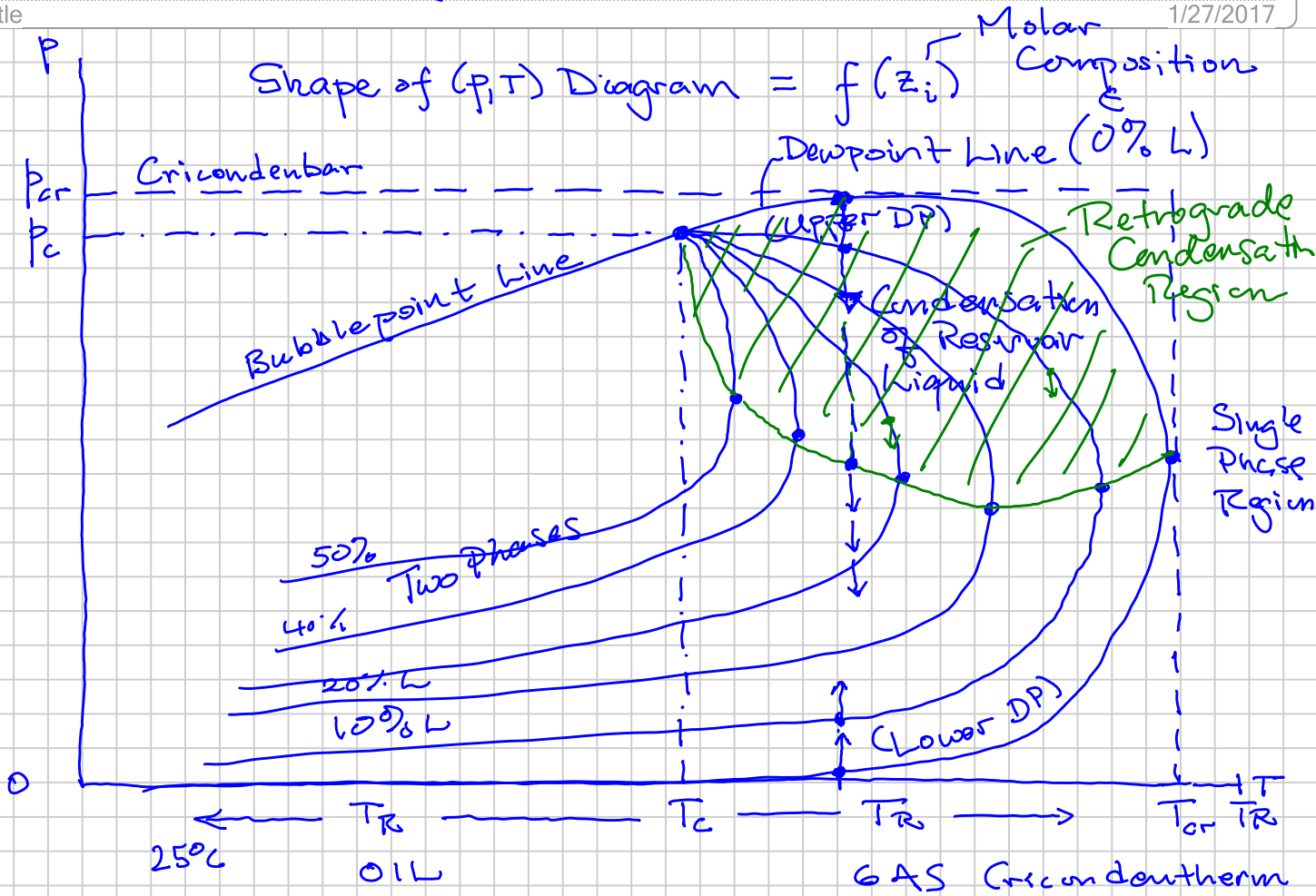


# RESERVOIR FLUID TYPES (GAS | OIL)

⊗  $P_{ri}$

Note Title

1/27/2017



OIL:  $T_r < T_c$  ( $z_{ri} = x_{ri}$ )

