

# PVT Fluid Behavior

Note Title

2013-09-05

<u>Phase</u>	$\&$	<u>Volumetric Behavior</u>	<u>(++)</u>
Gas		$V = f(p, T, n_i)$ Composition	Pa·s; cp *
Oil		Gas $y_i$	Viscosity ( $\mu$ )
		Oil $x_i$ liquid (oil)	Interfacial Tension ( $\sigma$ )
Water		Water $x_{wi}$ liquid (water)	IFT **
(Solid)			(Surface) Tension
		$n_i \equiv \frac{n_{ip}}{n_p}$	$\sigma_{go} \sigma_{gw} \sigma_{ow}$
		$y_i = \frac{n_{ig}}{n_g} = \frac{n_{ig}}{\sum_i n_{ig}}$	* $1 \text{ mPa}\cdot\text{s} = 1 \text{ cp}$
			** $\text{N/m}$ dynes/cm
		$v \equiv \frac{V}{n}$	$1 \text{ mN/m} \equiv 1 \frac{\text{dynes}}{\text{cm}}$
		$Z \equiv \frac{pV}{nRT} = \frac{pv}{RT}$	
		$\rho \equiv \frac{m}{V} = \frac{pM}{RTZ}$	
		Mass : $\rho \cdot V$	

## Equation of State

Gas:  $pV = nRT$  (Ideal)

$pV = nRTZ_g$  (Real)

$Z_g(p_r, T_r, y_i)$

Purely Volumetric

Oils: e.g.  $c_0 \equiv -\frac{1}{V} \left( \frac{\partial V}{\partial p} \right)_T \approx \text{constant}$

General EOS works for both  $g \neq 0$

Cubic EOS (other more complicated)

Ch. 4

$$P = \frac{RT}{v-b} - \frac{a}{[v^2]}$$

Repulsive

Attractive

vdW:  $[ ] = v^2$

\* SRK:  $[ ] = v(v+b)$

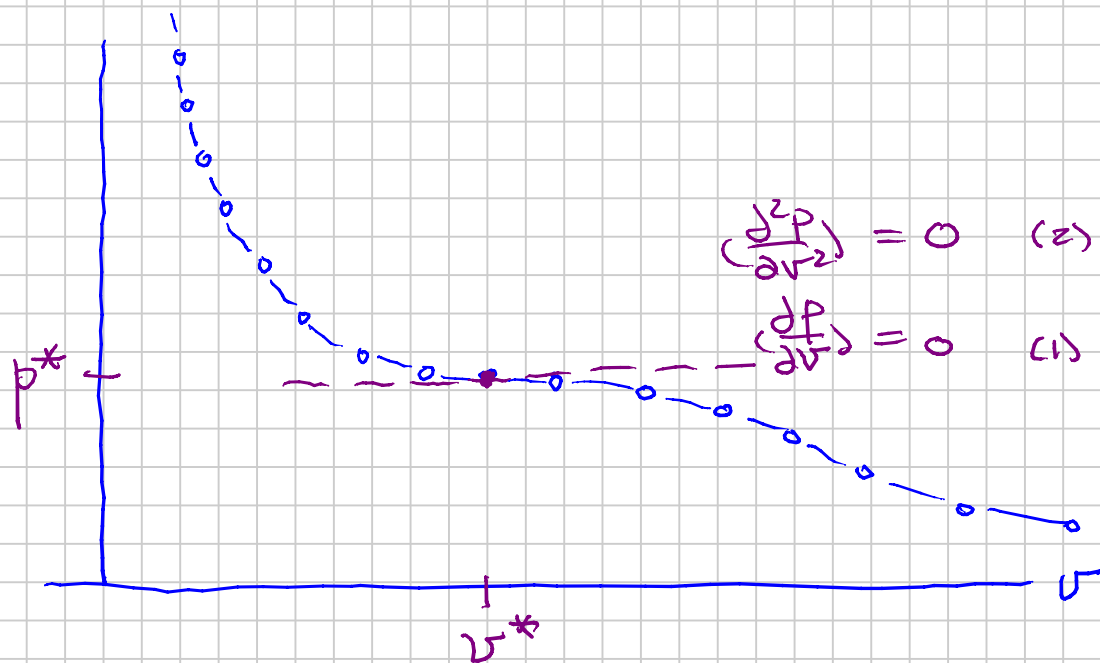
\* PR:  $[ ] = v(v+b) + b(v-b)$

van der Waals

$v \rightarrow \infty$  :  $P = \frac{RT}{v}$  Ideal Gas

Need  $a$  &  $b$  to use this equation!

