

CONSTANT VOLUME DEPLETION (CVD)

- Ch. 6 | Whitson-Torp SPE paper ~1983

- Introduction to / Method for Calculating "Modified" Black-oil PVT Tables (Standard Today)

Ch. 7 Black-oil PVT

$$\frac{U_g}{U_o} = \frac{k_{rg}/\mu_g}{k_{ro}/\mu_o} = \frac{k_{rg} \mu_o}{k_{ro} \mu_g}$$

\uparrow PVT Rock
 \uparrow PVT

$$S_o = \frac{V_{po}}{V_p} \sim \frac{B_{od}(p)}{B_{od,b}}$$

$$S_g = \frac{V_{pg}}{V_p} \sim (R_{sd,b} - R_{sd}(p)) \cdot B_g(p)$$

$$k_{rg} \sim S_g^{n_g} \quad n_g \sim 3-5$$

$$k_{ro} \sim S_o^{n_o} \quad n_o \sim 3-5$$

Corey-Type Equations saturations

$n =$ exponents

$= f(\text{pore size distribution})$

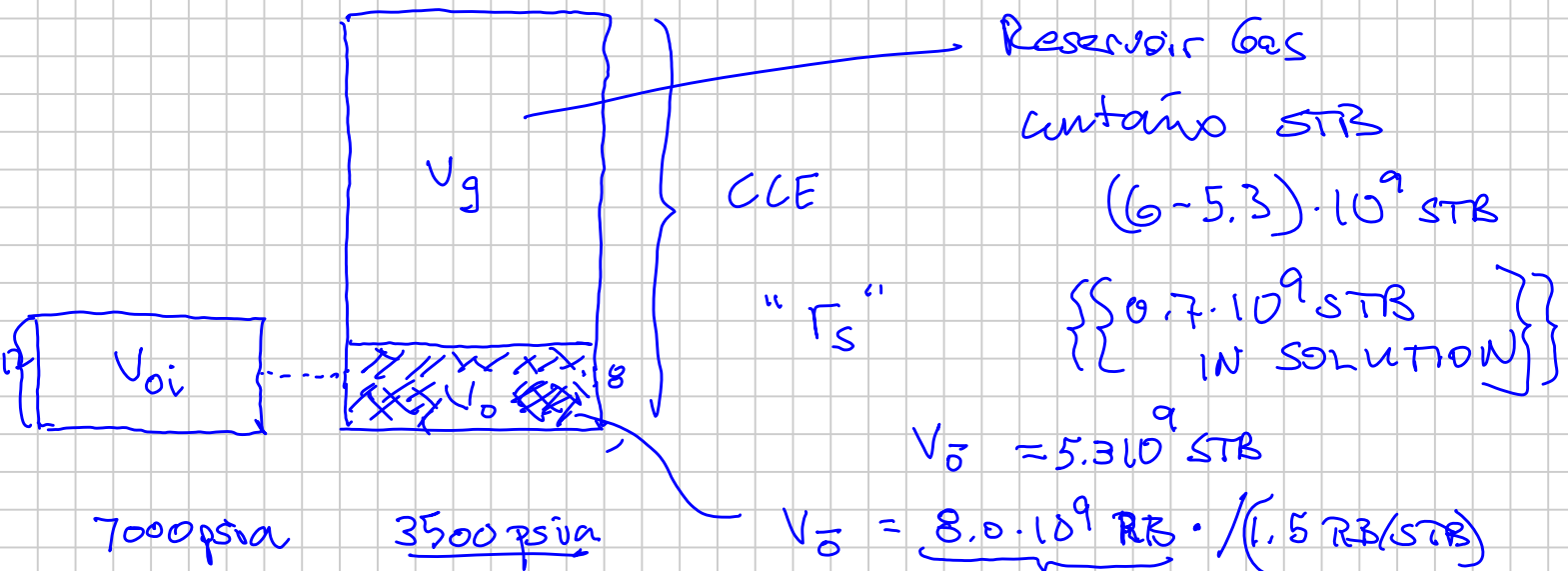
Shale

Chalk

Sandstone



$\left. \begin{matrix} p_o \mu_o \Delta V_{ro} \\ p_s \mu_g \end{matrix} \right\} \sim \text{independent @ } p \text{ on process of depletion}$



