

Ultrasonic Studies of Stressed Sand and Clay

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Motivation

- Explore the effect of fluid substitution on anisotropic parameters
- Explore the behavior of v_p/v_s for sand and clay

Impact of fluid substitution on Anisotropy?

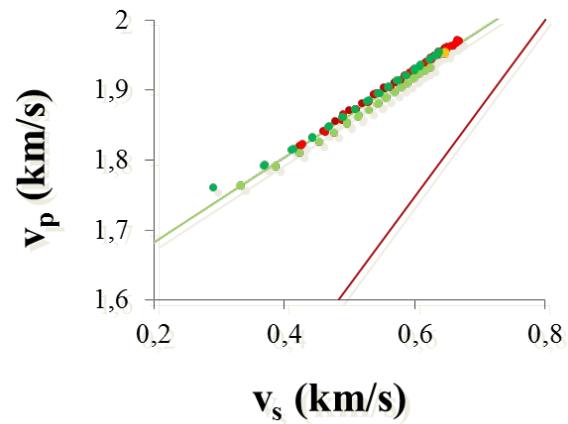
(Collett & Gurevich, 2013; Thomsen, 2012)

$$\epsilon^{\text{sat}} = \frac{L}{L^{\text{sat}}} \epsilon + \frac{a_0}{L^{\text{sat}}} \frac{((\delta - 4\epsilon)L + 4\gamma\mu)M}{3K_g}.$$

In a similar way, δ^{sat} is given by

$$\delta^{\text{sat}} = \frac{L}{L^{\text{sat}}} \delta + \frac{a_0}{L^{\text{sat}}} \frac{((\delta - 4\epsilon)L + 4\gamma\mu)M}{3K_g}.$$

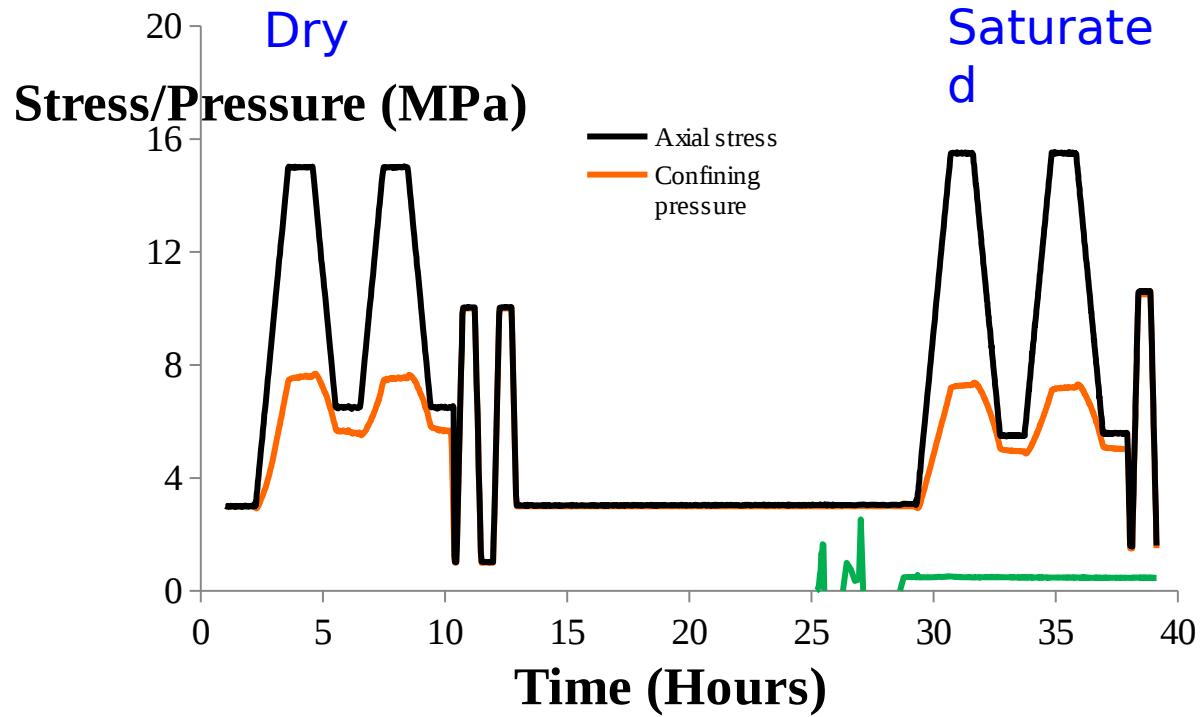
How well known v_p/v_s trends does not works for unconsolidated sediments?



Effect of fluid on anisotropic parameters

Lab tests in triaxial set-up

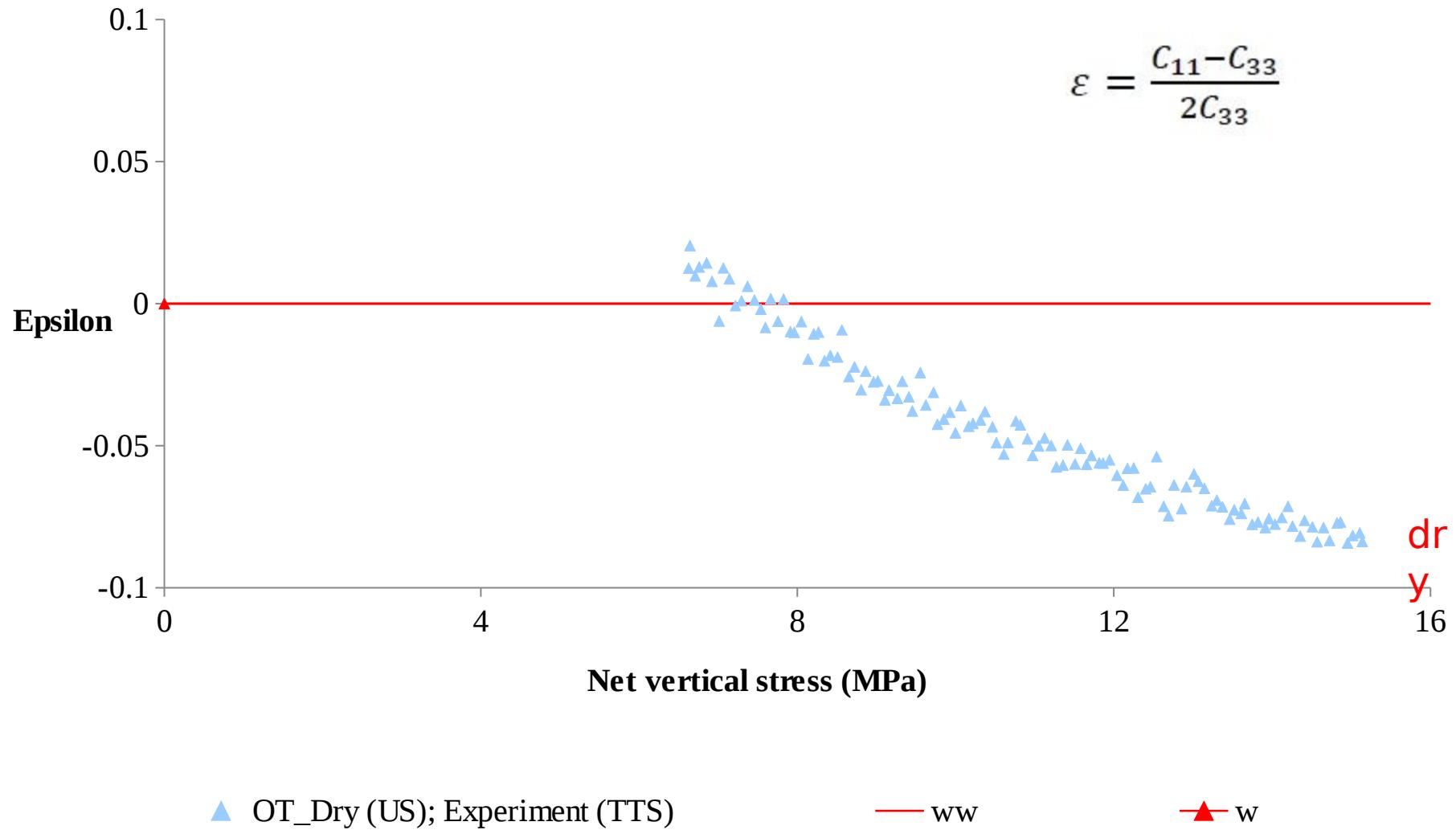
(only unsorted Ottawa sand)



