

# RESERVOIR RECOVERY METHODS

Note Title

9/3/2018

## (A) DEVELOPMENT METHODS

① Smaller and often onshore Projects

(G&G) Drill - Discover (HCs) - Produce - Monitor - Modeling  $\Rightarrow$  (HM)  
Forecasting ( $\frac{1}{2}$  Today's optimization) G's P's

History Matching  
Theory  
Eqs.  
Num. methods  
Data  
Tune

② Larger and usually offshore Projects

G-G - Drill - Discover (HCs) -  $\left( \begin{array}{l} \text{Might Start} \\ \text{Production} \\ \text{Test} \end{array} \right)$  - Delimitation - Drill  $\frac{1}{2}$

(a) Modeling - Design - PDO  
(???) Planned Development Operation

Sensitivity Analysis

Statistics

Monte Carlo

- Development - Produce - Monitor - Modeling  $\Rightarrow$  (b)  
Forecasting ( $\frac{1}{2}$  Today's optimization) (HM)

## (B) Modeling Methods

 $p_R(Q_p)$  $N_p \quad N$ 

① (Volumetric) Material Balance:  $p_R = f(p_{Ri}, Q_p, Q_i, Q_{inj})$

Product Volumes

$k \approx 0.01 - 0.1$

$G_p$        $\uparrow$  IGIP  
 $G$

[OIP IGIP WIP] INITIAL = Produced - Injected + Remaining

$\text{Sm}^3$      $\text{scf}$      $\text{Mscf}$

(a)

e.g. Gas M.B. "Pot Aquifer"

$$\frac{p_R}{Z_{GR}} \left[ 1 - c_e (p_{Ri} - p_R) \right] = \left( \frac{p_{Ri}}{Z_{Gi}} \right) \left( 1 - \frac{G_p}{G} \right)$$

$G_p$  = cum. Gas (surface Gas Product) Produced

$G$  = IGIP ( — " — )

$p_R(Q_p)$

(b) Each and All RFUs

Aside: Reservoir Simulation of Depletion

$$N_{\text{cells}} \approx N_{\text{RFU}}$$

if ends and bots (k sufficiently high)

$p_R \sim p(x, y, z)$   
during  $\Delta t = 1-6 \text{ mo.}$

## ② Approximate Flow Equations

- Mainly Darcy (In reservoir w/ reservoir rates / surface product rates)
- Depletion

• Surface Rate Eq.  $q_g = \frac{kh (P_R - P_{wf})}{\tau_R \cdot \left[ \underbrace{\ln \frac{r_e}{r_w}}_{2-10} + s + \frac{1}{\gamma} \right]} = \frac{dG_p}{dt}$

Single Phase Oil

$$\frac{dQ_o}{dt} = q_o = \frac{kh (P_R - P_{wf})}{\mu_o B_o \left[ \ln \frac{r_e}{r_w} + s \right]} = \frac{dN_p}{dt}$$

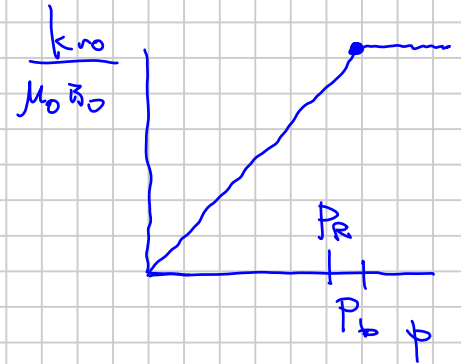
SS/D  
S<sub>w</sub>/D

$$P_p = 2 \int_{P_{inj}}^{P'} \frac{P'}{\mu Z} dp$$

$$-6 < s < +100$$

S&D  $P_R < P_b$

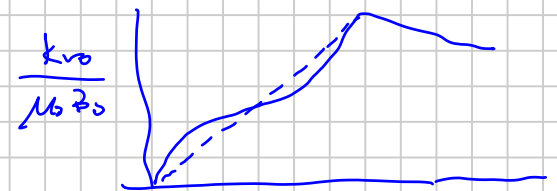
$$q_o = \frac{k_{ro} kh (P_R^2 - P_{wf}^2)}{\mu_o B_o (2P_b) \left[ \ln \frac{r_e}{r_w} + s \right]}$$