Heavy ( $M_o \geq 100$  cp)  
Dead  
Black  
Volatile  
Near-critical

scf/STB

GOR

ORR

API

< 100	< 15
< 100	any
100 - 1000 (1500)	30 any (25-40)
1000 - 2500	40 (35-50)
2500 - 4000	50 (45-50)

GAS:  $T_r > T_c$  ( $z_{ri} = y_{ri}$ )

GAS CONDENSATE:  $T_{cr} > T_r > T_c$

Reservoir condensation of liquid  
"Retrograde" Condensation

$$P_r \geq P_{du}(T_r)$$

ORR [STB/MMscf]

Lean GC	20-50
Average GC	50-150
Rich GC	150-250
Near-Critical GC	250-400

WET / DRY GAS

$$T_r > T_{cr}$$

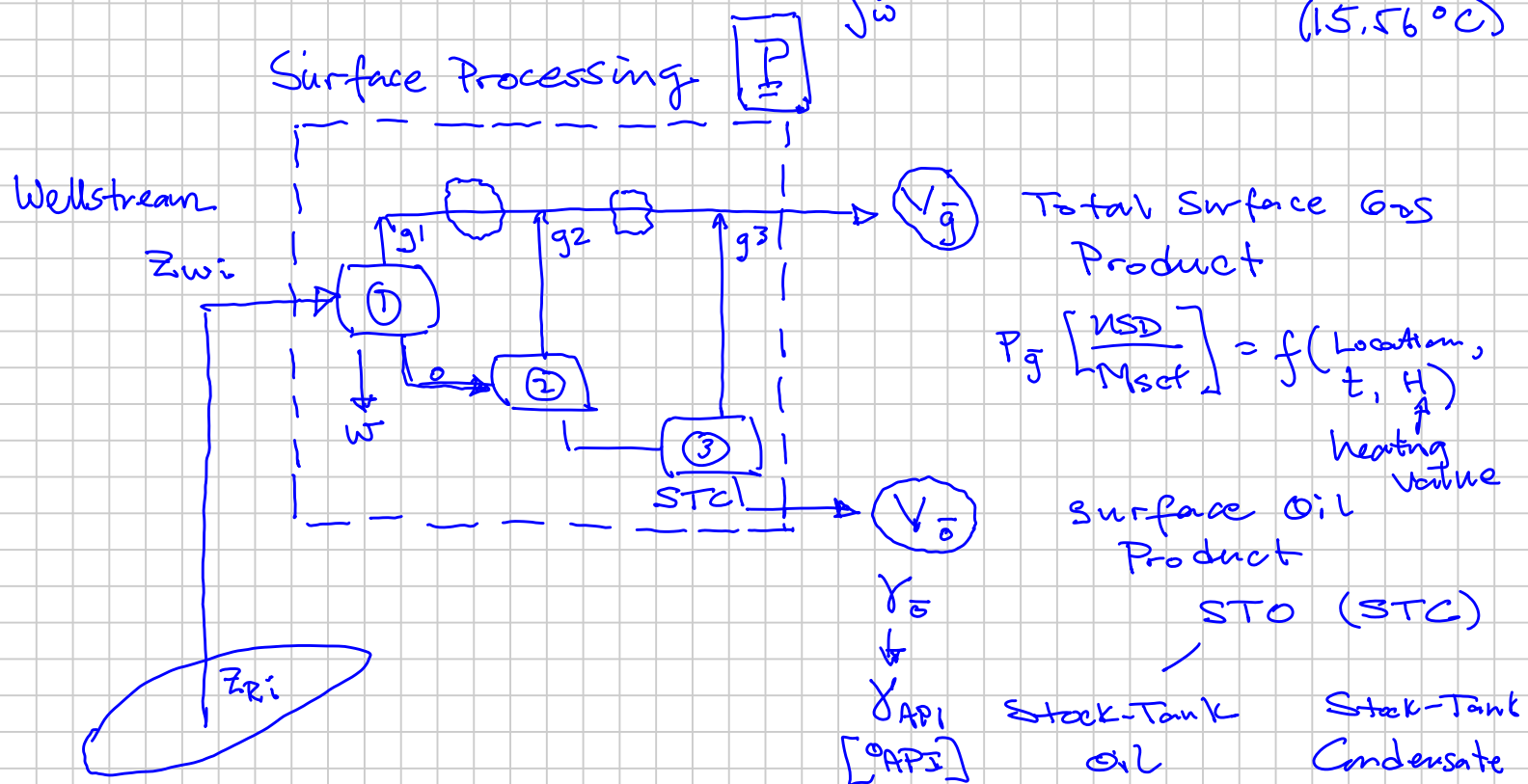
SOME Liquid Condenses at Surface Conditions

