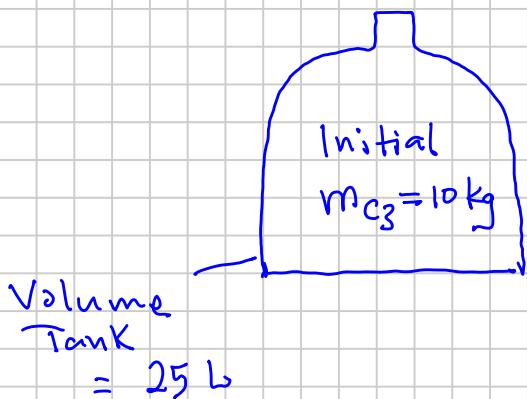


Qs related to 1-component p-T, p-V diagrams
2-component — " —

@ End of each usage



Known:

$$(a) T_{\text{outside}} \sim T_{\text{tank, inside}}$$

(b) m_{C3} (cumulative) used up

$$m_{C3} = 10 \text{ kg}$$

$$V_{C3} = 25 \text{ L} \cdot \frac{\frac{m^3}{1000 \text{ L}}}{\underbrace{x 1}} = 0.025 \text{ m}^3$$

Initially (no usage)

(a) p

Use ideal gas eq.- need T?

(c) γ_g / γ_t

Hints: Conserve!

Assume 1 Ask

$$\boxed{T = 0^\circ\text{C}}$$

- Either: Gas + Liquid $\dot{p} = p_v(T)$, Use Table
Gas-like $\dot{p} \approx nRT$

Liquid-Like

$$T = 0^\circ\text{C} \quad p_v = 4.769 \text{ bara}$$

$$m = 10 \text{ kg} = m_g + m_L$$

$$V \approx 0.025 \text{ m}^3 = V_g + V_L$$

(T, p_v) @

$$\left\{ \begin{array}{l} \rho_L = \frac{m_L}{V_L} = 527.22 \text{ kg/m}^3 \\ \rho_g = \frac{m_g}{V_g} = 10.325 \text{ kg/m}^3 \end{array} \right.$$

Assume all $(1-\epsilon_g)$ is Liquid $\Rightarrow V_L^* = 0.018 \text{ m}^3$

Assume all $(1-\epsilon_L)$ is Gas $\Rightarrow V_g^* = 0.97 \text{ m}^3$

$V_L^* < V_{\text{tank}} < V_g^*$

- Check
 \Rightarrow 2-phases

$$0.025 \text{ m}^3 = V_{\text{tank}} = V_L + V_g$$

$$m_L / \rho_L + m_g / \rho_g$$

Amran

$$\frac{m_L}{\rho_L} + \frac{(m - m_L)}{\rho_g} = 0.025$$

$$\Rightarrow m_L \Rightarrow m_g$$

$$\frac{V_L}{\rho_L} \quad \frac{V_g}{\rho_g}$$

$$V_g^* < V_{\text{tank}} \Rightarrow p < p_v(T)$$

Problem 1 – Gas Grill Propane Tank Depletion

Consider a domestic outdoor grilling propane (C_3) tank with 10 kg of propane filling a 25 L (liter) container.

Determine the following quantities at the end of each usage of the grill, where the cumulative amount removed is given as a percentage of the initial propane mass in the tank – e.g. 2%, ... 28%, ... 92%, for an arbitrary number of usages until the tank “runs empty”.

Known after each usage:

- (a) Outdoor (tank) temperature ($^{\circ}\text{C}$); could vary after each usage (ranging from -20°C to $+60^{\circ}\text{C}$).
- (b) Cumulative propane used (% of mass initially in tank).

To be calculated after each usage:

- (a) Pressure in the tank.
- (b) Mass propane remaining in the tank (kg).
- (c) Gas volume as a % of tank volume.
- (d) Whether the tank has two phases or one phase (1 or 2); if 1, which phase (gas or liquid).