vdW: At some special temperature  $T^*$



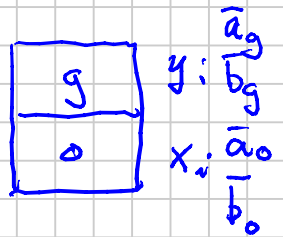
$T^* = T_c$   
 $P^* = P_c$

$$\Rightarrow a_i = \Omega_a \frac{R^2 T_{ci}^2}{p_{ci}} \quad \text{vdW} \quad \frac{27}{64} \quad \Omega_a = \text{number "1"} \sim 0.4$$

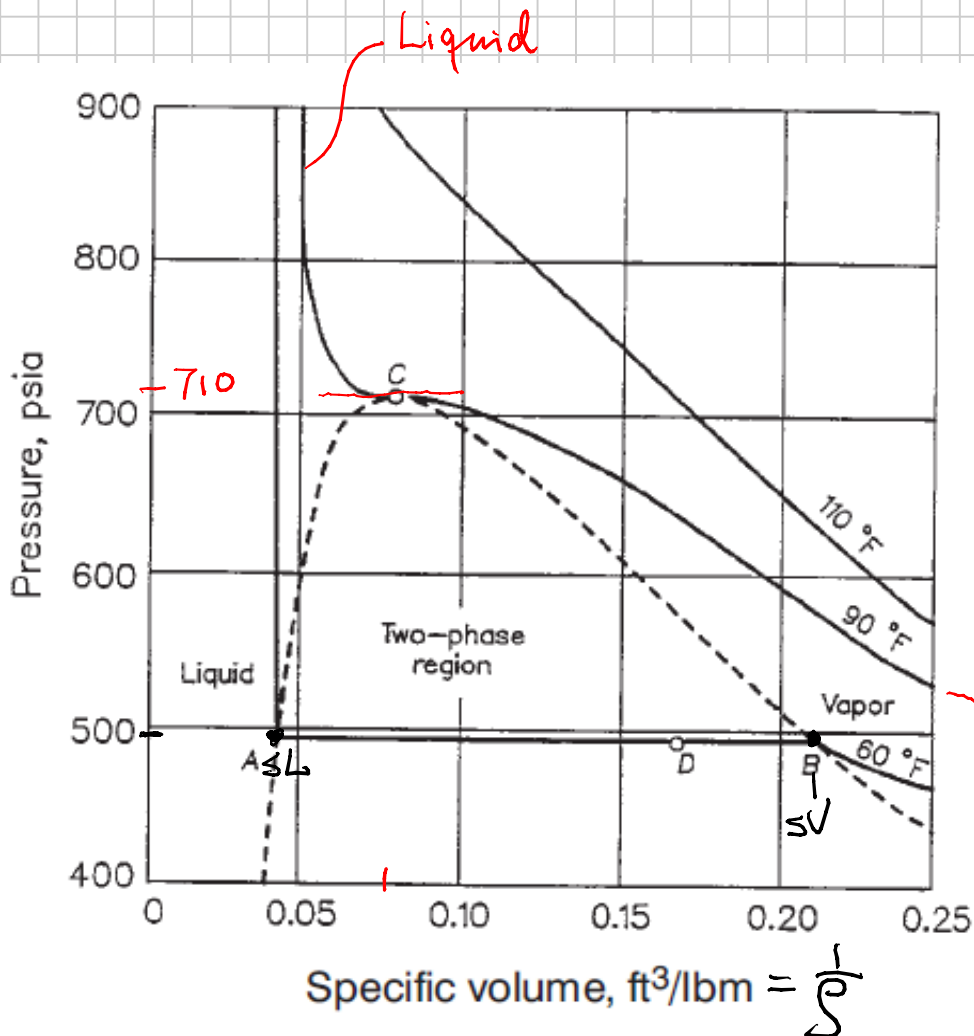
$$b_i = \Omega_b \frac{R T_{ci}}{p_{ci}} \quad \frac{1}{8} \quad \Omega_b = \text{number "2"} \sim 0.1$$