NO

NO liquid condensation IN the reservoir

$$\text{API Gravity} = \gamma_{\text{API}} \equiv \frac{141.5}{\gamma_o} - 131.5 \quad \Bigg| \quad \gamma_o = \frac{141.5}{131.5 + \gamma_{\text{API}}}$$

$$\gamma_o \equiv \text{Specific Gravity (Liquid)} = \frac{\rho_o}{\rho_w} \quad @ \quad \begin{matrix} \text{1 atm} \\ 60^\circ\text{F} \\ (15.56^\circ\text{C}) \end{matrix}$$



$$P_o \left[ \frac{\text{USD}}{\text{STB}} \right] = f(t, \gamma_{\text{API}})$$

$$\text{GOR} \equiv \frac{V_g}{V_o} \quad [\text{R}]$$

$$\text{OGR} \equiv \frac{V_o}{V_g} \quad [\text{R}]$$

$$\text{Producing GOR} = r_p$$

$$\text{Producing OGR} = r_p$$

$$\text{If } Z_{wi} \approx Z_{ri}$$

Reservoir Oil ( $T_R < T_c$ )

Reservoir Gas ( $T_{cr} > T_R > T_c$ )

$$R_p = R_s = \text{"solution" GOR}$$

all produced gas is in solution in the reservoir oil

$$r_p = r_s = \text{"solution" OGR}$$

all produced surface oil is in solution in reservoir gas

$$GOR \left[ \frac{\text{Sm}^3}{\text{Sm}^3} \right] \sim GOR \left[ \frac{\text{scf}}{\text{STB}} \right] \frac{1}{5}$$

$$5.615 \frac{\text{ft}^3}{\text{bbl}}$$

$$OGR \left[ \frac{\text{Sm}^3}{10^6 \text{Sm}^3} \right] \sim OGR \left[ \frac{\text{STB}}{10^6 \text{scf}} \right] \cdot 5$$

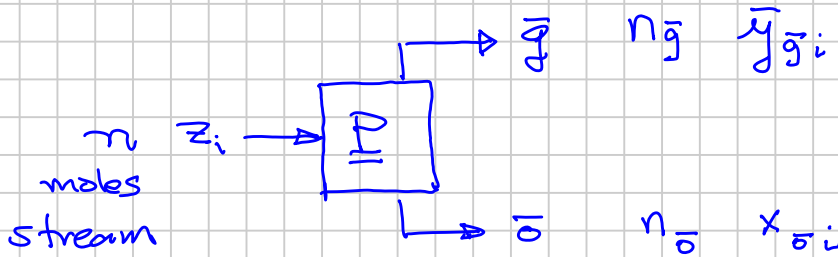
Field Units  
 $M_{scf} = 10^3 \frac{\text{ft}^3 @ \text{STC}}{\text{scf}}$   
 $MM_{scf} = 10^6 \text{ft}^3 @ \text{STC}$

