right]} \cdot (p_R^2 - p_{wf}^2)$

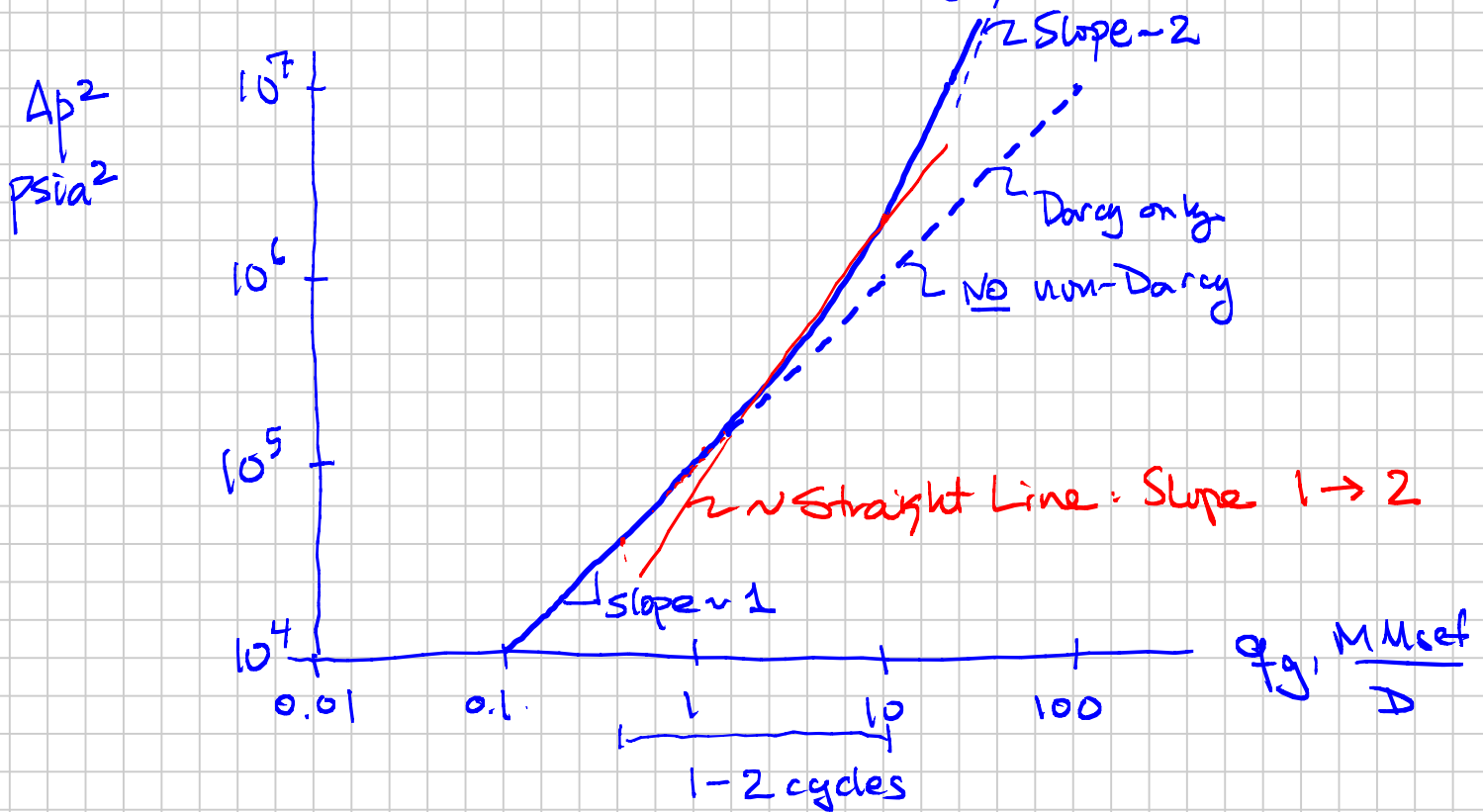
Constant

slope = 1

$$\log q_g = \log C + \log (\Delta p^2)$$

$$\log \Delta p^2 = \log q_g + \log C$$

General Rate Eq. w/ non-Darcy Term



$$\Delta p^2 = p_R^2 - p_{wf}^2 = B q_g^2 + A q_g$$

$$\lim_{q_g \rightarrow 0} \rightarrow A q_g$$

Slope = 1

$$\lim_{q_g \rightarrow \text{large}} \rightarrow B q_g^2$$

Slope = 2

# Approximate log-log straight line "model"

$$q_g = C_R (P_R^2 - P_{wf}^2)^n$$