Mixture:  $u_i$  ( $y_i$   $x_i$   $x_{wi}$ ) phase  $p$  ( $g$   $o$   $w$ )  
Phase

$$\bar{a}_p = \sum_{i=1}^N \sum_{j=1}^N u_i u_j (a_i a_j)^{1/2}$$



$$\bar{b}_p = \sum_{i=1}^N u_i b_i$$



$$P_{VCR} (T=60^\circ\text{F}) = 490 \text{ psia}$$

$$\int_{Vs} \sim 5 \frac{\text{lb}}{\text{ft}^3}$$

$$\int_{Ls} \sim 25 \frac{\text{lb}}{\text{ft}^3}$$

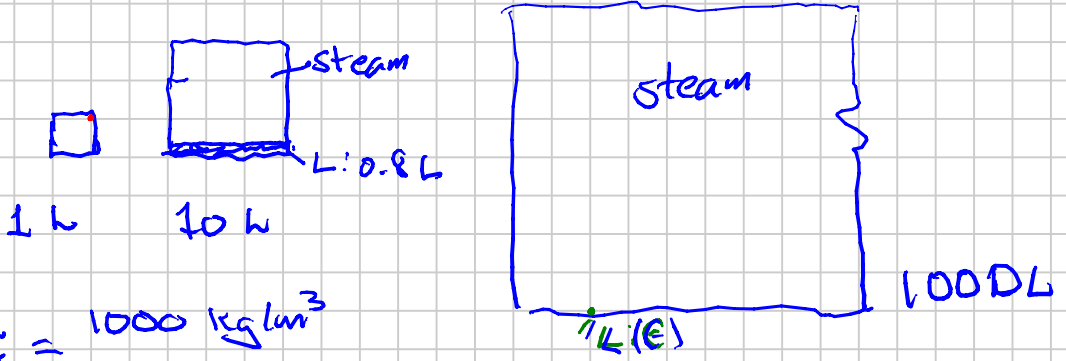
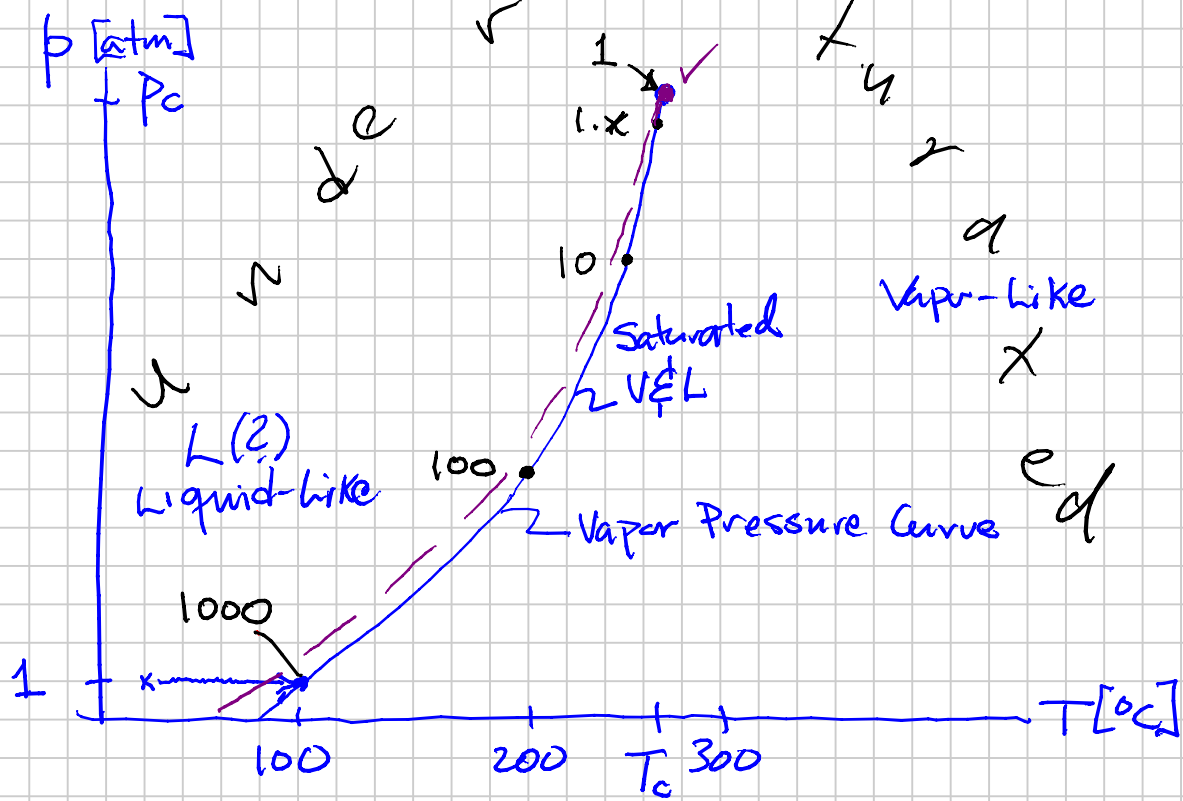
Ideal Gas

Fig. 2.7— $p$ - $V$  diagram for ethane at three temperatures (from Standing<sup>26</sup>).

