

## Development of Gas Material Balances

② Pot Aquifer Gas MB

① Straight-Line Gas MB

ASSUMPTIONS SLMB:

\* (a)  $HCPV_g (V_{gr}) = \text{constant during depletion}$

(b) Const.  $T_R$

(c) No injected gas

(d) Produced "Surface Gas" is  
"surface wet gas volume"

$$G_p = G_{pw} = G_{pd} + N_p \left( \frac{p_0}{M_0} \right) \left( \frac{RT_{sc}}{p_{sc}} \right)$$

Actual produced surface gas @ STC
 $\eta p_0$ 
 $23.68 \text{ Sm}^3 / \text{kg-mole}$

$G_{EQ}$

(e) Real Gas Law applies

$$p V_g = n R T Z$$

$$(f) \text{ " } G_{pw} \text{ " } = \eta \left( \frac{RT_{sc}}{p_{sc}} \right)$$

Surface Gas Volumes Used in Any / All

" $p/Z$ " gas material balances are  $G_{pw} \rightarrow \eta$

SLMB:

$$pV = nRTz \Rightarrow V_{gR} = \frac{n_{gR} R T_R z}{p_R}$$

$$V_{gRi} = V_{gR} \text{ at any } p_R < p_{Ri}$$

HCPU<sub>gi</sub>

$$\frac{n_{gRi} R T_R z_i}{p_{Ri}} = \frac{n_{gR} R T_R z_R}{p_R}$$

Molar Material Balance

$$n_{gR} = n_{gRi} - n_p$$

$$\frac{n_{gRi} z_i}{p_{Ri}} = \frac{(n_{gRi} - n_p) z_R}{p_R}$$

$$\frac{p_R}{p_{Ri}} = \left( \frac{n_{gRi}}{n_{gRi}} - \frac{n_p}{n_{gRi}} \right) \frac{p_{Ri}}{z_i}$$

$$\frac{p_R}{p_{Ri}} = \left( 1 - \frac{n_p}{n_{gRi}} \right) \frac{p_{Ri}}{z_i}$$

$$\frac{n_p \left( \frac{R T_{sc}}{p_{sc}} \right)}{n_{gRi} \left( \frac{R T_{sc}}{p_{sc}} \right)} = G_{pw} = G_p$$

$$n_{gRi} \left( \frac{R T_{sc}}{p_{sc}} \right) = G_w = G$$

$$\boxed{\frac{p_R}{p_{Ri}} = \frac{p_{Ri}}{z_i} \left( 1 - \frac{G_p}{G} \right)} \quad \text{SLMB}$$

② Pot Aquifer Gas M.B.