Plot tank pressure (left y-axis) and liquid vol-% (right y-axis) in tank versus cumulative propane mass consumed.

The properties of propane are estimated by the Soave-Redlich-Kwong (SRK) equation of state model as given in Table 1. Using the three hints below, find simple equations that give the vapor pressure and phase densities as a function of temperature or vapor pressure.

Hint 1. Fit all of the vapor pressure “data” in Table 1 to the Antoine equation given by $p_v(T)=A-B/(C+T)$, where you minimize the sum of squares of $\Delta p_v=(p_v^{\text{Antoine}} - p_v^{\text{Table}})$ by changing A, B, and C. Use this (your) custom best-fit Antoine equation to solve the problem above.

Hint 2. Use Excel Trend Line to fit the gas density “data” (only up to 60°C) in Table 1 as a linear function of pressure and zero intercept. What do we call this best-fit equation?

Hint 3. Use Excel Trend Line to fit the liquid density “data” (only up to 60°C) in Table 1 to a 2nd-degree polynomial in temperature.

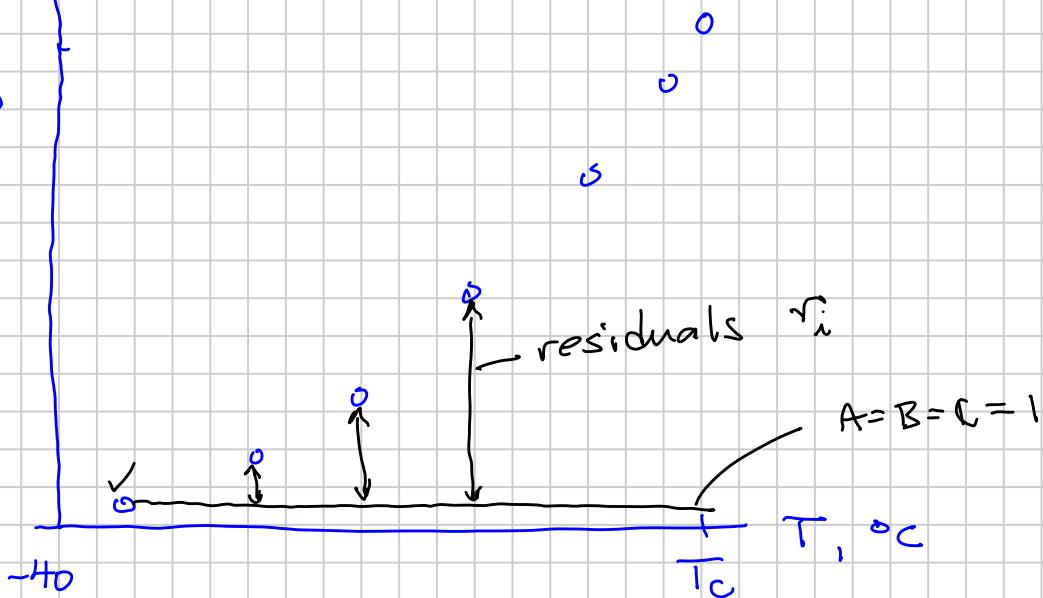
Least Squares Non-Linear Regression

"Best Fit" on equations to "data"

$$P_V = A - B / (T + C)$$

P_V
} P_V
(barra)

Table 1 - (ols. 1 ≠ 2)