Fedorovich

Alt. => Vogel (100s of simulations)

Muskat (1930s-40s)  
Meyers



$$\left\{ \begin{array}{l} \text{MB: } P_R(Q_p) \\ \text{Rate: } q = \frac{dQ_p}{dt} = \text{constant} = PI (P_R - P_{wf}) \end{array} \right.$$

$q(t) \Rightarrow$  Forecast  
(Today's Optimization)



# EOR: Displacement of Insitu Fluid by Injected Fluid

- Two or more wells (I → Ps)

- $v_D = \frac{k}{\mu} \cdot \frac{dp}{dx}$  Darcy Velocity

- Injected (w)

- Produced (o)

$$v_{wD} = \frac{\lambda_w}{\left(\frac{k_w}{\mu_w}\right)} \frac{dp_w}{dx} = k \left(\frac{k_{rw}}{\mu_w}\right) \frac{dp_w}{dx}$$

$$v_{oD} = \frac{\left(\frac{k_o}{\mu_o}\right)}{\lambda_o} \frac{dp_o}{dx} = k \left(\frac{k_{ro}}{\mu_o}\right) \frac{dp_o}{dx}$$

} @ Reservoir Conditions

$$p_w \approx p_o$$

Mobility  $\lambda \equiv \frac{k}{\mu}$   
md/cp

$$M \equiv \frac{\left(\frac{k_{rw}}{\mu_w}\right)}{\left(\frac{k_{ro}}{\mu_o}\right)} = \underbrace{\left(\frac{k_{rw}}{k_{ro}}\right)}_{\substack{\text{Behind Front} \\ \text{Ahead of} \\ \text{Front Rock}}} \underbrace{\left(\frac{\mu_o}{\mu_w}\right)}_{\substack{\text{Fluid} \\ \text{Viscosity} \\ \text{Ratio}}}$$

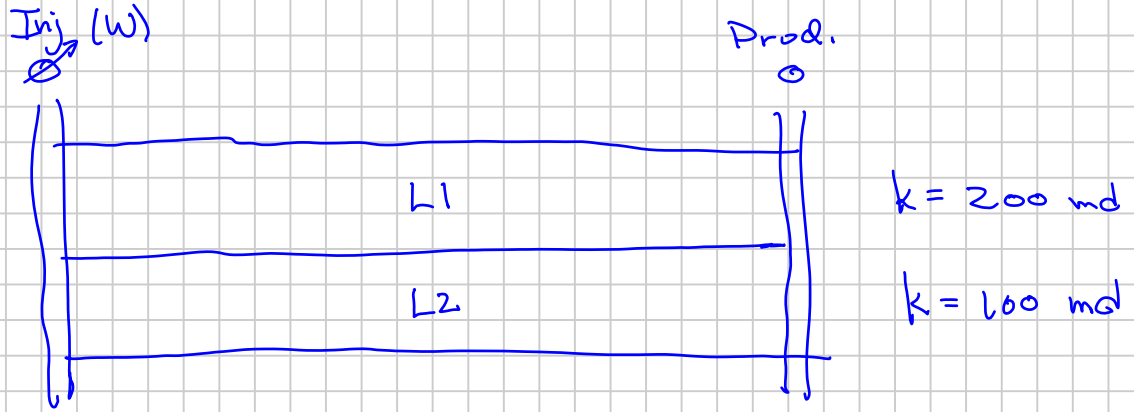
Mobility Ratio

Rel. Perm. Ratio

Viscosity Ratio

Fractional Flow (Ratio)  $f_w(s_w) \equiv \frac{v_{wD}}{v_{wD} + v_{oD}}$

$$= \frac{1}{1 + \frac{k_{ro}}{k_{rw}}(s_w) \frac{\mu_w}{\mu_o}}$$



$$h_1 = h_2$$

Breakthrough occurs at the Same Time  
 in both layers.  $\phi_{L1} = 0.2$        $\phi_{L2} = 0.10$

Transport  $v \neq v_D$   
 $\phi$