$$\frac{\text{bbl}}{\text{bscf}} = 10^9 \text{scf}$$

$$\frac{\text{Tcf}}{\text{Tscf}} = 10^{12} \text{scf}$$

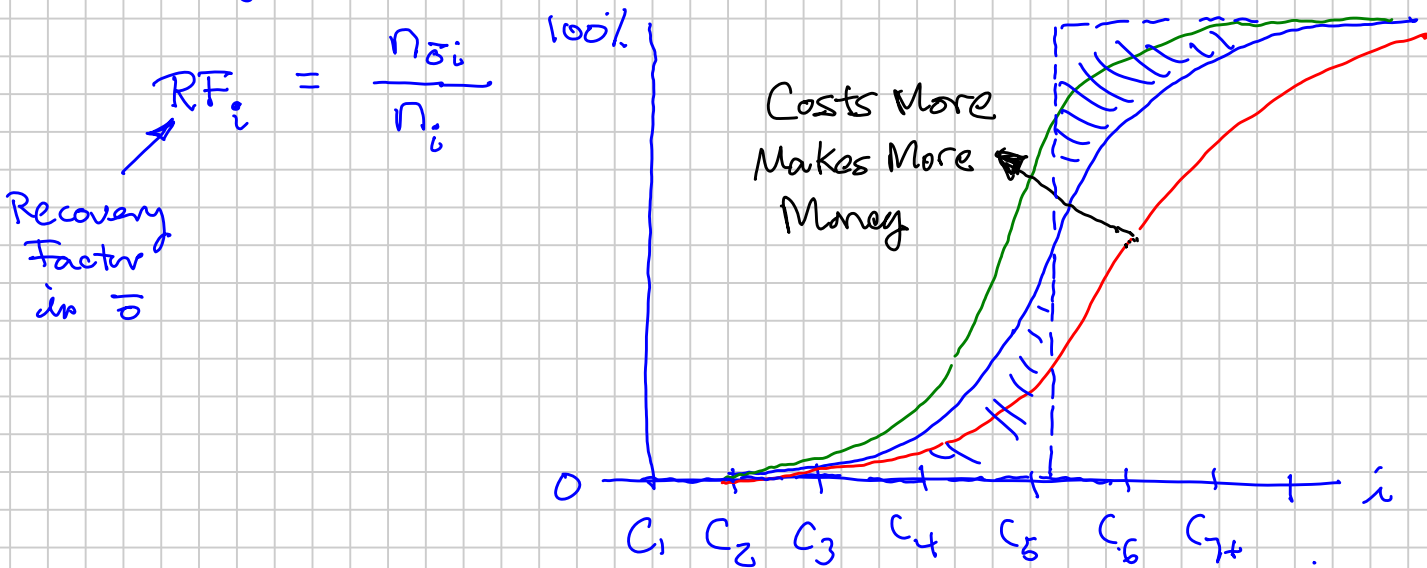
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~ Relationship between GOR (OGR) and  $z_i$



$$n_i = n \cdot z_i$$

Purpose of  $\mathbb{F}$  to maximize the moles  $n_o$  ( $n_{oi}$ )



Normal 2-3 stage  $\mathbb{F}$

$$\bar{g} \approx C_{4-} \quad (\bar{o}) \approx (C_{5+})$$

$$C_{5-} \quad (C_{6+})$$

~ 1-stage  
 ~ 2-stage  $\mathbb{F}$   
 ~ more efficient  $\mathbb{F}$

GOR  $\sim z_{n+}$  simple, but 1st order accurate  
 OGR

$$\text{OGR} \equiv \frac{V_o}{V_g}$$

Assume  $\bar{o} = C_{n+}$  e.g.  $C_{5+}$  or  $C_{6+}$

$$V_o = n_o \cdot \left( \frac{M_o}{\rho_o} \right)$$

$$V_g = n_g \cdot \left( \frac{RT_{sc}}{p_{sc}} \right)$$

assume ideal gas at STC

$$23.68 \text{ Sm}^3/\text{kg-mole}$$

$$379.5 \text{ scf/lb-mole}$$

$$\frac{0.08314 (15.56 + 273.15)}{1.0135}$$

$$\frac{10.7315 (60 + 459.67)}{14.696}$$

$$14.696$$

$n = 1$  mole (arbitrary choice)

$$n_o = n \cdot \underbrace{z_{n+}}_{\text{"oil"}} = z_{n+}$$

$$n_g = 1 - n_o = 1 - z_{n+}$$

$$\text{OGR} = \frac{V_o}{V_g} = \frac{z_{n+} (M/\rho)_{n+}}{(1 - z_{n+}) (RT_{sc}/p_{sc})} = \left( \frac{z_{n+}}{1 - z_{n+}} \right) \cdot \text{Constant}$$