$$\text{Slope} = \frac{1}{n}$$

$$0.5 \leq n \leq 1$$

Highly  
non-Darcy  
 $Bq_{fg}^2$

Darcy  
 $Aq_{fg}^2$

$$\text{"Reservoir"} \sim \frac{kh}{(\mu z)^T R \left[ \ln \frac{r_e}{r_w} - \frac{3}{4} + s \right]}$$

only  $\rightarrow$  to this  
if  $n=1$

if  $n=0.5$

$$C_R = \frac{1}{\sqrt{B}}$$

$$D \propto \beta \propto \frac{1}{k}$$

# Pipe Flow :

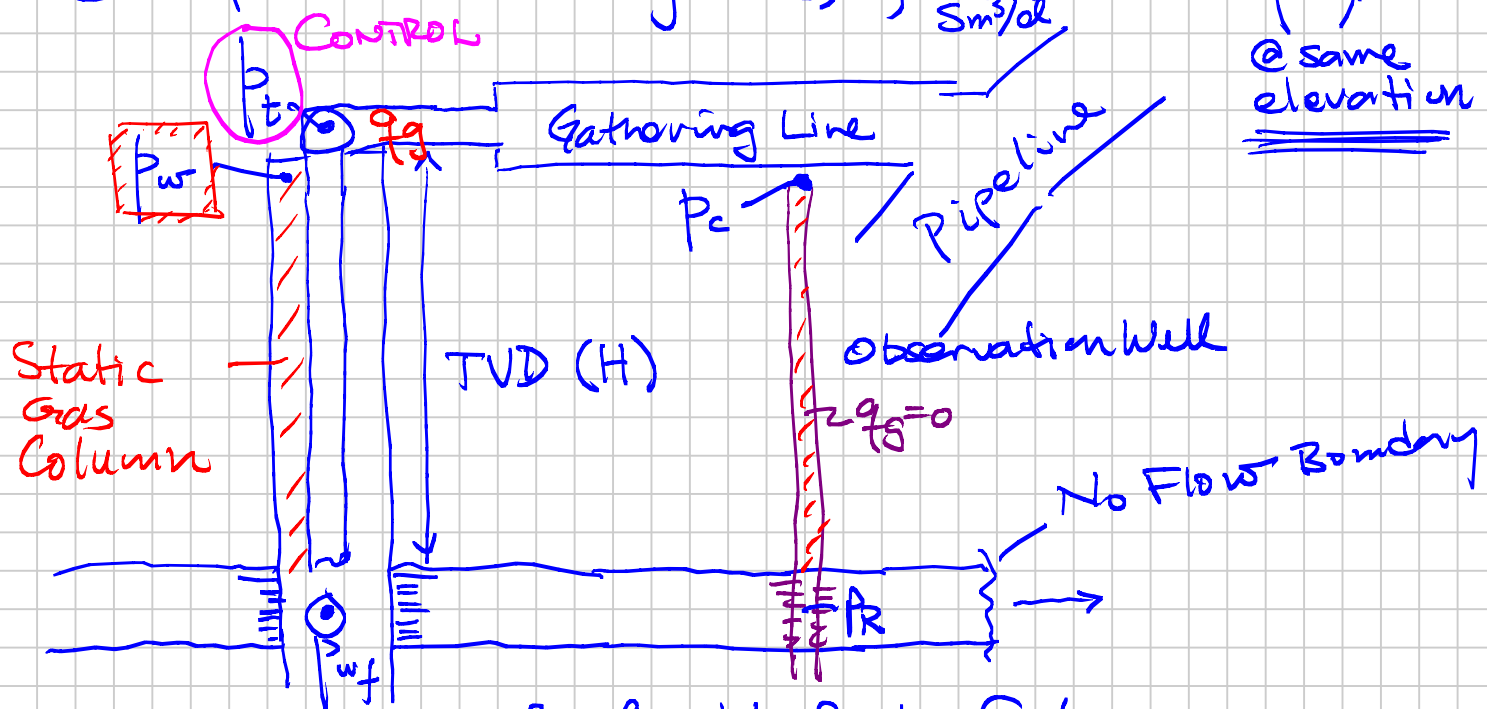
- ① Tubing
- ② Pipeline (Gathering Line)