# Single-Component Phase Equilibria (Chemical Equilibria) ?

Phase Behavior  $\leftrightarrow a$

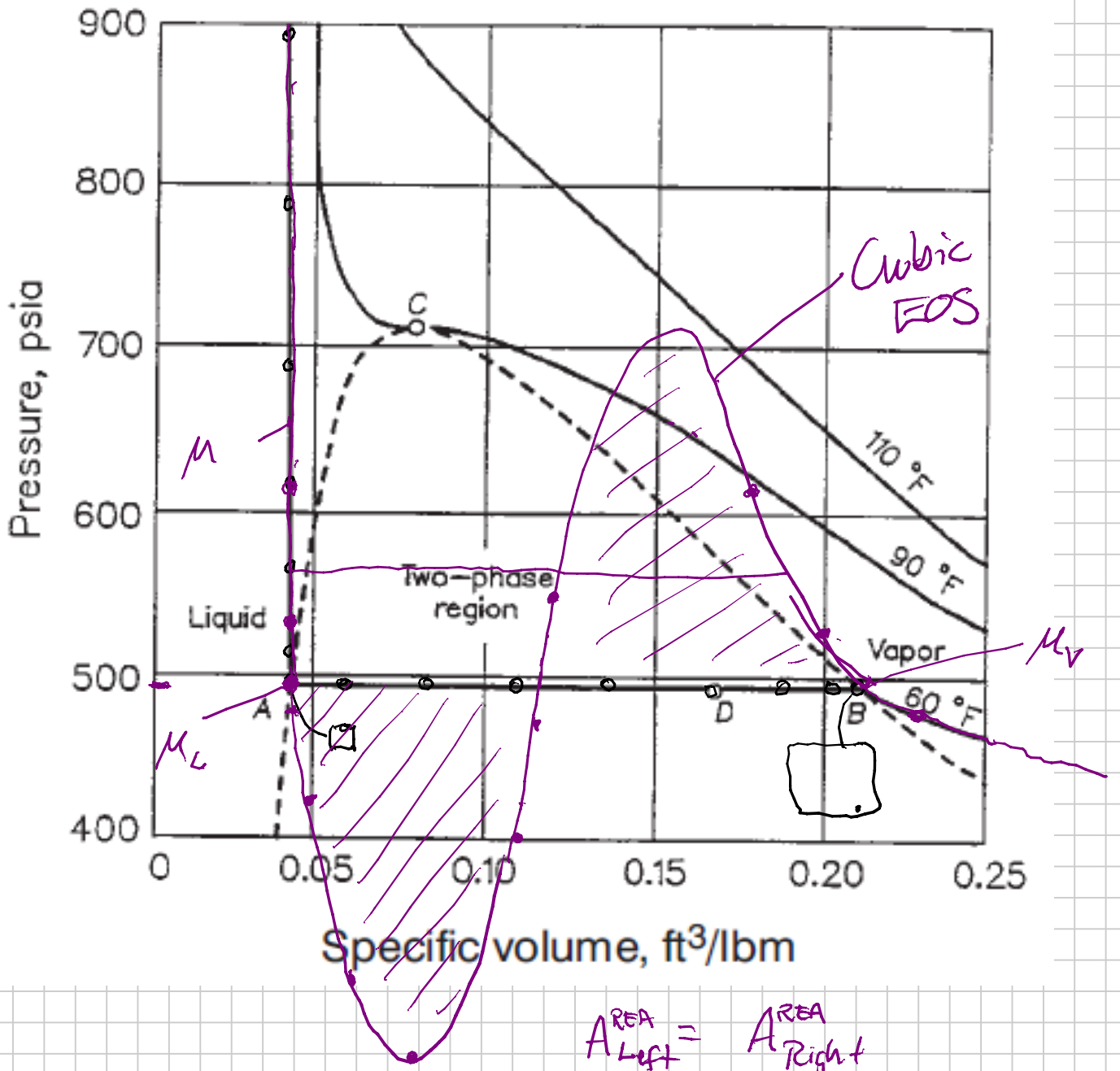
H<sub>2</sub>O



Liquid  $\frac{\rho_L}{\rho_V} = 1000 \text{ kg/m}^3$   
 Steam  $1 \text{ kg/m}^3$