Ch. 3 Cragoe  $M \sim \rho$  of SW

$$\frac{(M/\rho)_{n+}}{(RT_{sc}/p_{sc})}$$

$$M = \frac{6084}{\gamma_{API} - 5.9}$$

e.g. Crut assume  $(\gamma_{API})_{nt} \Rightarrow M_{nt}$  (Cragee)

Field Units:  $\gamma_{API} = 50 \Rightarrow \gamma_o = \frac{141.5}{131.5 + API} = 0.780$

$M_o \approx 138 \text{ lb/lb-mole}$

$\rho_o = \gamma_o \cdot \rho_w$

62.4

$= 48.65 \text{ lb/ft}^3$

$$OGR = \frac{z_{nt}}{1-z_{nt}} \cdot \frac{(138/48.65)}{379.5} \cdot \frac{\cancel{\text{ft}^3}}{\cancel{\text{ft}^3}} \cdot \frac{10^6 \cancel{\text{ft}^3}}{\text{MMscf}} \cdot \frac{\text{STB}}{5.615 \cancel{\text{ft}^3}}$$

$OGR = \frac{z_{nt}}{1-z_{nt}} \cdot 1331$

50° API  
Lean GC 0.01 Rich/NCGC 0.15

Gas Condensate  $z_{nt} \sim 1 \text{ mol-%} \rightarrow 15 \text{ mol-%}$   
 $C_5+$

$13 \frac{\text{STB}}{\text{MMscf}}$

$235 \frac{\text{STB}}{\text{MMscf}}$

Ekofisk  $\gamma_{API} \sim 36$

$$GOR = \frac{1-z_{nt}}{z_{nt}} \cdot \frac{379.5 \text{ ft}^3}{(M/\rho)} \cdot \frac{5.615 \cancel{\text{ft}^3}}{\text{STB}} \left[ \frac{\text{scf}}{\text{STB}} \right]$$

OILS  $\cancel{\text{ft}^3}$

$\gamma_{API} \sim 25-45$

$\text{Sm}^3 / \text{M Sm}^3$

$\text{Sm}^3 / 10^6 \text{ Sm}^3$

Homework Exercise: develop  $OGR = f(z_{nt})$  metric

$GOR$

Given  $\gamma_{API}$

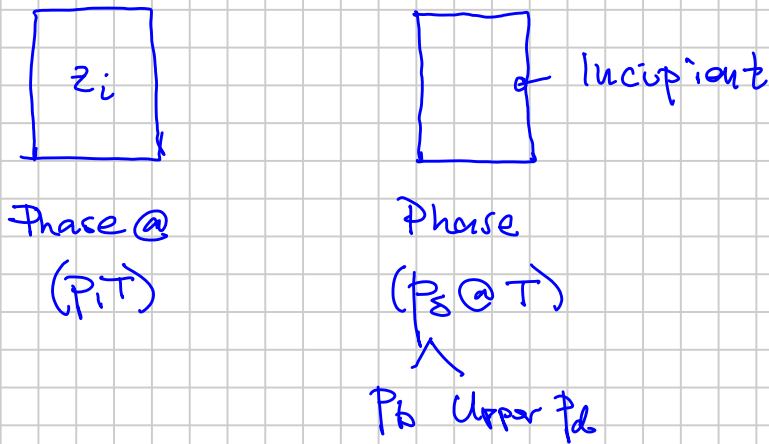
$\text{Sm}^3 / \text{Sm}^3$

2-component

...  $GOR / OGR \sim$  represent the "composition"

# SATURATED vs UNSATURATED FLUID STATES

One phase saturated or unsaturated w.r.t another phase.



Traditional definition is relative to the incipient phase.

