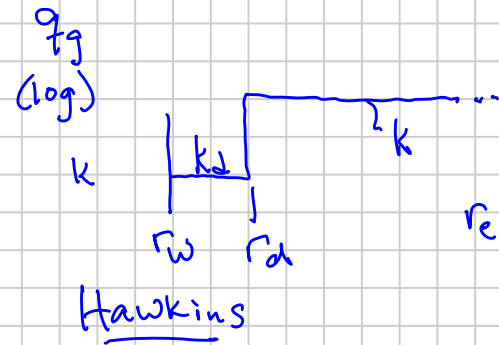


$$(AOF)_{BPE} \geq (AOF)_{FE}$$

? ?

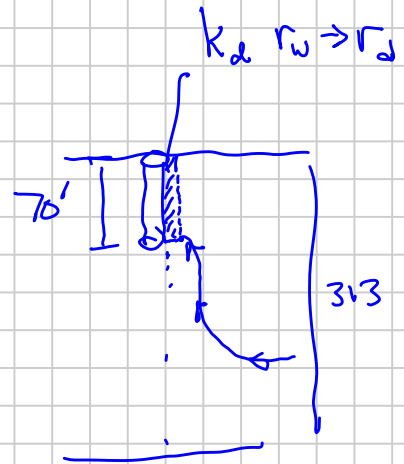


$$Z = S_d = \left(\frac{k}{k_d} - 1 \right) \ln \frac{r_d}{r_w}$$

$$\left. \begin{aligned} (S_d) &= +22.8 \\ S_b &= +17? \end{aligned} \right\} = \underbrace{S_d \cdot \frac{1}{b}}_{23-17=+6} + S_b$$

S_d

Pre-Cleanup: $S_2 \sim +68 = S_d \cdot \frac{1}{b} + S_b$



$$q = C (\Delta p^2)^n$$

$$\Delta p^2 = \frac{1}{C^{1/n}} q^{1/n}$$

TrendLine Power eq.

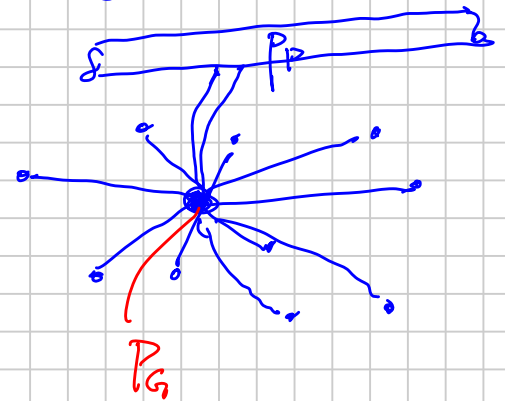
$$x = q$$

$$y = \Delta p^2$$

$$y = \alpha \cdot x^\beta$$

$$\alpha = \frac{1}{C^{1/n}} \quad \beta = 1/n$$

Large (offs hore)
Gas Field Development :



Long-term Gas Purchase Contract

DCQ = Daily Contract Rate (with ±10-20 swing)

$$q_{GF} = \sum_{w=1}^{N_w(t)} q_{gw}(t)$$

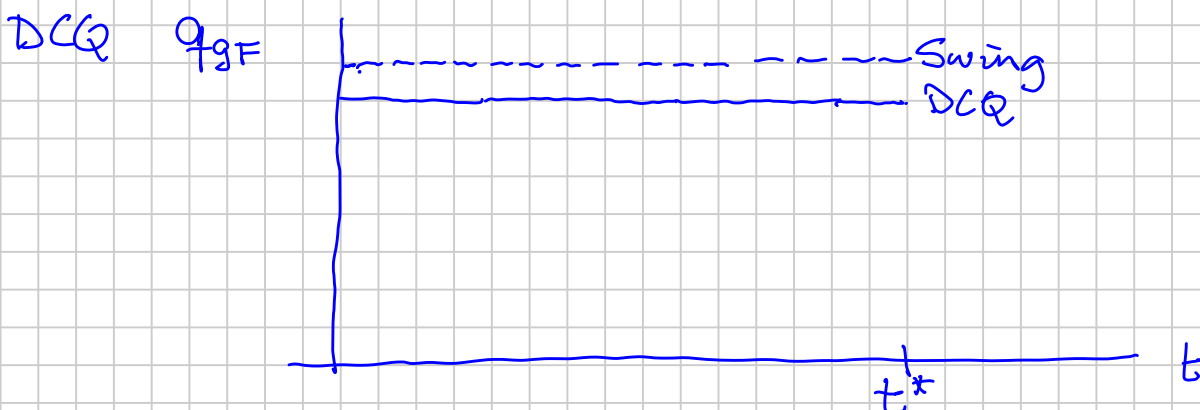
A_w & B_w : Are Wellhead or Gathering-Point Constants
 R
 T
 q