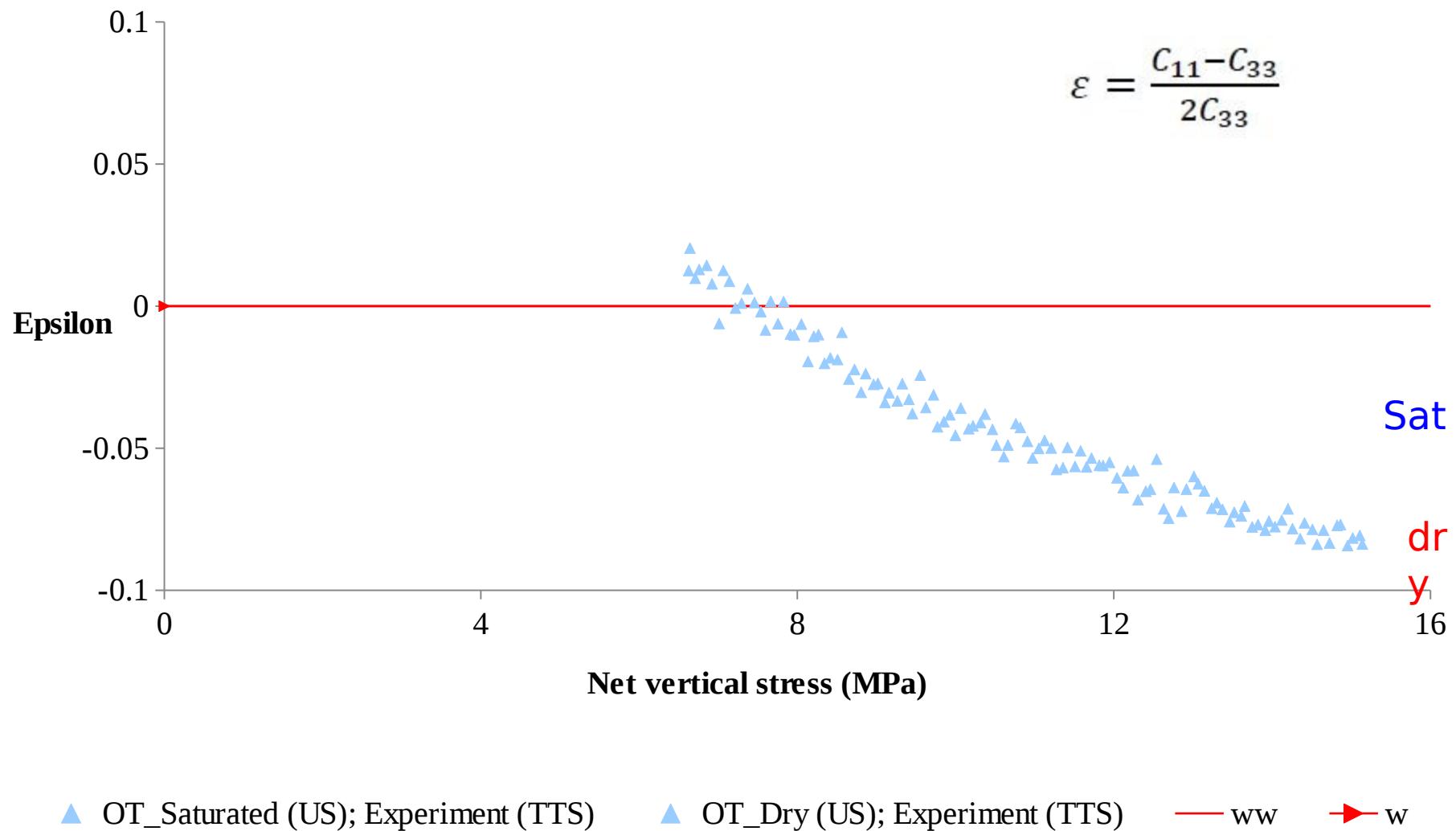
Saturated with 3.5wt%
NaCl

Multi-directional P- & S-wave velocity measurements permit determination of all 5 TI elastic stiffness parameters => Thomsen's ϵ , γ , δ (+ η)

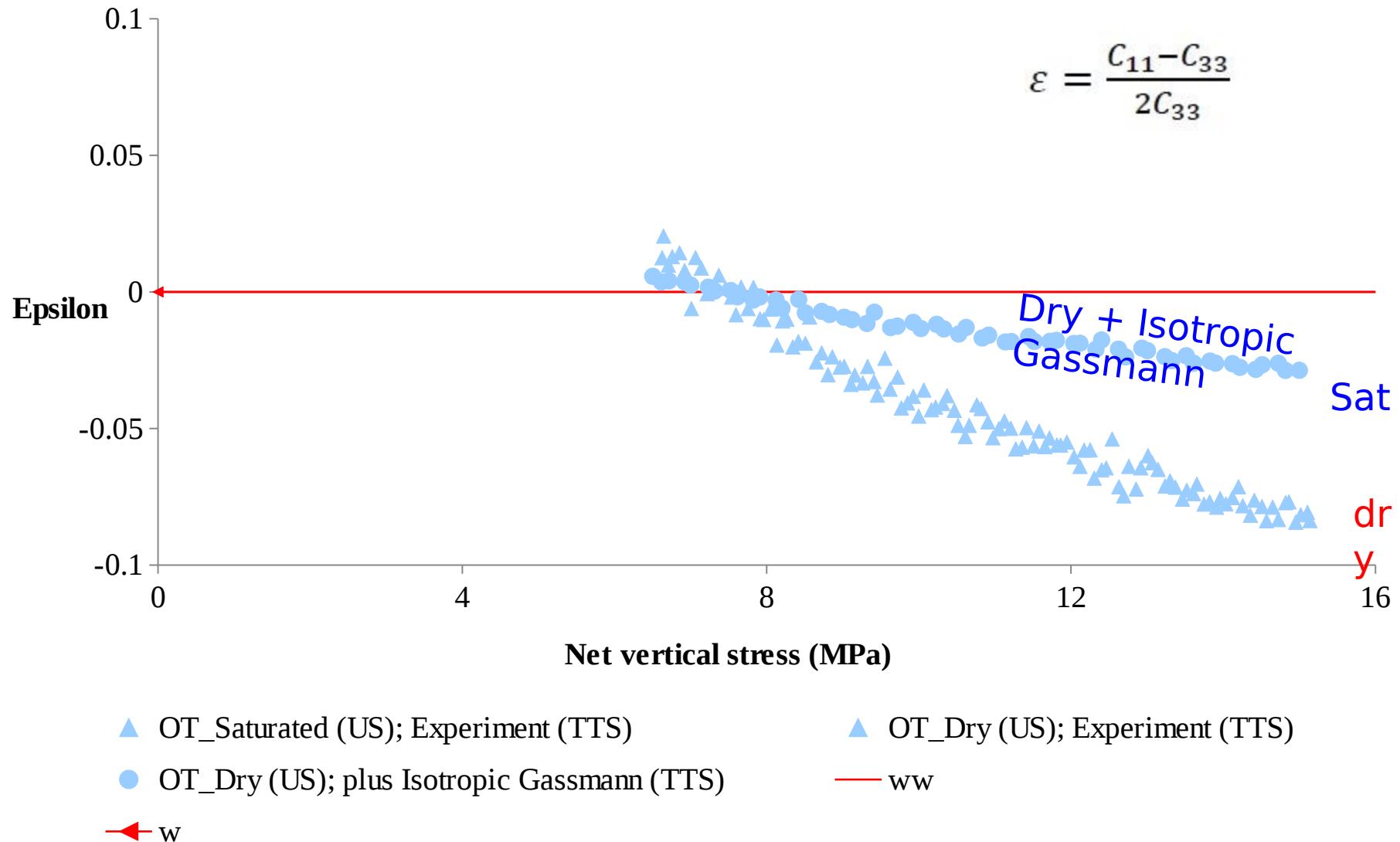
Effect of fluid on Epsilon (Uniaxial strain condition)



