Spatial reservoir characterization using the dilation factor α

Kenneth Duffaut (Interpretation of Geophysical Data (IGD))

Faculty of Engineering Science and Technology Department of Petroleum Engineering and Applied Geophysics RoSe meeting, Trondheim, 28th April, 2015



Outline

- Introduction
- Spatial traveltime analysis a new application?
- Geological scenarios and numerical examples
- Conclusions



Introduction 4D or time-lapse traveltime analysis

$$t_0(x_0) = \frac{2z(x_0)}{v_{p0}(x_0)}$$

 $\frac{\Delta t_0(x_0)}{t_0(x_0)} \approx \frac{\Delta z(x_0)}{z(x_0)} - \frac{\Delta v_{p0}(x_0)}{v_{p0}(x_0)}$

(Landrø and Stammeijer 2004)

Layer unit
$$v_{p0}(x_0) z(x_0)$$

= two-way vertical time thickness of unit

_b = coordinate position along a line

= vertical P-wave velocity of unit = changes in physical parameters

and R = ratio between relative velocity

= thickness of formation unit

nd thickness changes

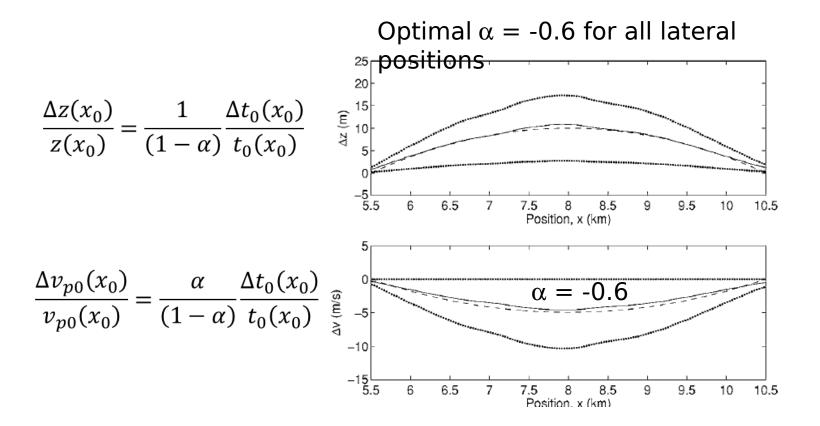
$$\frac{\Delta v_{p0}(x_0)}{v_{p0}(x_0)} = \alpha \frac{\Delta z(x_0)}{z(x_0)}$$

$$\frac{\Delta v_{p0}(x_0)}{v_{p0}(x_0)} = -R \frac{\Delta z(x_0)}{z(x_0)}$$

(Hatchell et al., 2005)

Assuming uniaxial deformation **DINTNU**

Introduction Relative changes in layer thickness and velocity



(Figure courtesy: Røste et al., 2006)

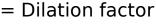


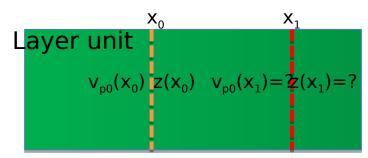
Spatial zero offset traveltime analysis

= two-way vertical time thickness of unit at x_0

= coordinate reference position along a line

- = a new coordinate position along the line
- = thickness of formation unit
- $_{0}$ = vertical P-wave velocity of unit
- = spatial difference in physical parameters





$$t_0(x_0) = \frac{2z(x_0)}{v_{p0}(x_0)}$$

$$\frac{\Delta t_0(x_1, x_0)}{t_0(x_0)} \approx \frac{\Delta z(x_1, x_0)}{z(x_0)} - \frac{\Delta v_{p0}(x_1, x_0)}{v_{p0}(x_0)}$$

$$\frac{\Delta v_{p0}(x_1, x_0)}{v_{p0}(x_0)} = \alpha(x_0) \frac{\Delta z(x_1, x_0)}{z(x_0)}$$