$$q_{gw} = \frac{-A_w + [A_w^2 + 4B_w \Delta p^2]^{0.5}}{2B_w}$$

$$\Delta p^2 = \underbrace{p_c^2(t)}_{\text{"Pc"}} - \underbrace{p_g^2}_{\text{Constant}} = p_p$$

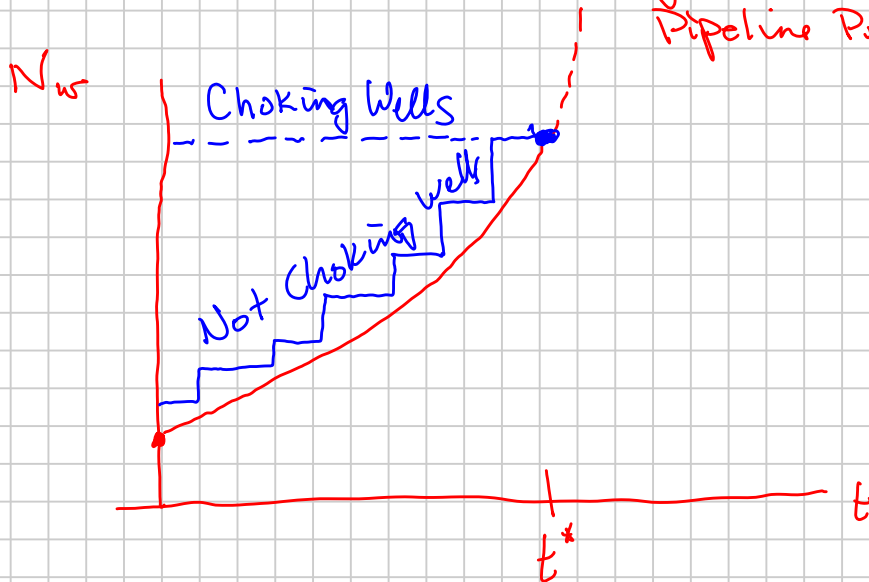
No Compress Min Wells Required (No Choke)