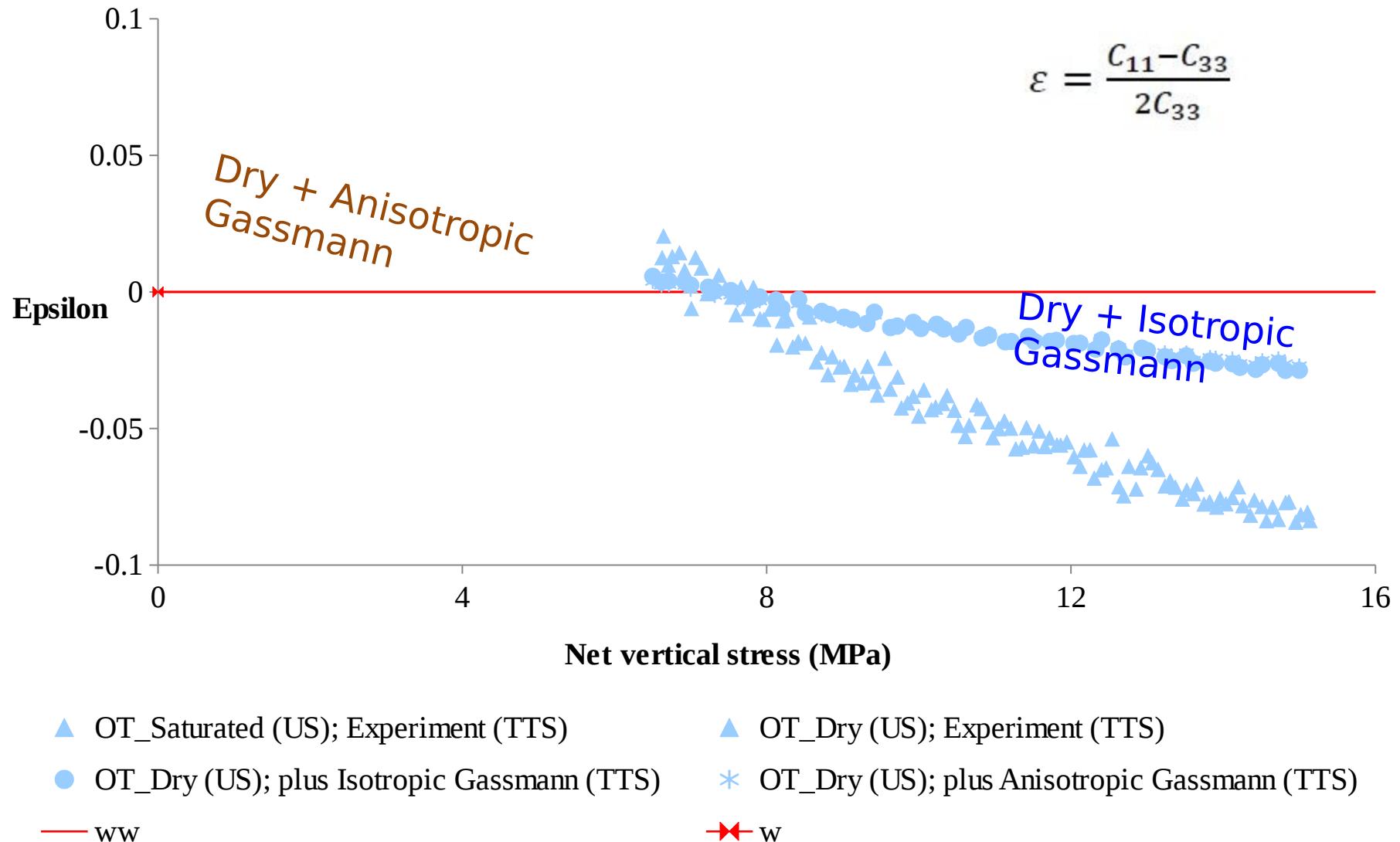
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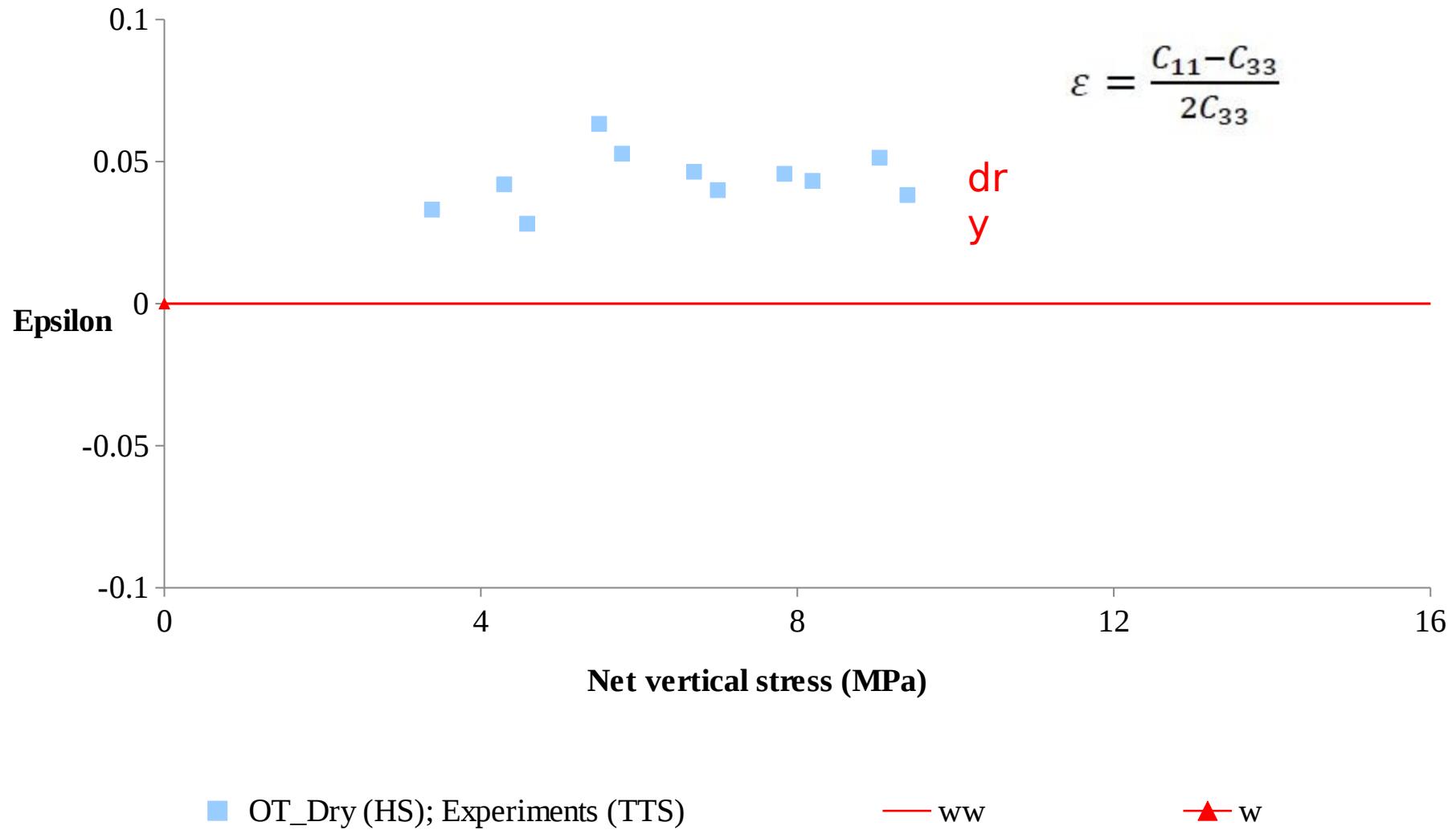
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