Assuming uniaxial deformation **D**NTNU

Porosity-strain relation Assume only changes in pore volume

Porosity
$$\varphi = \frac{V_b - V_s}{V_b} = 1 - \frac{V_s}{V_b}$$
 Solid volume
Bulk volume

Rewritting we get

$$\frac{V_s}{V_b} = 1 - \varphi$$

Differentiation gives

$$\frac{d\varphi}{dV_{b}} = \frac{V_{s}}{V_{b}^{2}} \Longrightarrow d\varphi = \frac{V_{s}}{V_{b}} \frac{dV_{b}}{V_{b}} \quad \text{where} \quad \frac{dV_{b}}{V_{b}} = \epsilon_{vol}$$

We get porosity-strain relation

$$\frac{d\varphi}{(1-\varphi)} = \epsilon_{vol}$$



Spatial varying layer thickness and velocity Relative changes in layer thickness and velocity

$$\frac{\Delta z(x_{1,}x_{0})}{z(x_{0})} = \frac{1}{(1-\alpha(x_{0}))} \frac{\Delta t_{0}(x_{1,}x_{0})}{t_{0}(x_{1,}x_{0})}$$

$$\frac{\Delta v_{p0}(x_{1,}x_{0})}{v_{p0}(x_{0})} = \frac{\alpha(x_{0})}{\left(1 - \alpha(x_{0})\right)} \frac{\Delta t_{0}(x_{1,}x_{0})}{t_{0}(x_{1,}x_{0})}$$

$$\frac{\Delta v_{p0}(x_1, x_0)}{v_{p0}(x_0)} = \alpha(x_0) \frac{\Delta \varphi(x_1, x_0)}{(1 - \varphi(x_0))}$$



Dilation factor in clean and shaly sandstone Uniaxial deformation

Clean sandstone

$$v_{p0} = a - b\phi$$

 $\frac{d\phi}{(1-\phi)} = \frac{dz}{z}$

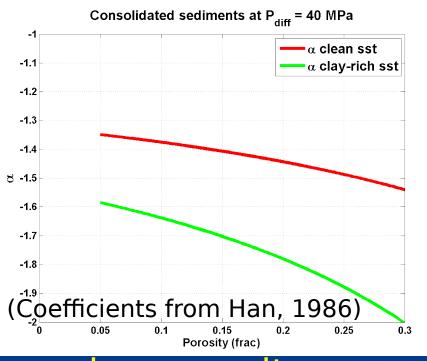
$$\frac{\Delta\varphi}{(1-\varphi)} = \frac{1}{\alpha} \frac{\Delta v_{p0}}{v_{p0}}$$

$$\alpha = \frac{(a-b)}{v_{p0}} - 1$$
 (Røste et al., 2006)

Clay-rich sandstone

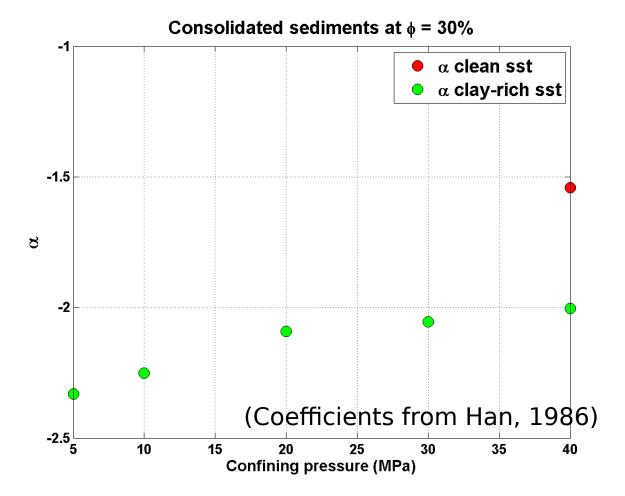
$$v_{p0} = \mathbf{a} - \mathbf{b}\boldsymbol{\varphi} - \mathbf{c}\boldsymbol{v}_{cl}$$