Ignore Gravity (Only consider friction)

$$q_{fg} = C (P_{in}^2 - P_{out}^2)^{0.5}$$

$\frac{Sm^3/d}{d}$

@ same elevation



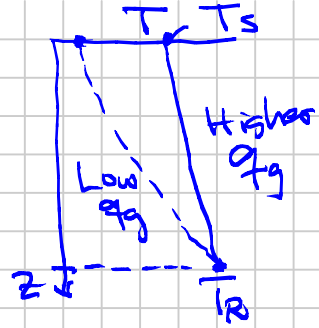
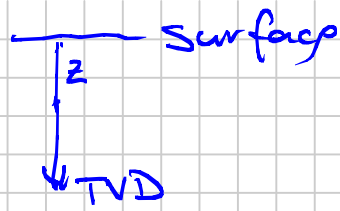
$f_R$  : Reynolds friction factor

$$C(d, L, \overbrace{E, \mu}^{\text{roughness of the pipe}})$$

Correcting for gravity to bring  $P_{wf}$  and  $P_R$  @ TVD depth datum to SURFACE depth datum where  $P_t$  (that we control) is measured.

| <u>PRESSURE</u>   | <u>Datum</u> | <u>Datum</u> | <u>PRESSURE</u> |
|-------------------|--------------|--------------|-----------------|
| $\Rightarrow P_R$ | TVD          | Surface      | $P_c$           |
| $P_{wf}$          | TVD          | Surface      | $P_w$           |
| $P_t$             | Surface      | Surface      | $P_t$           |

$$p_{wf} \leftrightarrow p_w$$



Static Fluid Column:

$$\frac{dp}{dz} = \text{constant} = \rho_g g$$

$$\rho_g = \frac{pM}{RTz}$$

$$\bar{T} = \frac{1}{2}(T_s + T_b)$$

$$\bar{z}(p, T) = \frac{z(p, T_s) + z(p, T_b)}{2}$$

$$= \left( \frac{M}{RT\bar{z}} \right) \cdot p$$

constant H(TVD)

$$\int_{p_T}^{p_B} \frac{1}{p} dp = \left( \frac{Mg}{RT\bar{z}} \right) \int_0^H dz$$

$$\ln(p_B/p_T) \approx \underbrace{\left( \frac{Mg}{RT\bar{z}} \right) H}_{= S/2}$$

$$\frac{p_B}{p_T} \approx \exp(S/2)$$

$$\frac{p_{wf}}{p_w} = e^{S/2}$$

where  $S = 0.0375 \frac{GH(T_a z_a)}{R}$

$$S = \frac{\rho_g g H}{\bar{T} \bar{z}}$$

units  
28.97  $\frac{\text{Marr}}{R}$   
 $\frac{\text{ft} \cdot \text{OR}}{R}$

|                             |
|-----------------------------|
| $\frac{p_2}{p_1} = e^{S_1}$ |
| $\frac{p_2}{p_1} = e^{S_2}$ |