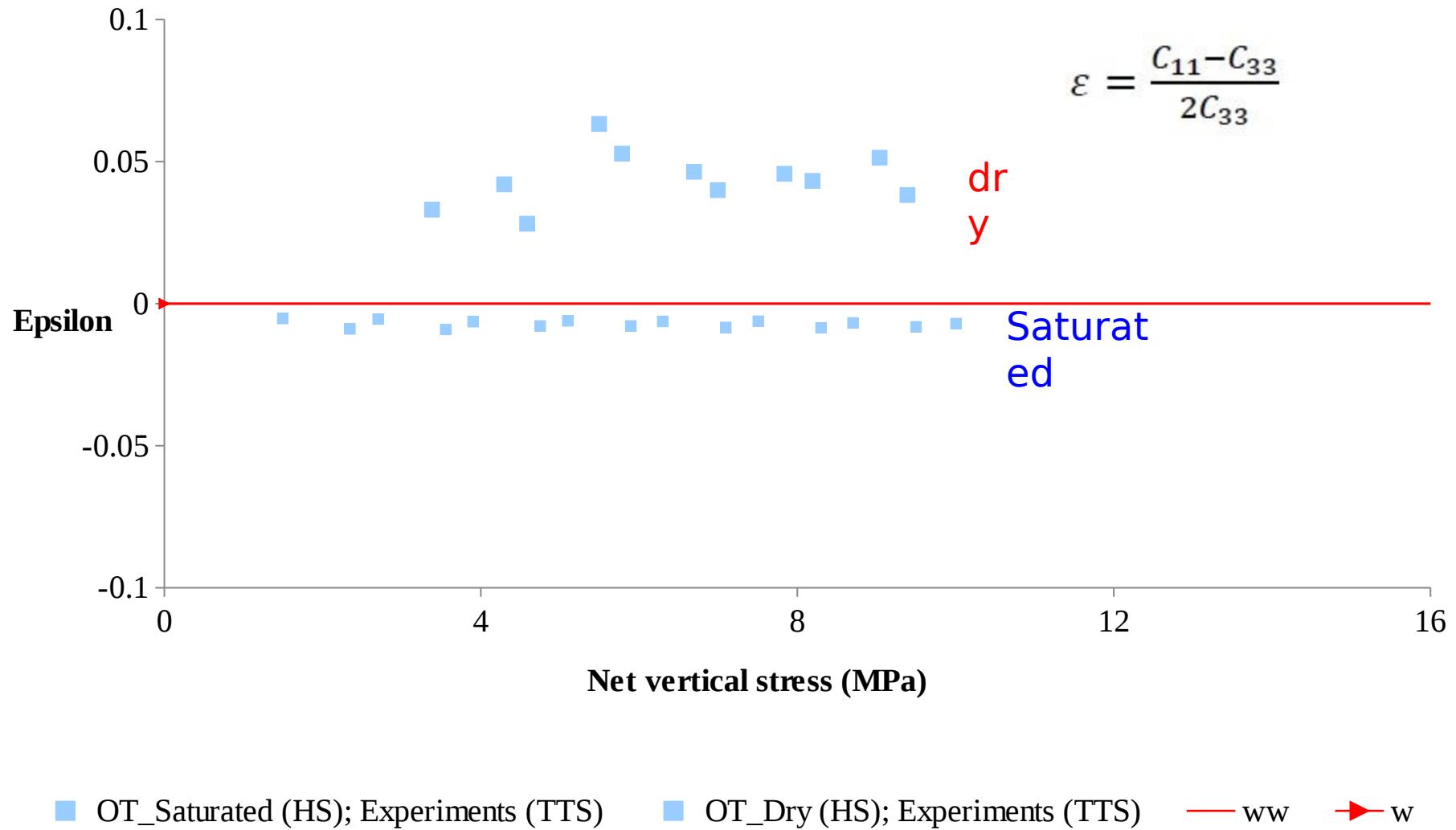
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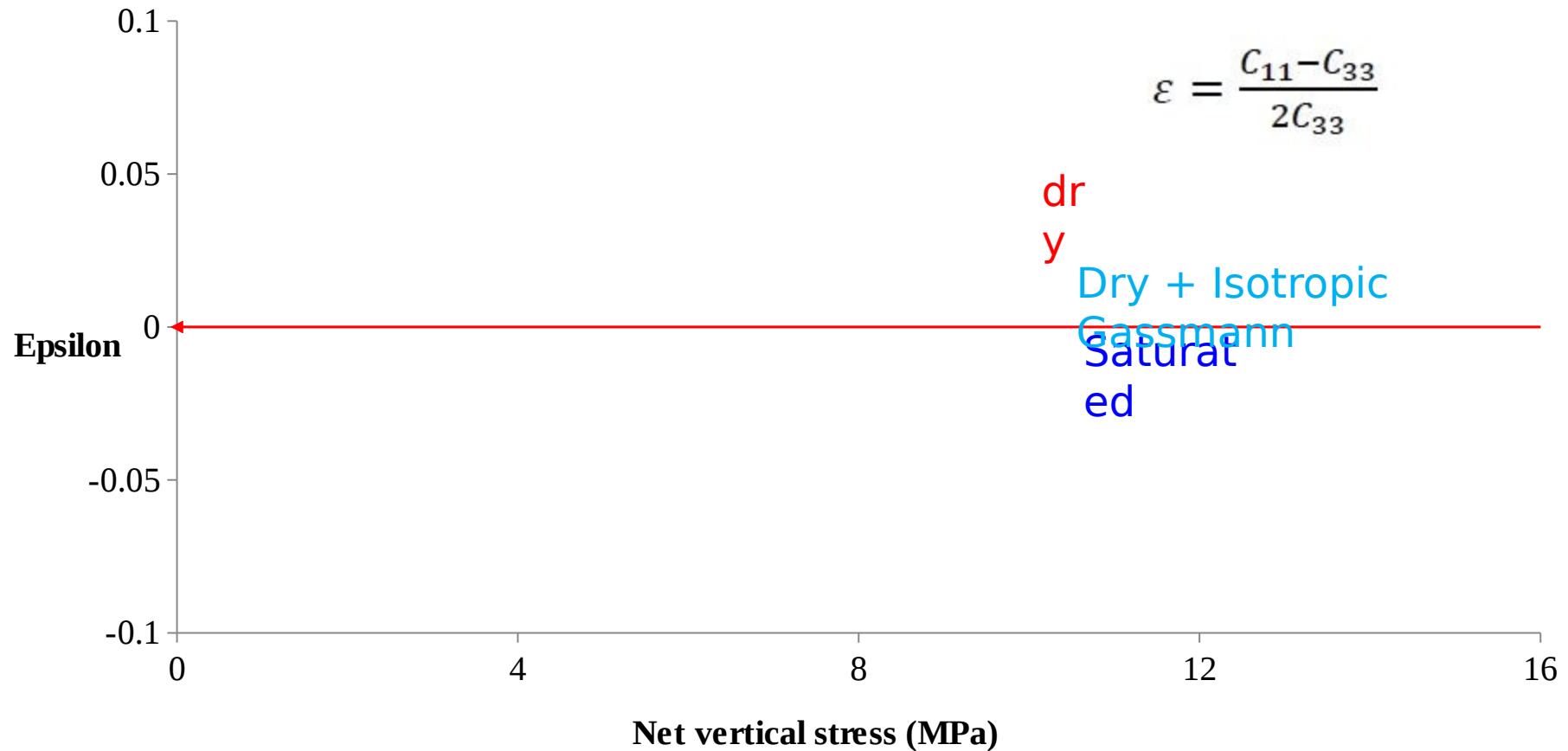
Effect of fluid on Epsilon (Hydrostatic stress)