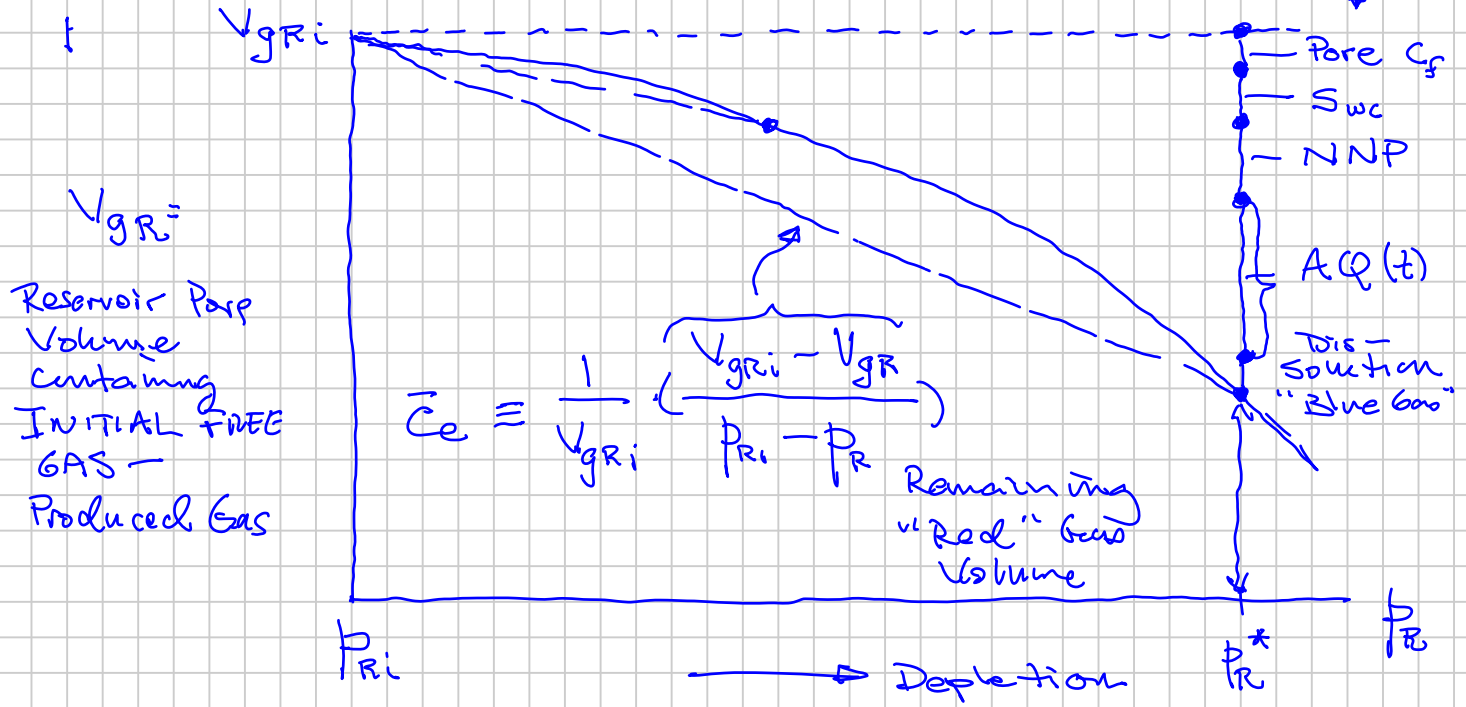
(b)-(f) same assumptions

(a)  $V_{GR} \neq \text{constant}$

$HCPV_g(p_R)$

$C \equiv -\frac{1}{V} \frac{dV}{dp}$

$p = p_R$



Pot Ag.  $C_f(p_R)$   $C_{tw}(p_R)$

99% GMB+AQ

$C_f = \text{const}$

$C_w = \text{const}$

$R_{sw} = 0$   
Blue Gas

# Development of Pot Aquifer Gas M.R. Eq.

$$V_{gRi} = \left[ \frac{n_{gRi} R T_R Z_i}{p_{Ri}} \right]$$

After Depletion to  $p_R$ ,  $V_{gR} < V_{gRi}$

$$\frac{V_{gRi}}{V_{gR}} V_{gR} = \frac{n_{gR} R T_R Z_R}{p_R} \quad ; \quad n_{gR} = n_{gRi} - n_p$$

$$V_{gRi} = \left[ \frac{(n_{gRi} - n_p) R T_R Z_R}{p_R} \cdot \left( \frac{V_{gRi}}{V_{gR}} \right) \right]$$

$$\frac{n_{gRi} R T_R Z_i}{p_{Ri}} = \frac{(n_{gRi} - n_p) R T_R Z_R}{p_R} \cdot \left( \frac{V_{gRi}}{V_{gR}} \right)$$

$$\frac{p_R}{Z_R} \left( \frac{V_{gR}}{V_{gRi}} \right) = \frac{p_{Ri}}{Z_i} \left( \frac{n_{gRi} - n_p}{n_{gRi}} \right)$$

$$\frac{p_R}{Z_R} \left( \frac{V_{gR}}{V_{gRi}} \right) = \frac{p_{Ri}}{Z_i} \left( 1 - \frac{G_p}{G_i} \right)$$

Current Reservoir Volume

Containing "Red" Gas

" ——— " "