$V_{oi} = 12 \cdot 10^9 \text{ RB}$

$V_{oi} = 6 \cdot 10^9 \text{ STB}$
 $C_{st} = \text{STB}$
 Surface Oil STO

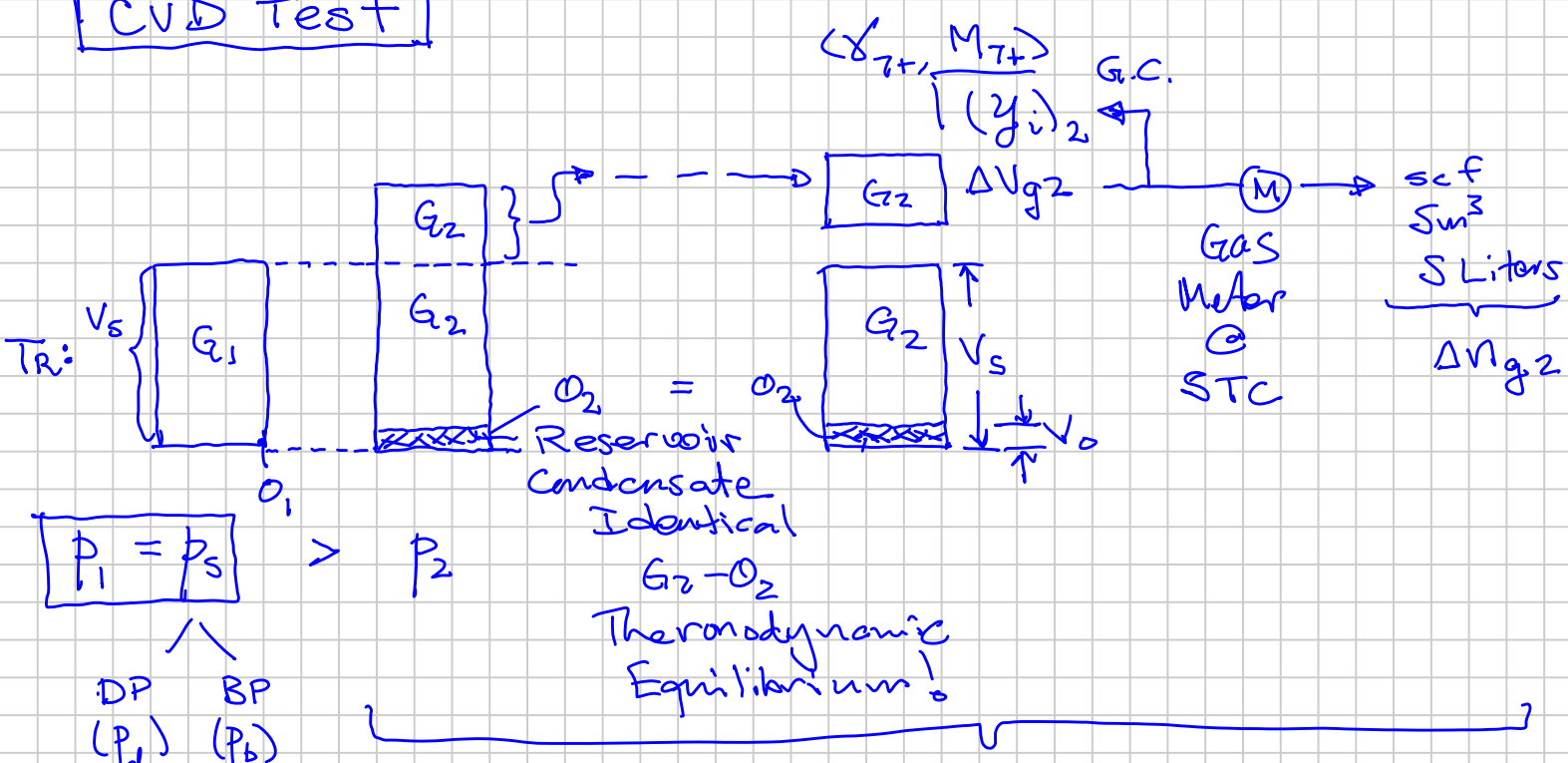
$V_o = 5.3 \cdot 10^9 \text{ STB}$
 $V_o = \frac{8.0 \cdot 10^9 \text{ RB} \cdot (1.5 \text{ RB/STB})}{1.5}$