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■ OT_Saturated (HS); Experiments (TTS)

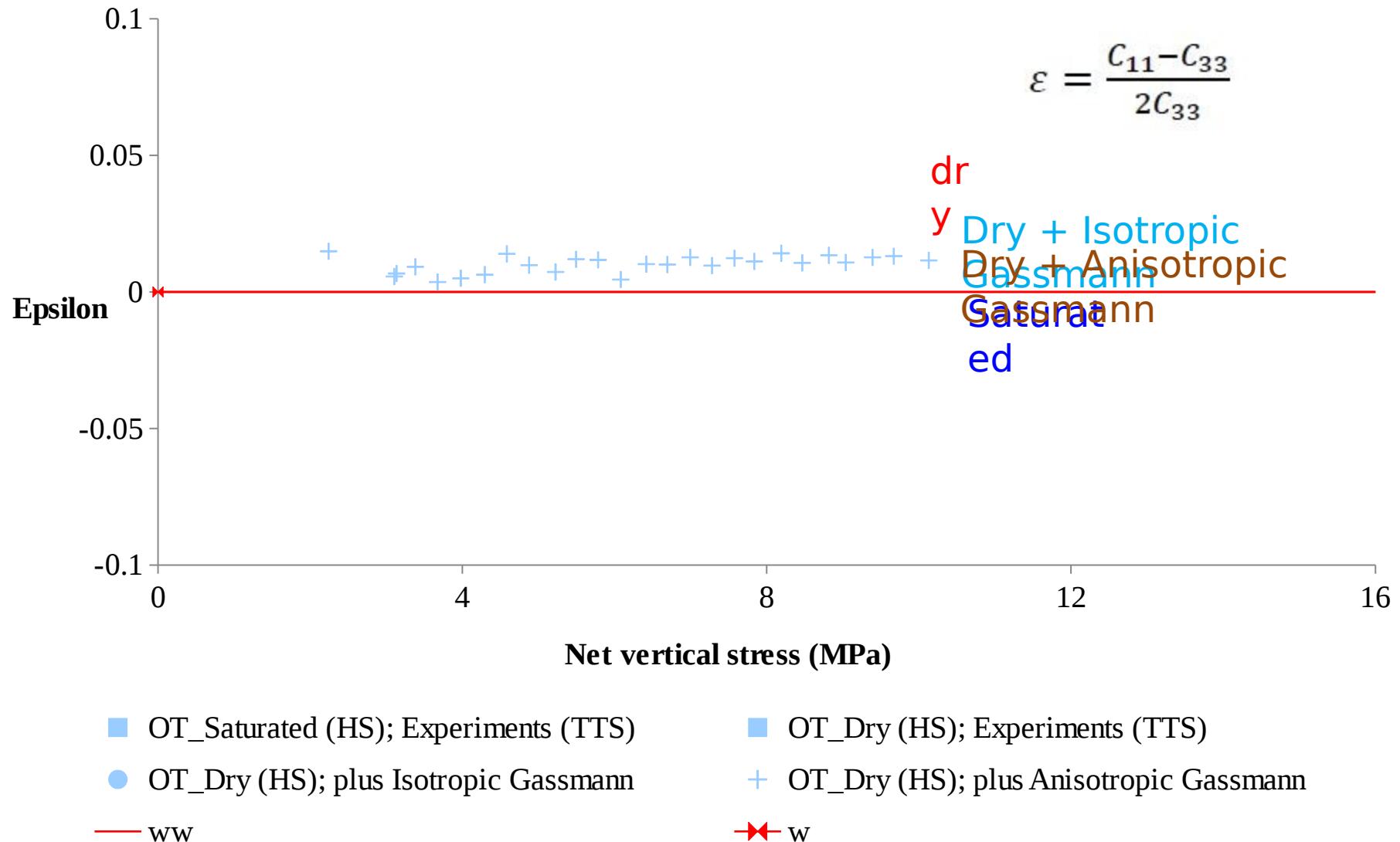
● OT_Dry (HS); plus Isotropic Gassmann

← w

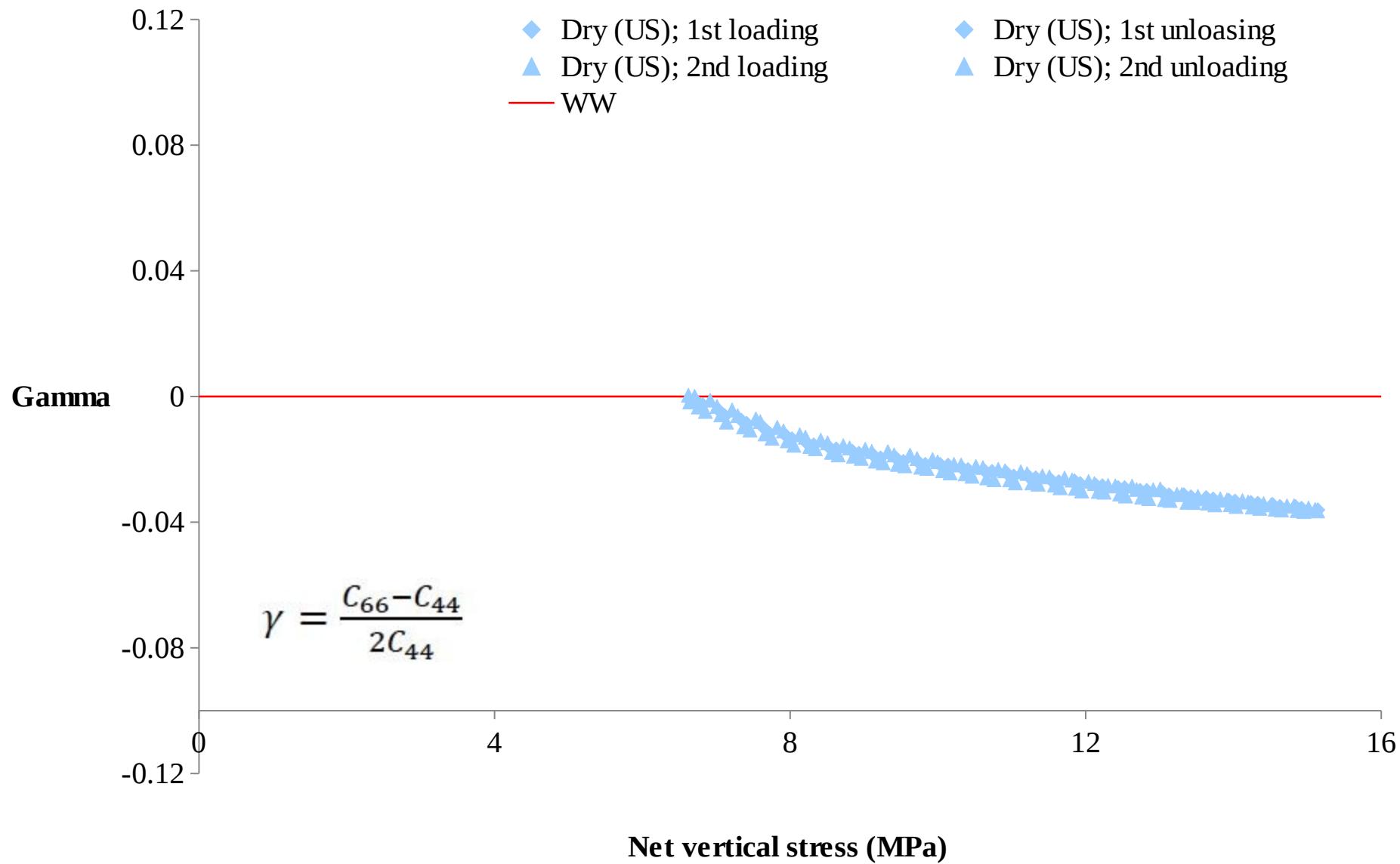
■ OT_Dry (HS); Experiments (TTS)