$$lpha=rac{(arphi-1)b}{v_{p0}}$$
 (Carcione et al., 2007



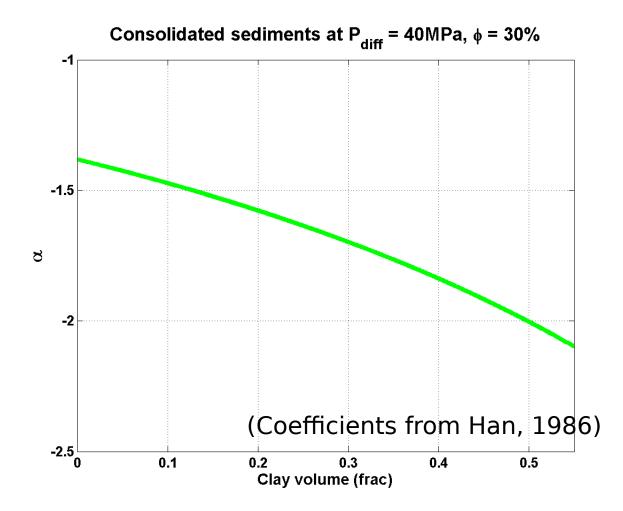
α decreases with decreasing porosity \square NTNU

Dilation factor vs. stress Clean and clay-rich sandstone



α decreases with increasing net stress NTNU

Dilation factor vs. volume of clay



α decreases with decreasing clay content of the second second

Geological scenarios - numerical examples

- Plausible geological reasons causing spatially variation in layer thickness and velocity in a unit
 - Equal depositional layer thickness followed by 'differential compaction" or diagenetic effects within a formation unit
 - Erosion
 - Lithology changes
 - clean vs. shaly sandstone

Assume net stress = 40 MPa in all three cases NU

Spatial porosity and thickness change within unit Differential compaction of clean sandstone

x_0 location with a well		x_1 location without a well	
φ = 24%	Z = 33m	φ = 20% Z = 31m	

 $v_{p0}(x_0) = 6.08 - 8.06 * 0.24 \sim 4146 m/s$

$$t_0(x_0) = \frac{2z(x_0)}{V_{p0}(x_0)}$$

$$t_0(x_0) = \frac{66m}{4146m/s} \approx 0.01592s$$

$$\alpha_0 = \frac{(a-b)}{v_{p0}} - 1 = \frac{(6.08 - 8.06)}{4.146} - 1 \approx -1.48$$

 $v_{p0}(x_1) = 6.08 - 8.06 * 0.20 = 4468m/s$

$$t_o(x_1) = \frac{62m}{4468m/s} \approx 0.01388s$$



Estimates of layer thickness and velocity at new location Case: Differential compaction

Layer thickness estimate at x_1 location:

$$\frac{\Delta z(x_{1,}x_{0})}{z(x_{0})} = \frac{1}{2.48} \frac{(0.01388 - 0.01592)}{(0.01592)} \approx -0.0517$$

$$\tilde{z}(x_1) = z(x_0) + \Delta z(x_1, x_0) = 33 m - 1.71m \approx 31.3 m$$

Correctorrect= 31m

Velocity estimate at x₁ location:

$$\frac{\Delta v_{p0}(x_{1,}x_{0})}{v_{p0}(x_{0})} = \frac{-1.48}{2.48} \frac{(0.01388 - 0.01592)}{(0.01592)} \approx 0.07647$$
$$\tilde{v}_{p0}(x_{1}) = v_{p0}(x_{0}) + \Delta v_{p0}(x_{1,}x_{0}) = 4146 + 317 = 4463 \text{m/s}$$

Correct v_p of p_0 (p_0 (p_0) 4468m/s



Spatially varying layer thickness Erosion of a clean sandstone unit

$\varphi = 24\%$ Z = 33m $\varphi = 24\%$ Z = 23m	\mathbf{x}_{0} location with a well		x_1 location without a well
	φ = 24%	Z = 33m	φ = 24% Z = 23m