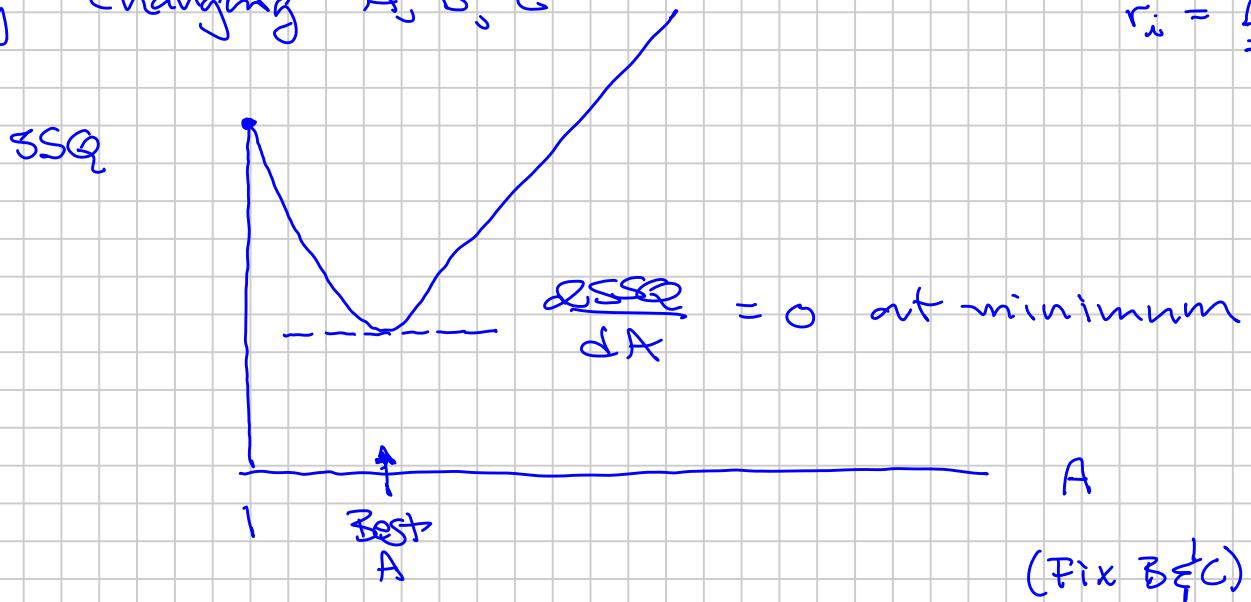


Model Data

$$SSQ = \sum r_i^2 = \sum \frac{(P_V^A - P_V^{\text{Table}})^2}{P_{V,\text{ref}}^2}$$

min by changing A, B, C

Reference Value
e.g. P_V^{Table}
 $r_i = \Delta_i$



$$\log_{10} p_v \left[\frac{\text{mmHg}}{\text{bar}} \right] = [A' - B' / (C' + T_c)]$$

$$\log_{10} p_v [\text{bar}] \cdot \underbrace{\frac{\text{mmHg}}{0.00133 \text{ bar}}}_{=} = A' - B' / (C' + T_c)$$

$$\log_{10} p_v [\text{bar}] - \log_{10} (0.00133) = A' - B' / (C' + T_c)$$

$$\log_{10} p_v [\text{bar}] = \underbrace{[A' + \log(0.00133)]}_{A} - B' / (C' + T_c)$$

Gas Density Model:

$$p V_g \approx n_g R T \quad m_g = n_g \cdot M_g$$

$$\rho_g = \frac{m_g}{V_g}$$

$$p V_g = \left(\frac{m_g}{M_g} \right) R T \Rightarrow \frac{m_g}{V_g} = \frac{p M_g}{R T}$$

$$\rho_g \approx \left(\frac{M_g}{R T} \right) \cdot p$$

$$\rho_g \approx a \cdot p ?$$

$$p \Leftarrow \begin{cases} T \\ M_g \\ V_g = V_{\text{tank}} \\ \rho_g = \frac{m_g}{V_{\text{tank}}} \end{cases} \quad \dots$$

$$f : \underline{\underline{1(G)}}$$

$$\rho_g \approx \frac{M_g}{R T} p$$

$$[p] = \left(\frac{m_g}{V_{\text{tank}}} \right) \cdot \frac{R T}{M_g}$$

\textcircled{R}, T, M_g

$R = 0.08314$ bar, K, m³, kg-mole
(kmol)