— ww

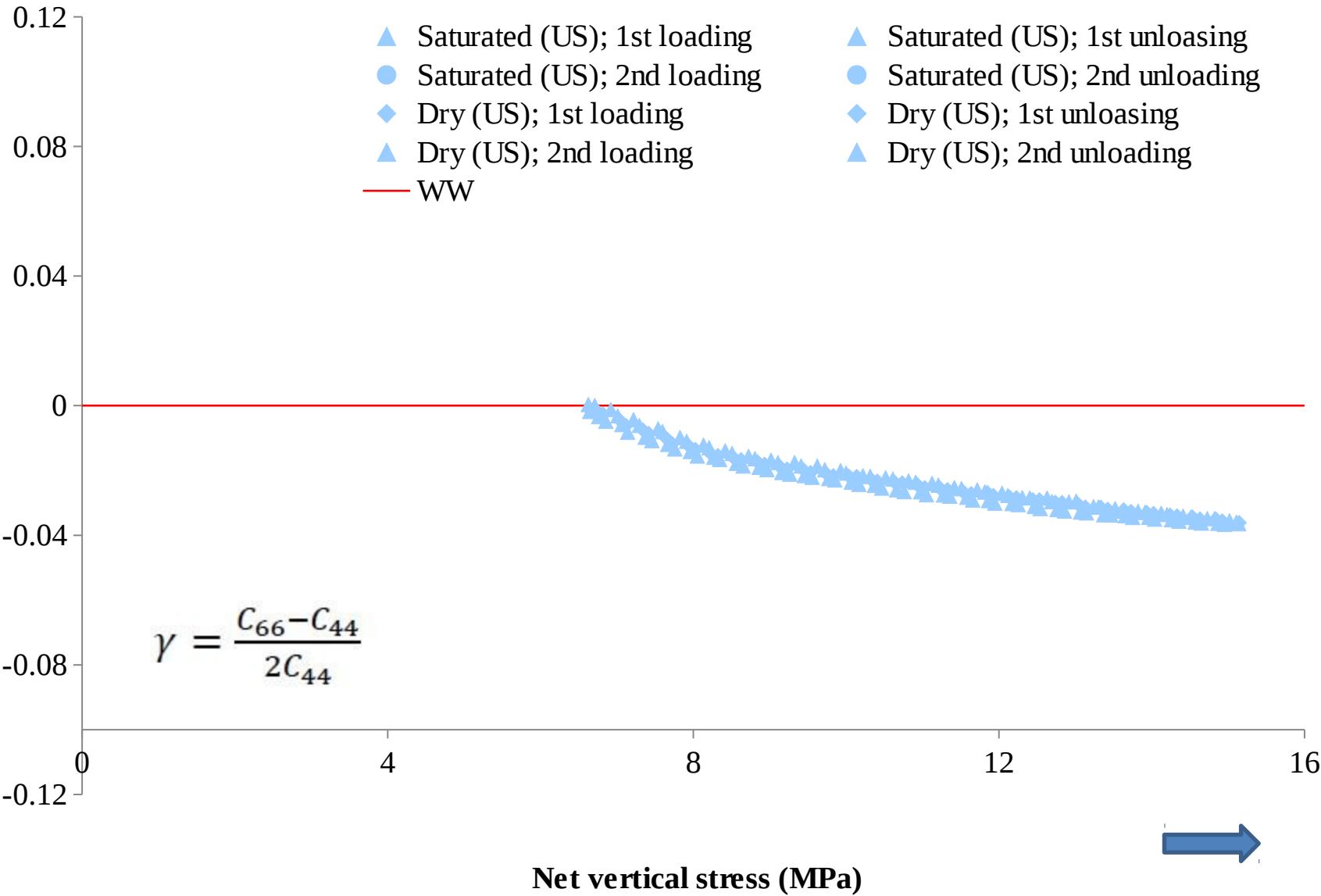
Effect of fluid on Epsilon (Hydrostatic stress)



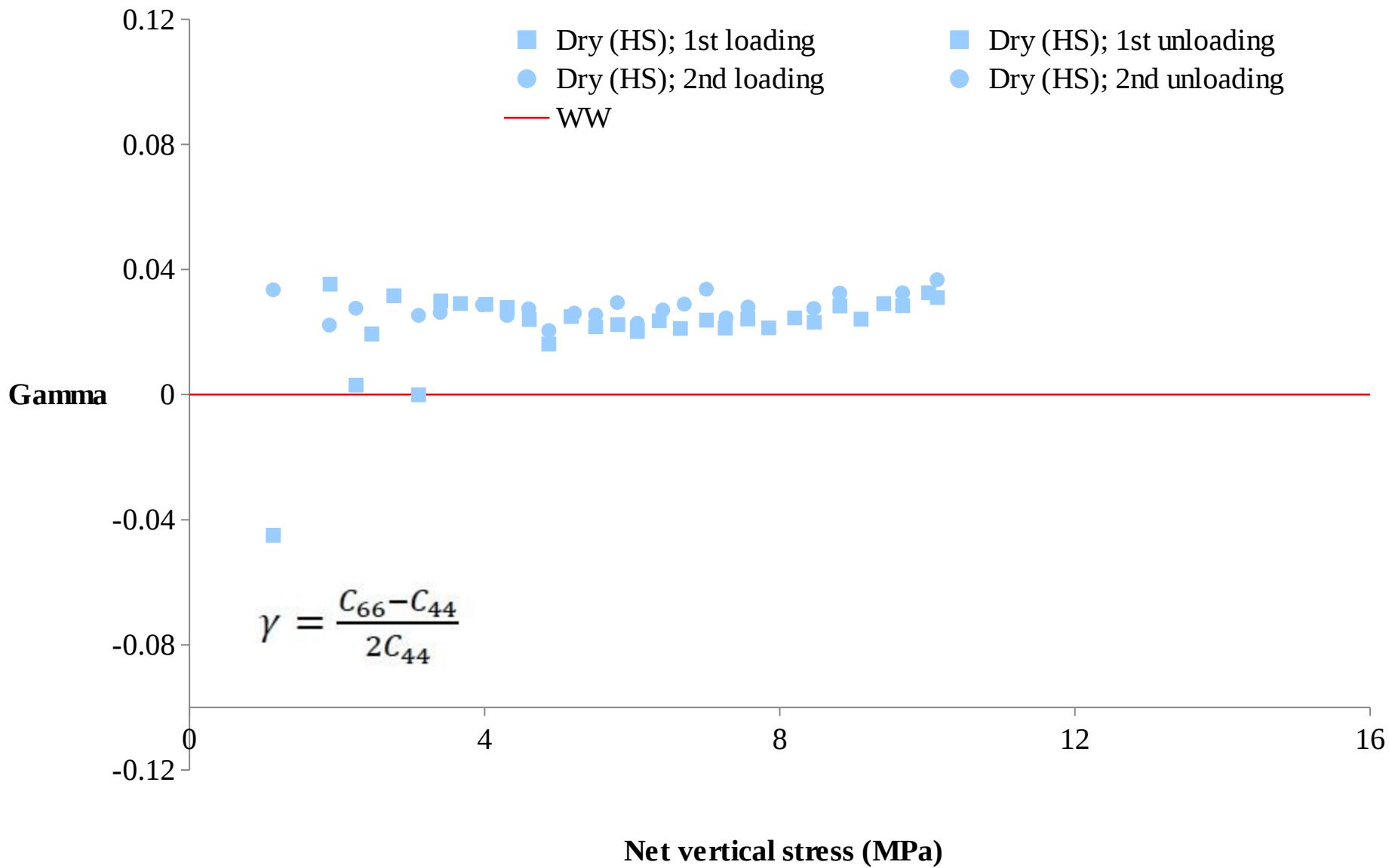
Effect of fluid on Gamma (Uniaxial strain condition)