$$p = \frac{RT}{v-b} - \frac{a}{v^2} = \frac{RTv^2 - a(v-b)}{v^3 - bv^2}$$

Cubic in Volume ...  $v^3 + v^2 + v + = 0$



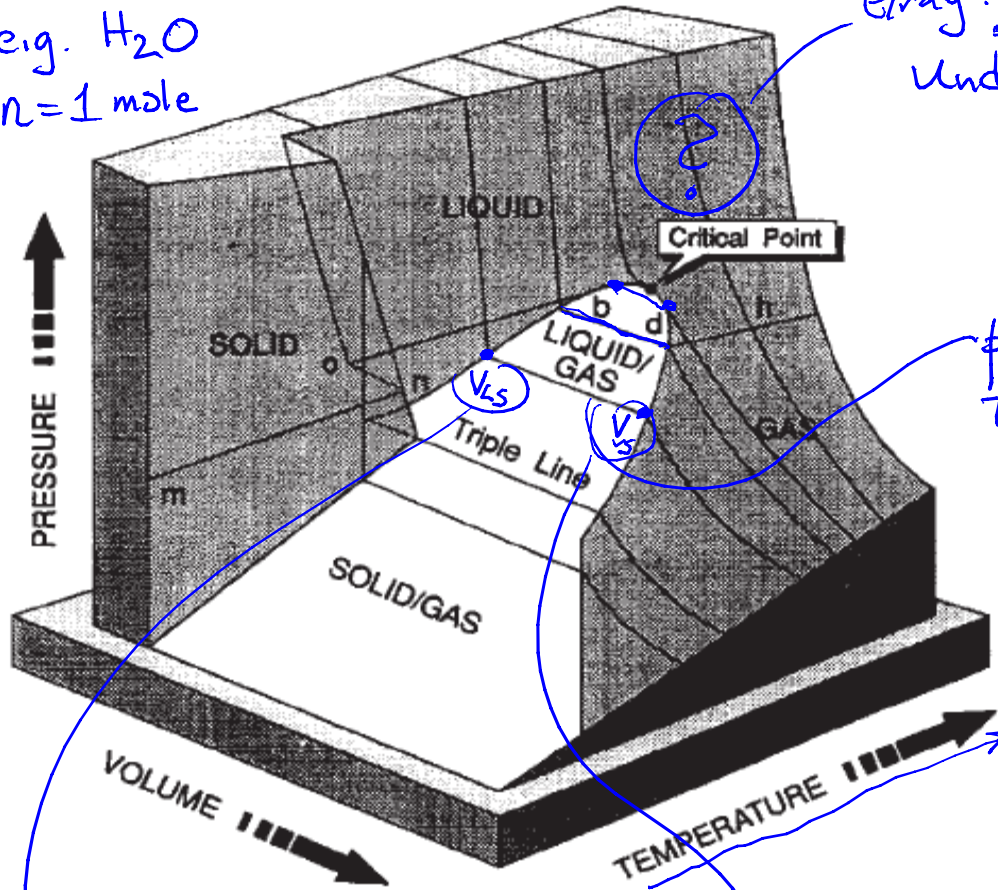
$$\mu = \text{chemical energy} = \int_0^P \left( v - \frac{RT}{P} \right) dp$$