$B_o^{3500} = B_{od,3500} \cdot \frac{B_{ob}^{SEP}}{B_{od,b}^{DLE}} \approx 1.5 \frac{\text{RB}}{\text{STB}}$
 $= \frac{V_o}{V_o} = 1.5$

Surface Process of R. O.I @ 3500

$\{ T_2, p_2, \Delta V_{g2}(T_2, p_2), \Delta n_{g2} \} \Rightarrow (Z_g)_2$

CVD Test



$P_1 = P_s$		$>$	P_2
DP (P_d) 95%	BP (P_b) 5%		

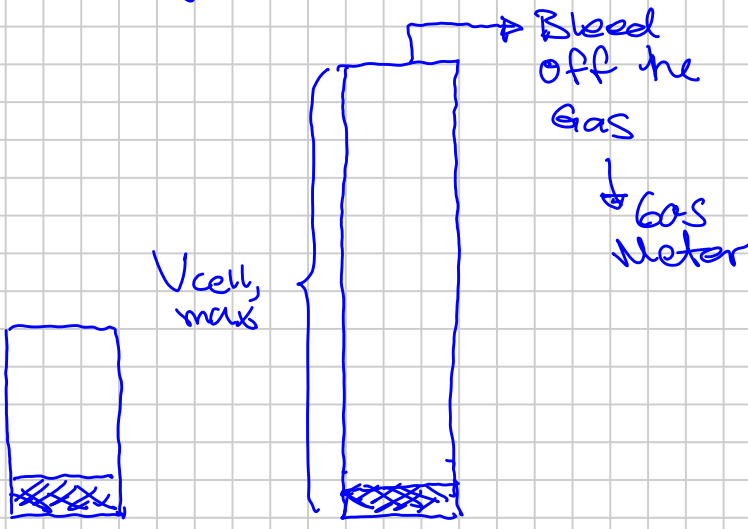
Reservoir Condensate Identical G₂-O₂ Thermodynamic Equilibrium!

Stage 2

6-8 stages (repeated)