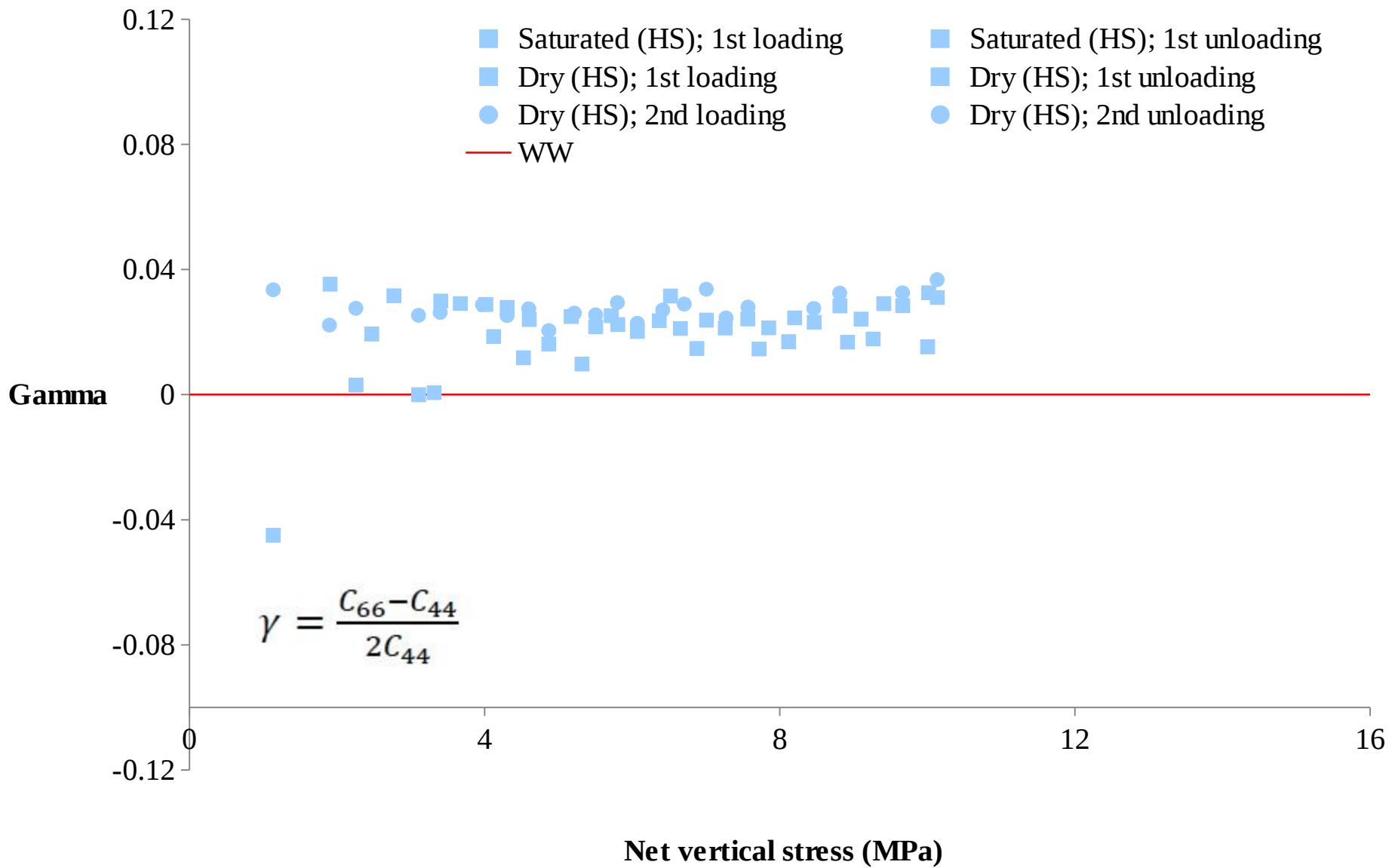
Effect of fluid on Gamma (Uniaxial strain condition)



Effect of fluid on Gamma (Hydrostatic stress)

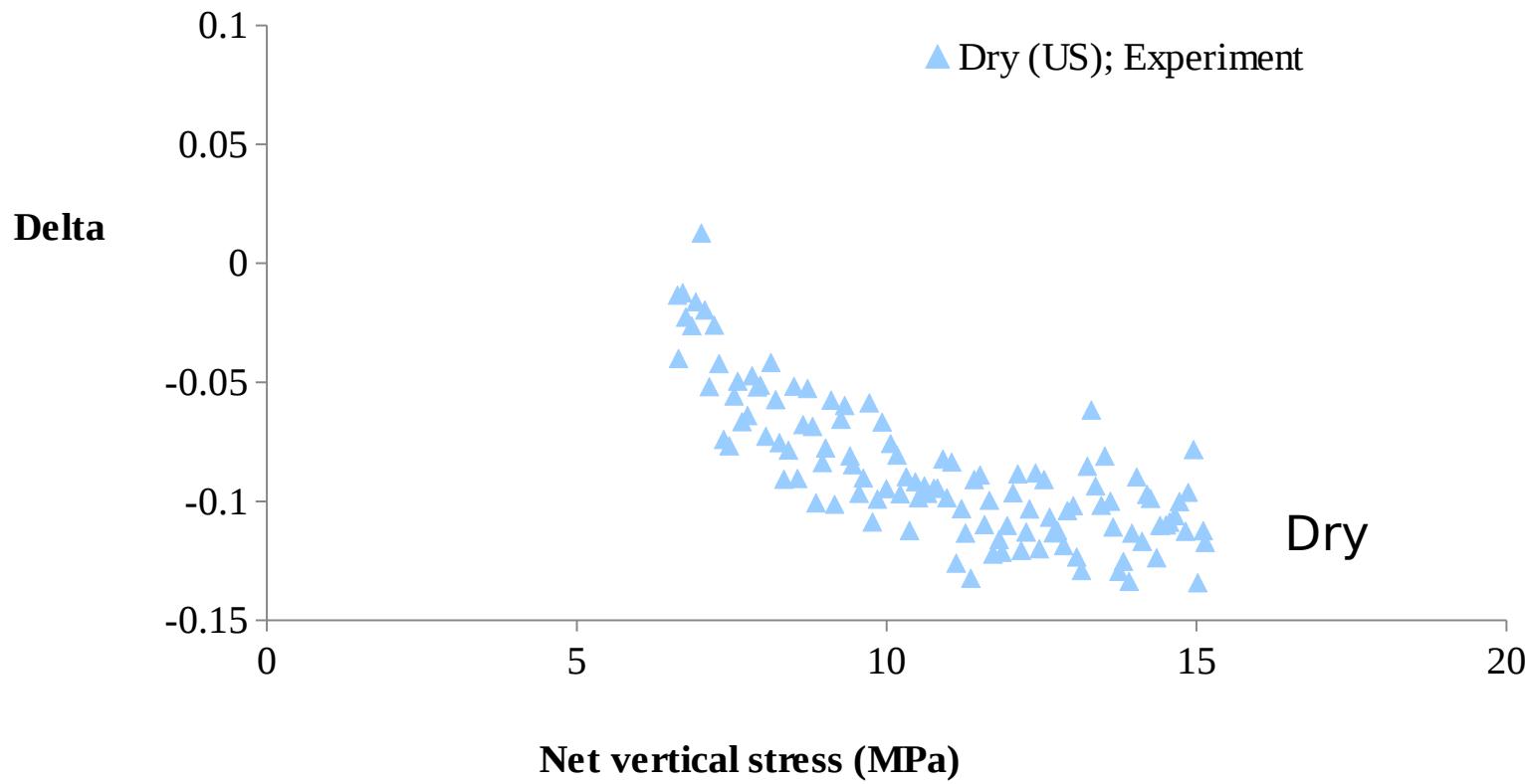


Effect of fluid on Gamma (Hydrostatic stress)