~ constant

Reservoir  $\Delta p$   
 $P_R - P_{wf}$

$$\left(\frac{D_R^2}{C^S}\right) \left(\frac{P_{wf}^2}{e^S}\right) = \left(\frac{B_R}{C^S}\right) q_{fg}^2 + \left(\frac{A_R}{C^S}\right) q_{fg}$$

$$p_c^2 - p_w^2 = B'_R q_{fg}^2 + A'_R q_{fg}$$

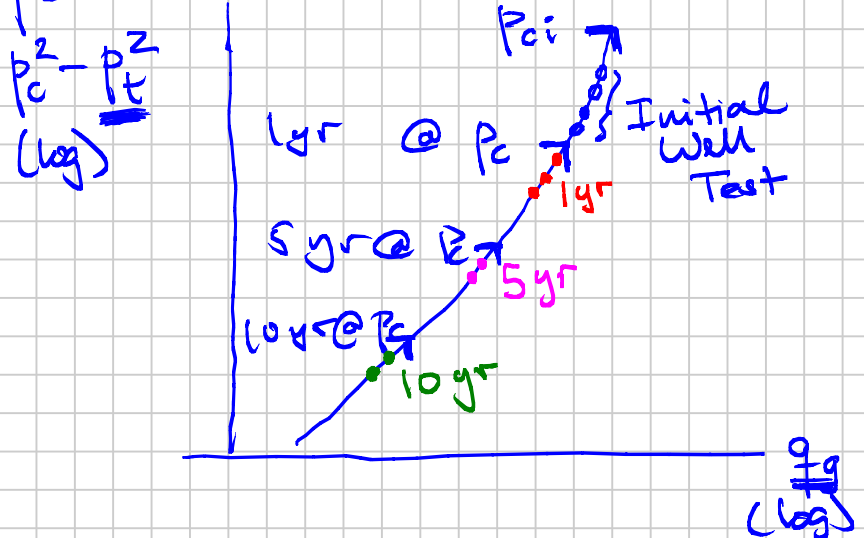
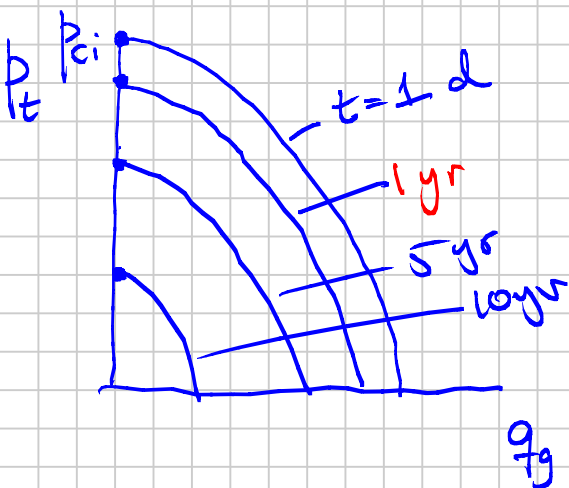
Tubing  $\Delta p$   
 $P_{wf} - P_t$

$$p_w^2 - p_t^2 = \frac{1}{C_T^2} q_{fg}^2$$

$$p_c^2 - p_t^2 = \underbrace{\left(B'_R + \frac{1}{C_T^2}\right)}_{\text{run-Darcy + Friction}} q_{fg}^2 + \underbrace{A'_R}_{\text{Darcy}} q_{fg}$$

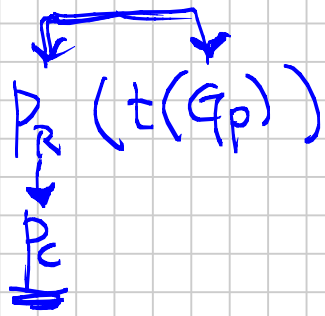
$$p_c^2 - p_t^2 = B_{wh} q_{fg}^2 + A'_R q_{fg}$$

Wellhead Backpressure Eq. @ a particular time in depletion when  $p_c$  exists.





$$\underbrace{p_c^2 - p_k^2}_{R + T}$$



$$G_p = \int_0^t q_g dt$$