Initial Reservoir Volume

Containing "Red" Gas

————— above

" - - - - - " "

$$\bar{c}_e \equiv \frac{1}{V_{gRi}} \left( \frac{V_{gRi} - V_{gR}}{p_{Ri} - p_R} \right) \Rightarrow \left( \frac{V_{gR}}{V_{gRi}} \right) = \left[ 1 - \bar{c}_e^{(p_R)} (p_{Ri} - p_R) \right]$$

$$\frac{P_R}{Z_R} [1 - c_e(P_R) (P_{Ri} - P_R)] = \frac{P_{Ri}}{Z_i} \left(1 - \frac{G_p}{G}\right)$$

$$\bar{c}_e(P_R) = \frac{\bar{c}_f(P_R) + \bar{c}_{tw}(P_R) S_{wc} + M (\bar{c}_f^{(A)} + \bar{c}_{tw})}{1 - S_{wc}}$$

NUP + AQ

$(1 - c_e \Delta p) < 1$  Shrinkage of Red Gas Reservoir Volume

Brief Comment on limitation of "Bot Aquifer"

- AQ volume "encroachment"

There's a delay between  $P_{Rg}$  drops and  $P_{RA}$  drops the same amount

How much delay?

How much less shrinkage of  $\Delta V_{GR, AQ}(t)$

Aquifer Models:

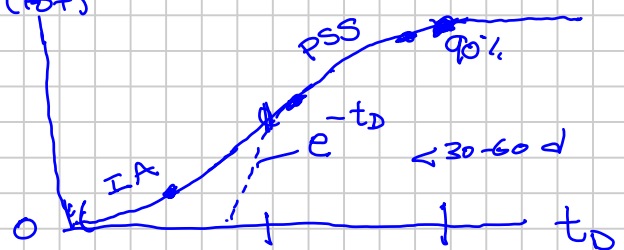
1. Hurst van Everdingen (~0 Aq. Influx  $\Rightarrow$  Bot Aq.)  
- Solves the Aq. diffusivity eq. (Superposition)

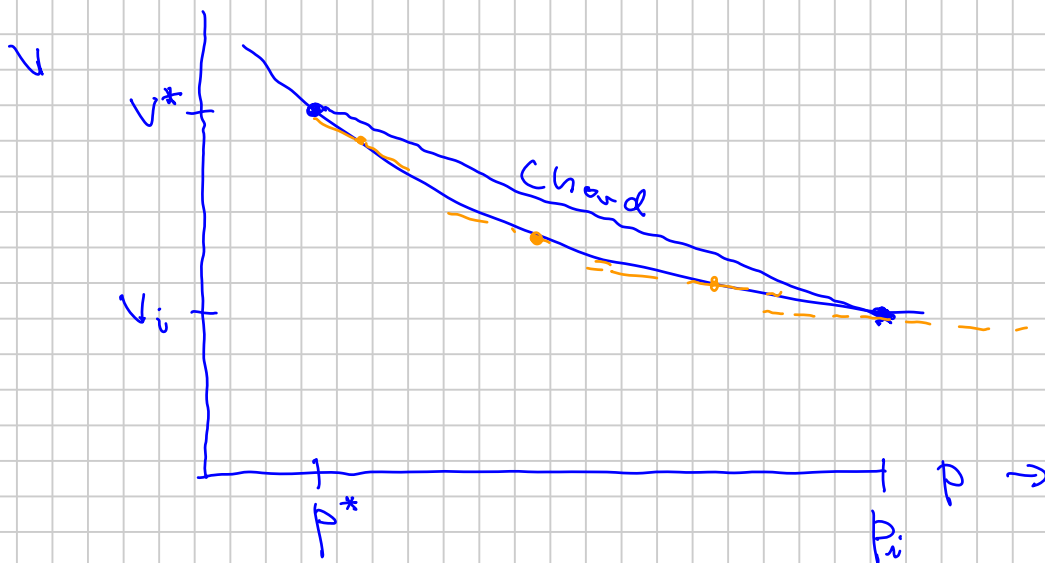
2. Schilthuis (IA) 100% (Bot)

3. ?

4. Fetkovich (PSS)

5. Carter-Tracy





"Cumulative" Compressibility

$$\bar{c}(p) \equiv \frac{1}{V_i} \underbrace{\frac{V(p) - V_i}{p - p_i}}_{\substack{\text{Chord Slope} \\ \text{from } (p_i, V_i)}}$$

$\bar{c}(p)$  finds directly  $V^*$  ( $p = p^*$ )  
from initial  $(p_i, V_i)$