t^* Contract Delivery Period : 5-15 (20) years



$$\text{min. } N_w(t) = \frac{DCQ}{\sum q_{gw} (p_G = \text{const.})}$$

No Choke
Against
Pipeline Pressure



FAF(N) \neq FAF(R) \neq Isochronal \Rightarrow

$$A = () \left[\underbrace{p_D(t_D)} + s \right]$$

Superposition is
not required

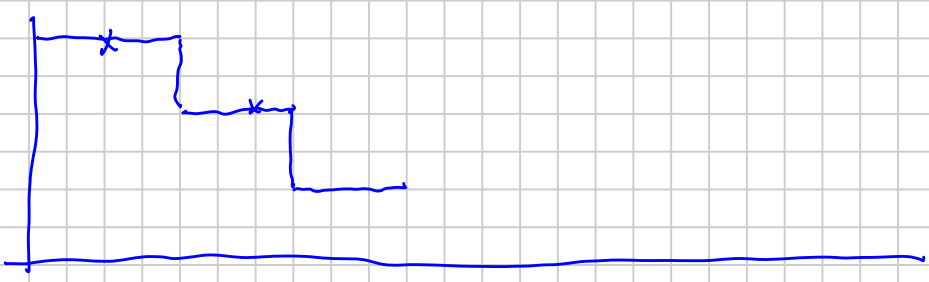
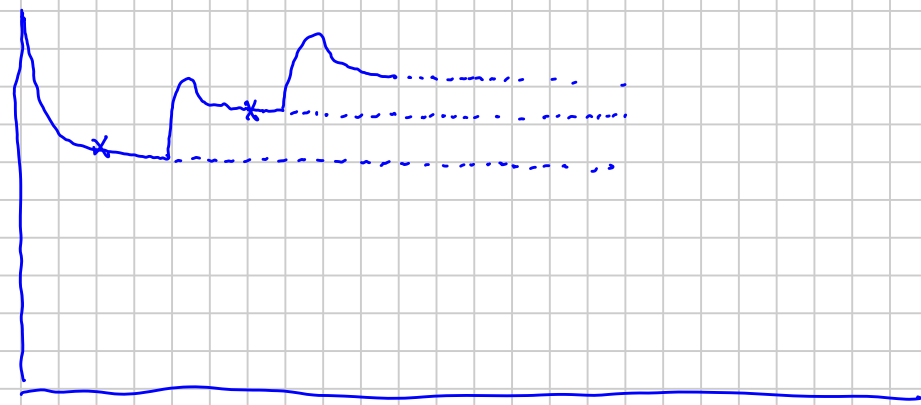
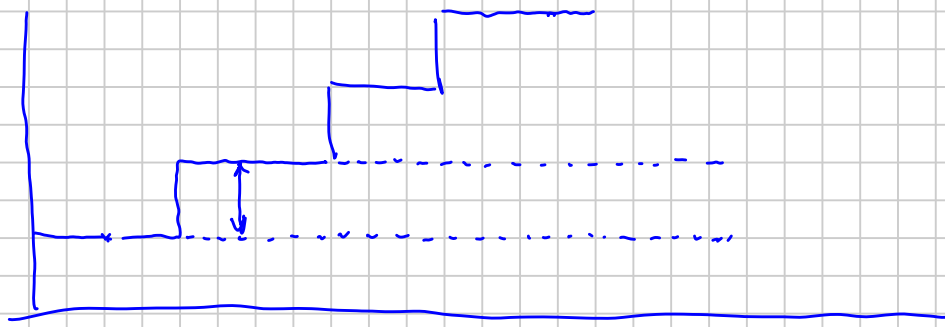
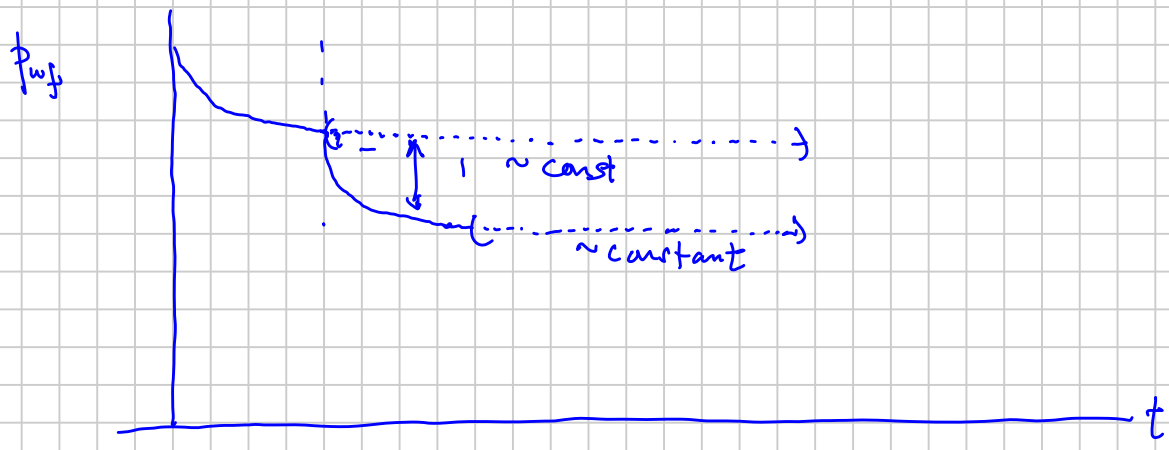
① Needs to be the same at
"t_D" used (e.g. @ 4 hr)

