**3.3.5 Gas Viscosity.** Viscosity of reservoir gases generally ranges from 0.01 to 0.03 cp at standard and reservoir conditions, reaching up to 0.1 cp for near-critical gas condensates. Estimation of gas viscosities at elevated pressure and temperature is typically a two-step procedure: (1) calculating mixture low-pressure viscosity  $\mu_{gsc}$  at  $p_{sc}$  and T from Chapman-Enskog theory<sup>3,6</sup> and (2) correcting this value for the effect of pressure and temperature with a corresponding-states or dense-gas correlation. These correlations relate the actual viscosity  $\mu_{gsc}$  or difference ( $\mu_g - \mu_{gsc}$ ) as a function of pseudoreduced properties  $p_{pr}$  and  $T_{pr}$  or as a function of pseudoreduced density  $\rho_{pr}$ .

Gas viscosities are rarely measured because most laboratories do not have the required equipment; thus, the prediction of gas viscosity is particularly important. Gas viscosity of reservoir systems is often estimated from the graphical correlation  $\mu_g/\mu_{gsc} = f(T_r, p_r)$ proposed by Carr *et al.*<sup>42</sup> (**Fig. 3.11**). Dempsey<sup>43</sup> gives a polynomial approximation of the Carr *et al.* correlation. With these correlations, gas viscosities can be estimated with an accuracy of about  $\pm 3\%$  for most applications. The Dempsey correlation is valid in the range  $1.2 \leq T_r \leq 3$  and  $1 \leq p_r \leq 20$ .

The Lee-Gonzalez gas viscosity correlation (used by most PVT laboratories when reporting gas viscosities) is given by<sup>44</sup>

$$\mu_g = A_1 \times 10^{-4} \exp(A_2 \rho_g^{A_3}), \qquad (3.65a)$$

where  $A_1 = \frac{(9.379 + 0.01607M_g)T^{1.5}}{209.2 + 19.26M_g + T}$ ,

$$A_2 = 3.448 + (986.4/T) + 0.01009M_g,$$

and  $A_3 = 2.447 - 0.2224A_2$ , ..... (3.65b)

with  $\mu_g$  in cp,  $\rho_g$  in g/cm<sup>3</sup>, and *T* in °R. McCain<sup>19</sup> indicates the accuracy of this correlation is 2 to 4% for  $\gamma_g < 1.0$ , with errors up to 20% for rich gas condensates with  $\gamma_g > 1.5$ .