$$\mu_L(P) = \mu_V(P) \quad p = P_V$$

PURE COMPOUND

e.g.  $H_2O$

$n = 1 \text{ mole}$



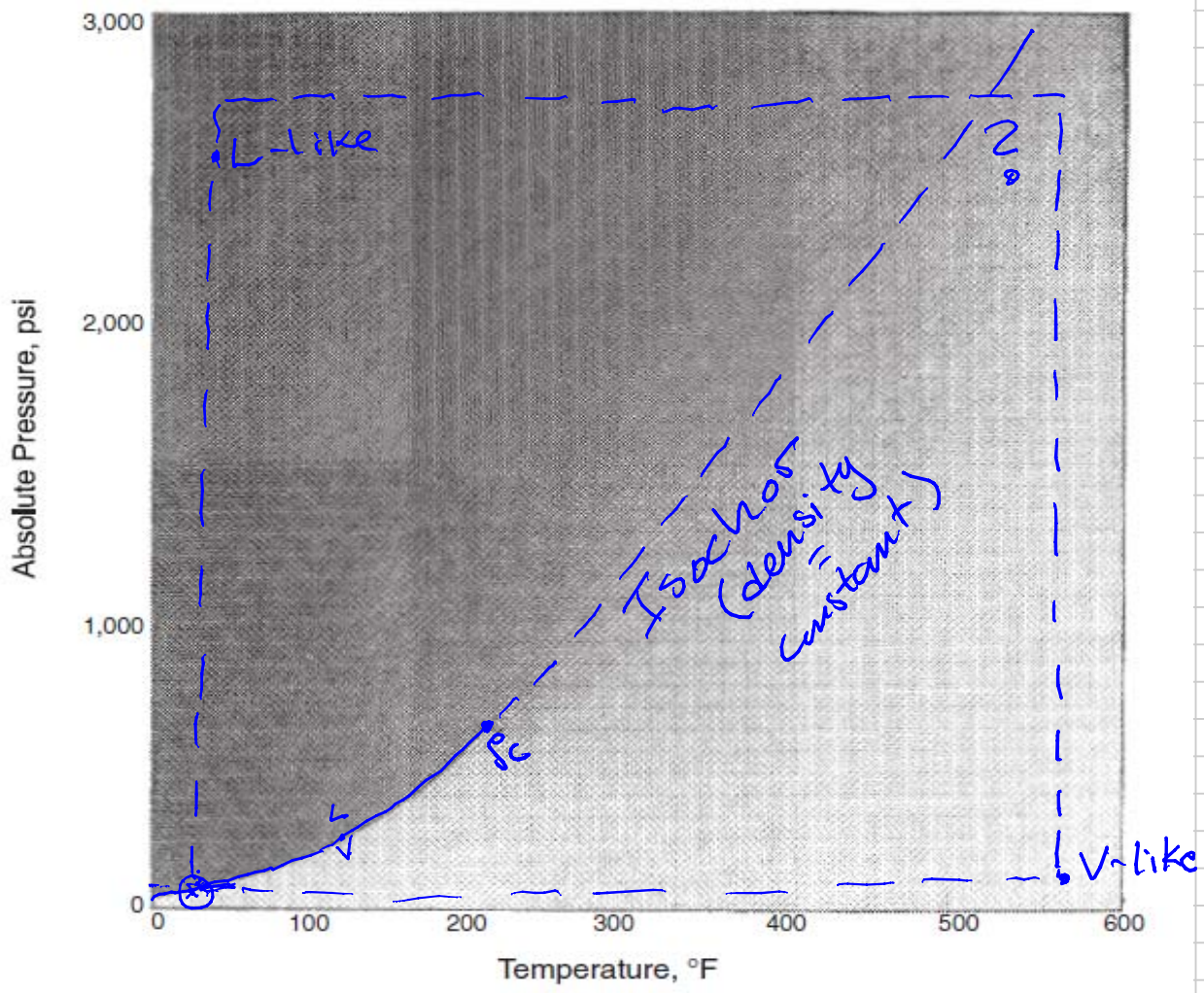
Gray: ~~Single Phase~~  
Undersaturated  
Phase