(N-1)th Stage ~ 15-50 bar

T_R



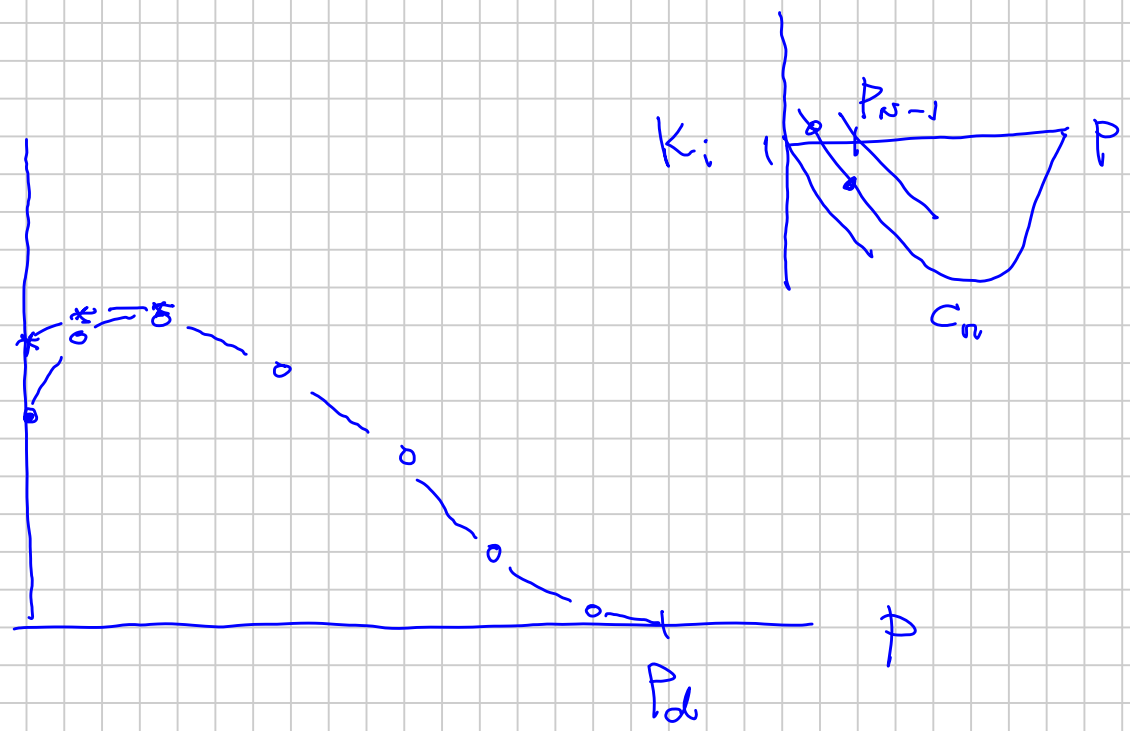
$$\Delta V_{gN} = \Delta U_{gN} - \Delta n_{gN}$$

$(\bar{y}_i)_N$

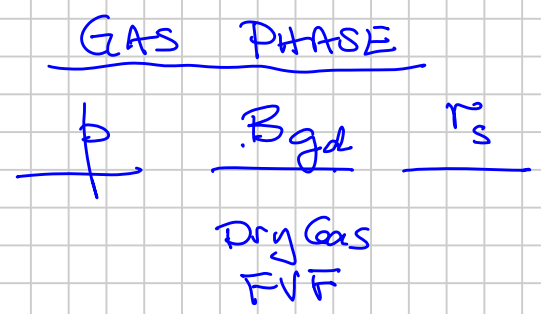
$\left\{ \begin{array}{l} x_{or} \bar{u} \\ M_{or} \bar{v}_{or} \end{array} \right\}$
 $p_N = 1 \text{ atm}$

p_{N-1}
50

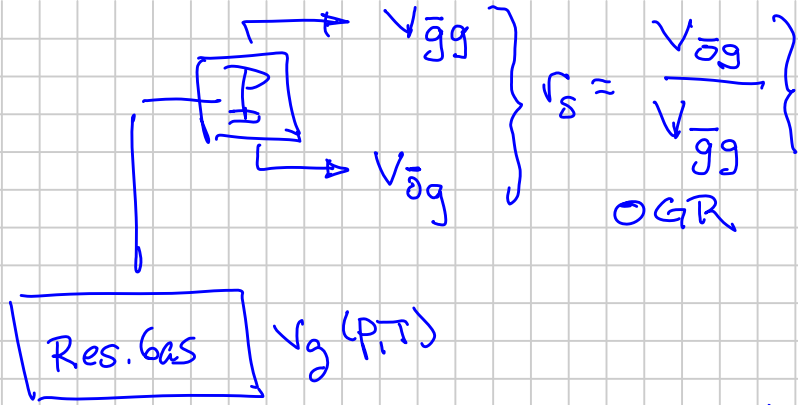
$p^* > p_N$
32 bars



Modified Black-Oil PVT



B_{gd}
↑
"dry"
Reservoir Gas that
has been processed



into
Surface Condensate
(STB)
and Surface Gas
"dry gas"

$$B_{gd} = \frac{V_g(PIT)}{V_{gg}}$$

Difference
1% - 20%

$$\frac{P_{sc}}{P} \frac{T_R Z_s}{Z_{sc}} \neq B_g \text{ text books}$$

$$n_g = n_{gR}$$

$$n_{og} = 0$$