Saturated : If  $p = p_s @ T$

$\Rightarrow$  Two phases in equilibrium @  $(p_i, T)$

Undersaturated : If  $p > p_s @ T$

$\Rightarrow$  Only one phase

Alternative meaning in gas EOR

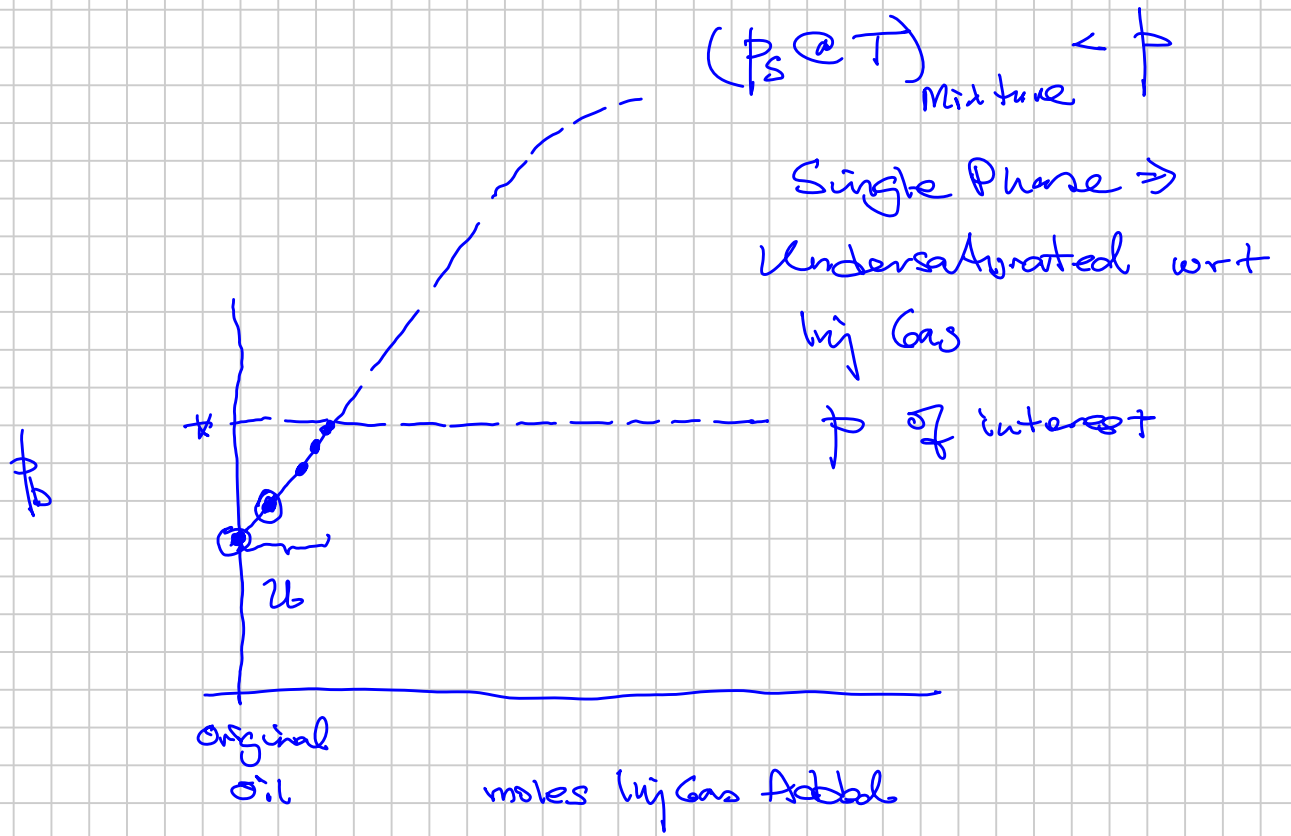
Is my reservoir fluid saturated w.r.t injected gas



+  $\in$  inj. gas  $\Rightarrow$

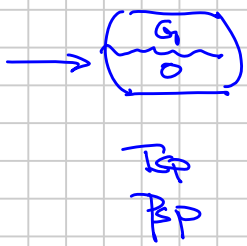


If Two-Phase  $\Rightarrow$  "Saturated"



Gas/Oil Contact  $p_{RGOC} = p_{OGOC} = p_{DOGOC}$   
 SATURATED GAS-OIL SYSTEM @ GOC

GOC  $p_R > p_s$  (all depths)  
 UNDERSATURATED FLUID SYSTEM



Acutys have a saturated oil  
 & a saturated gas

Two equilibrium phases are always saturated with each other!