$p = 1 \text{ atm}$   
 $T = 100^\circ \text{C}$   
 $212^\circ \text{F}$

$V_{sh}$  saturated liquid  
↓

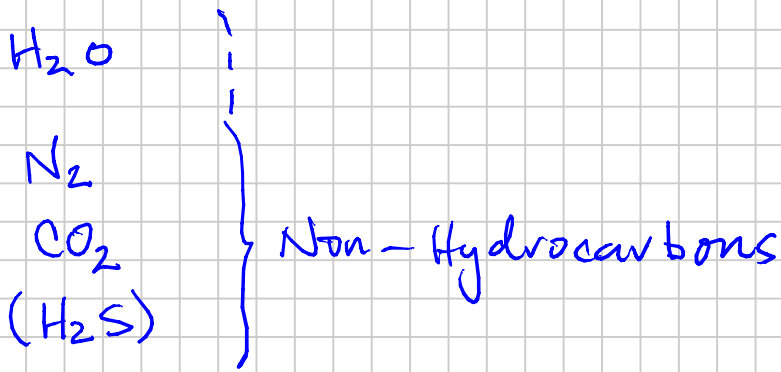
$V_{sv}$  = saturated vapor  
↑

Propane

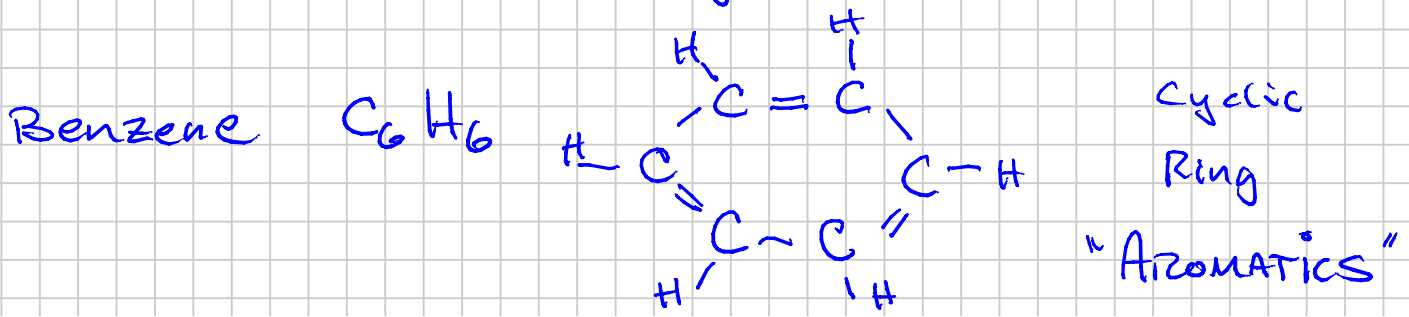
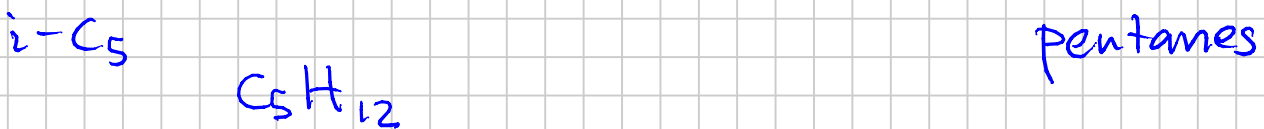
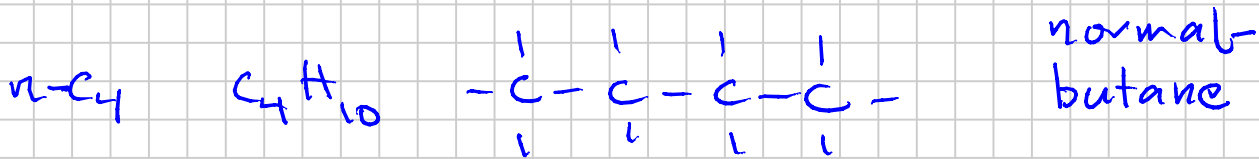
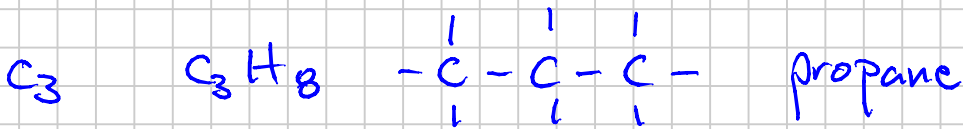
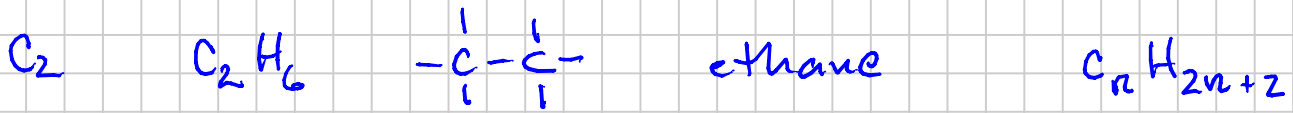
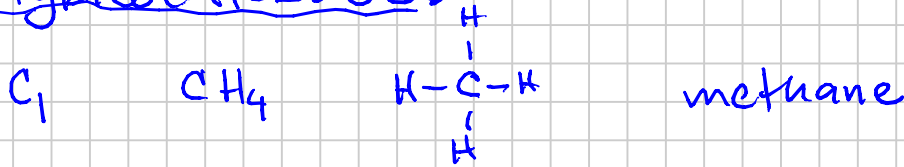


Degree of Shading  $\propto p$

# Compounds Making up Petroleum Systems



## Hydrocarbons:





- Density much higher than  $\rho_{n-C_6}$   
 $875 \text{ kg/m}^3$   $655 \text{ kg/m}^3$