② All infinite-acting
transients from earlier
rates & shut-ins need
to have "died out"

"Lower" - k wells often
violate ②

When does FAF satisfy (2)

higher $k > 100 \text{ md}^{-1}$ - D_s



NORMAL ISOCHRONAL TEST

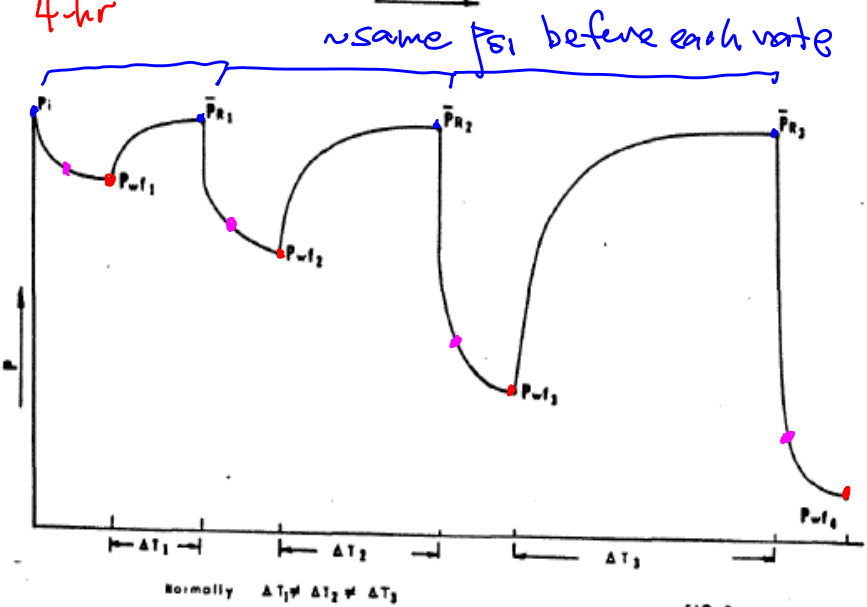
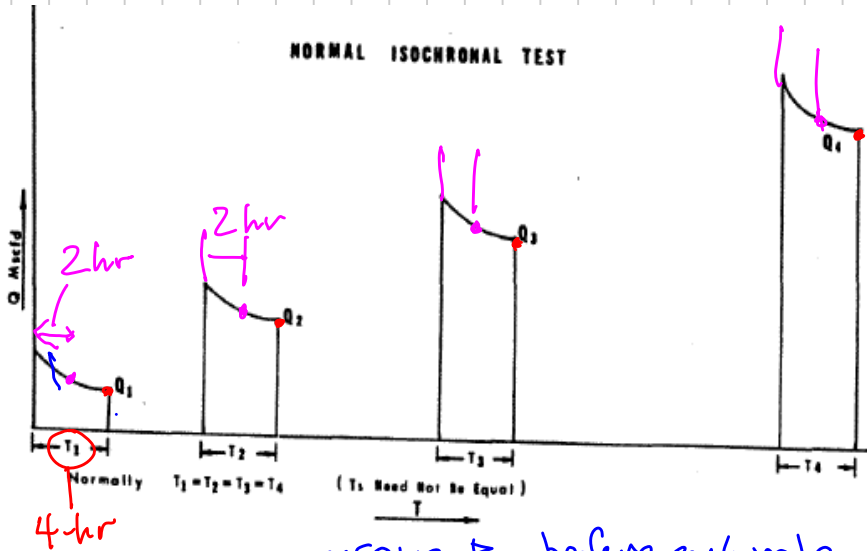


FIG. 3

Winestock & Golpitts

Const

$$P_i - P_{wf}(t) = C \cdot q \cdot P_0(t_0)$$

DTA

$$P_i - P_{wf}(t) \approx C \cdot q(t) \cdot P_0(t_0)$$

IF $P_{wf}(t)$ & $q(t)$ are smoothly varying functions of time