 $v_{p0}(x_0) = 6.08 - 8.06 * 0.24 \sim 4146 m/s$

$$t_0(x_0) = \frac{2z(x_0)}{V_{p0}(x_0)}$$

$$t_0(x_0) = \frac{66m}{4146m/s} \approx 0.01592s$$

$$\alpha_0 = \frac{(a-b)}{v_{p0}} - 1 = \frac{(6.08 - 8.06)}{4.146} - 1 \approx -1.48$$

 $t_o(x_1) = \frac{46m}{4146m/s} \approx 0.01110s$

 $v_{p0}(x_1) = 6.08 - 8.06 * 0.24 = 4146m/s$



Estimates of layer thickness and velocity at new location Case: Erosion

Layer thickness and porosity estimate at x_1 location:

$$\frac{\Delta z(x_{1,}x_{0})}{z(x_{0})} = \frac{1}{2.48} \frac{(0.01110 - 0.01592)}{(0.01592)} \approx -0.12221$$

$$\tilde{z}(x_1) = z(x_0) + \Delta z(x_1, x_0) = 33m - 4m = 29m$$

Correctorpedt= 23m

Velocity estimate at x_1 location:

$$\frac{\Delta v_{p0}(x_{1,}x_{0})}{v_{p0}(x_{0})} = \frac{-1.48}{2.48} \frac{(0.01110 - 0.01592)}{(0.01592)} \approx 0.1809$$

$$\tilde{v}_{p0}(x_1) = v_{p0}(x_0) + \Delta v_{p0}(x_1, x_0) = 4146$$
m/s + 750m/s = 3396m/s

Correct v_p of p_{10} Correct 4146m/s



Spatial varying lithology clean vs. shaly sandstone unit

\mathbf{x}_{0} location with a well		x_1 location without a well
φ = 24%	Z = 33m	φ = 12.5% Z = 28m Vcl = 30%

 $v_{p0}(x_0) = 6.08 - 8.06 * 0.24 \sim 4146 m/s \ v_{p0}(x_1) = 5.59 - 6.93 * 0.125 - 2.18 * 0.30 = 4070 m/s$

$$t_0(x_0) = \frac{2z(x_0)}{V_{p0}(x_0)}$$

$$t_0(x_0) = \frac{66m}{4146m/s} \approx 0.01592s \qquad t_o(x_1) = \frac{56m}{4070m/s} \approx 0.01376s$$

$$\alpha_0 = \frac{(a-b)}{v_{p0}} - 1 = \frac{(6.08 - 8.06)}{4.146} - 1 \approx -1.48$$

Estimates of layer thickness and velocity at new location Case: Lithological change

Layer thickness and porosity estimate at x_1 location:

$$\frac{\Delta z(x_1, x_0)}{z(x_0)} = \frac{1}{2.48} \frac{(0.01376 - 0.01592)}{(0.01592)} \approx -0.0547$$

$$\tilde{z}(x_1) = z(x_0) + \Delta z(x_1, x_0) = 33m - 1.8m \approx 31.2m$$

Correctorpedt= 28m

Velocity estimate at x_1 location:

$$\frac{\Delta v_{p0}(x_{1,}x_{0})}{v_{p0}(x_{0})} = \frac{-1.48}{2.48} \frac{(0.01376 - 0.01592)}{(0.01592)} \approx 0.081$$

 $\tilde{v}_{p0}(x_1) = v_{p0}(x_0) + \Delta v_{p0}(x_1, x_0) = 4146$ m/s + 336m/s ≈ 4482 m/s

Correct v_p (p_p) (p_p)



Conclusions

- New approach tested by estimating relative changes in layer thickness and velocity using the dilation factor (α) and spatially traveltimes differences of a unit
 - A few numerical examples are shown.
 - Only the "differential compaction" case gave good estimates of laterally variable layer thickness (porosity) and velocity
- Method depends on
 - reference location
 - porosity-strain relation of the unit
- α is not constant when assuming Han's model. It decreases as
 - Porosity decreases (clean and shaly sandstones)
 - Clay content decreases
 - Net stress increases (shaly sandstone)



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Thank you for your attention