## Chemical Make-up Character of HCs (PNA)

Paraffins

Napthenes

Aromatics

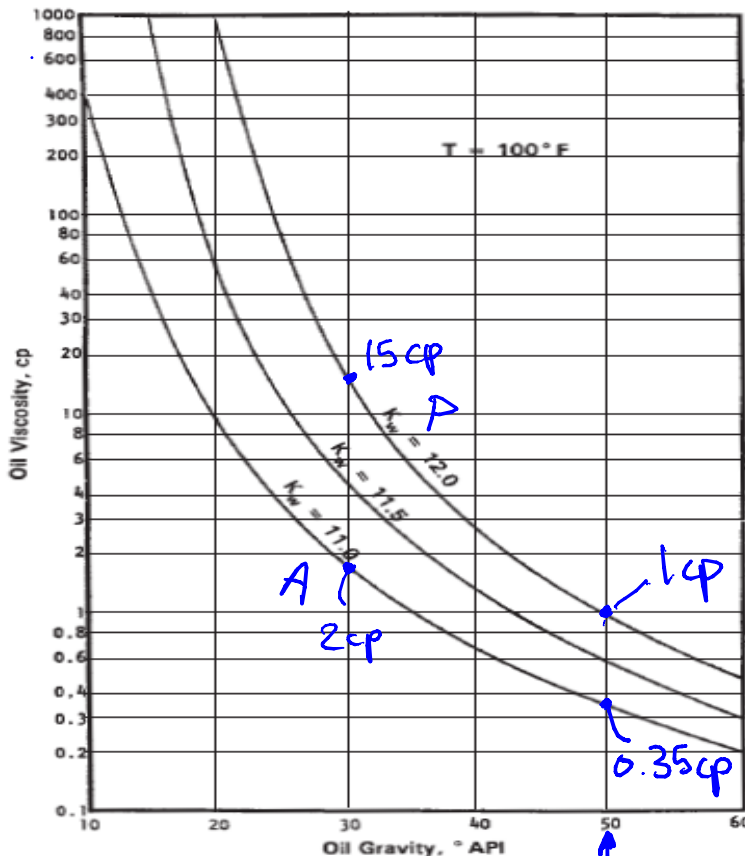


Fig. 3.21—Dead-oil (stock-tank-oil) viscosities at 100°F for varying paraffinicity (from Ref. 33).

1000  
C30+

SCN

750

700  
C7

$\rho_L$   $\text{kg/m}^3$

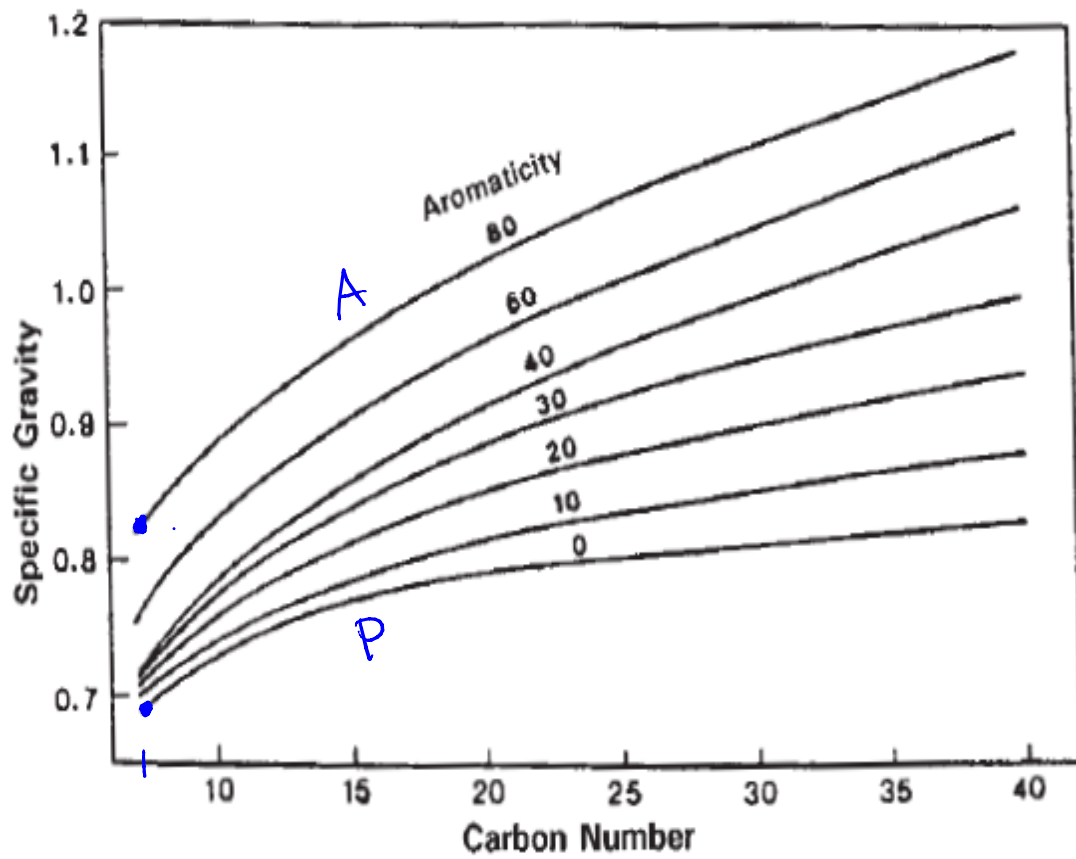


Fig. 5.15—Specific gravity vs. carbon number for constant values of the Yarborough aromaticity factor (after Yarborough<sup>1</sup>).