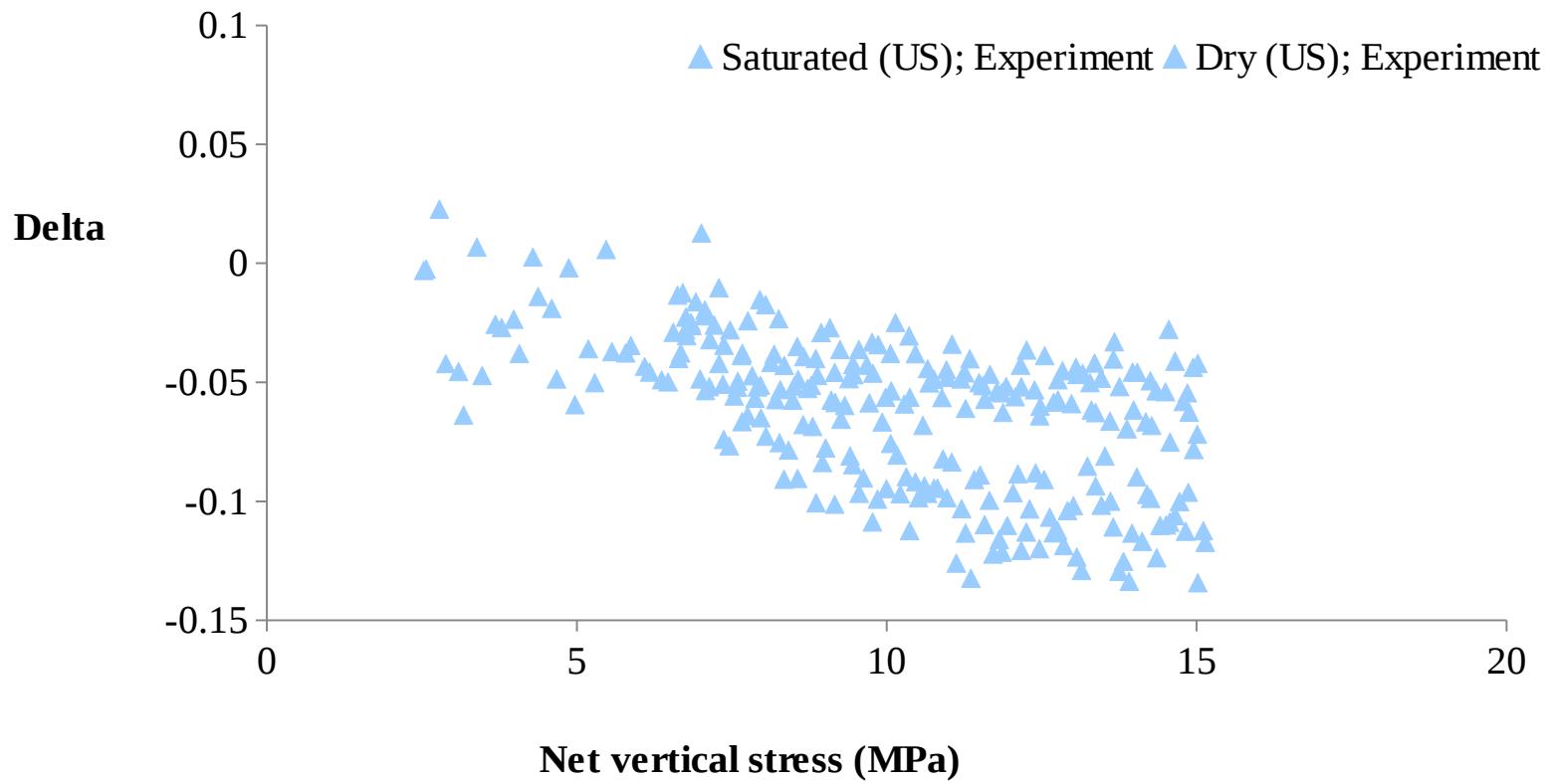
Effect of fluid on Delta (Uniaxial strain condition)

$$\delta = \frac{(C_{13}+C_{44})^2 - (C_{33}-C_{44})^2}{2C_{33}(C_{33}-C_{44})}$$



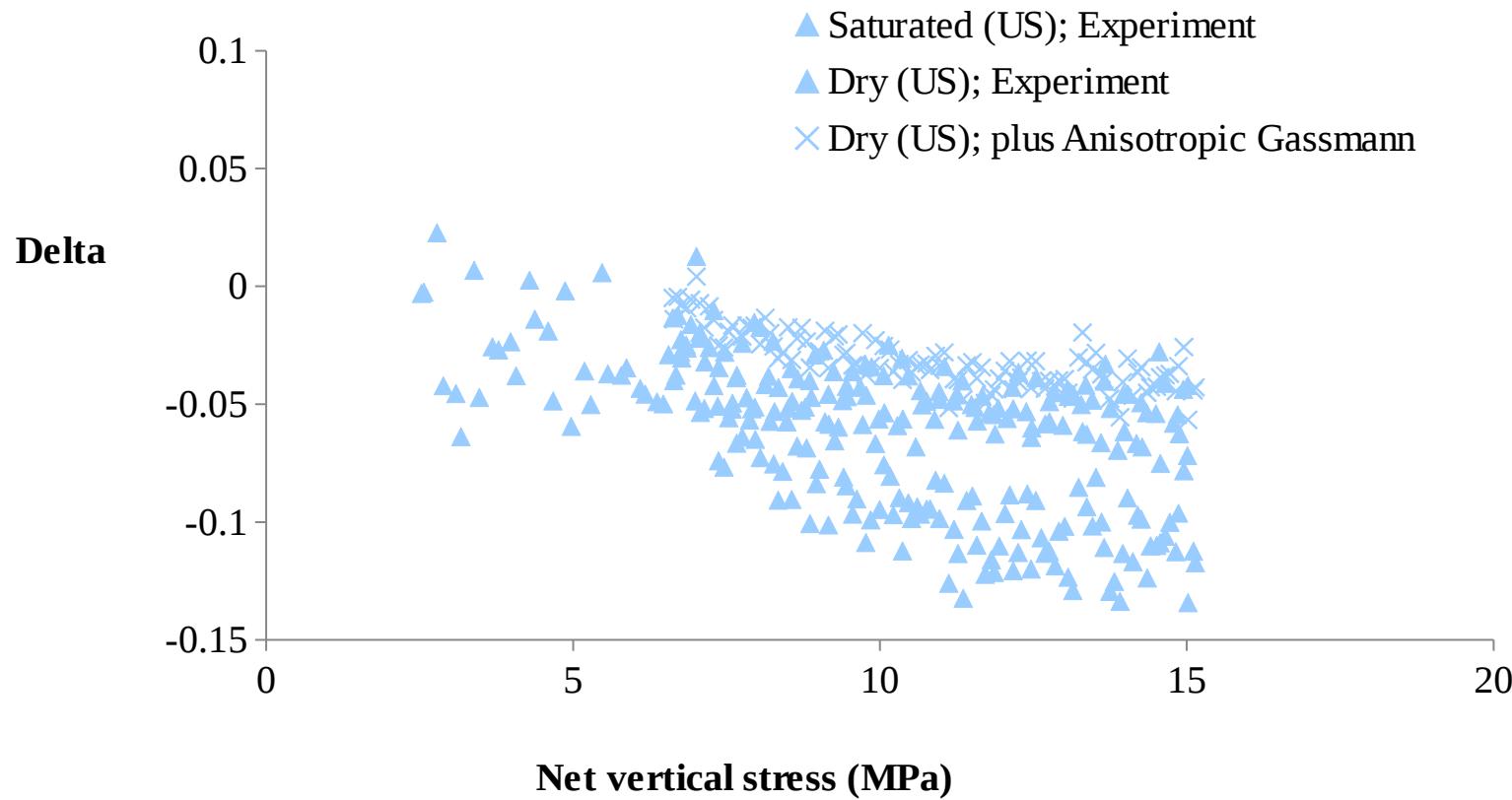
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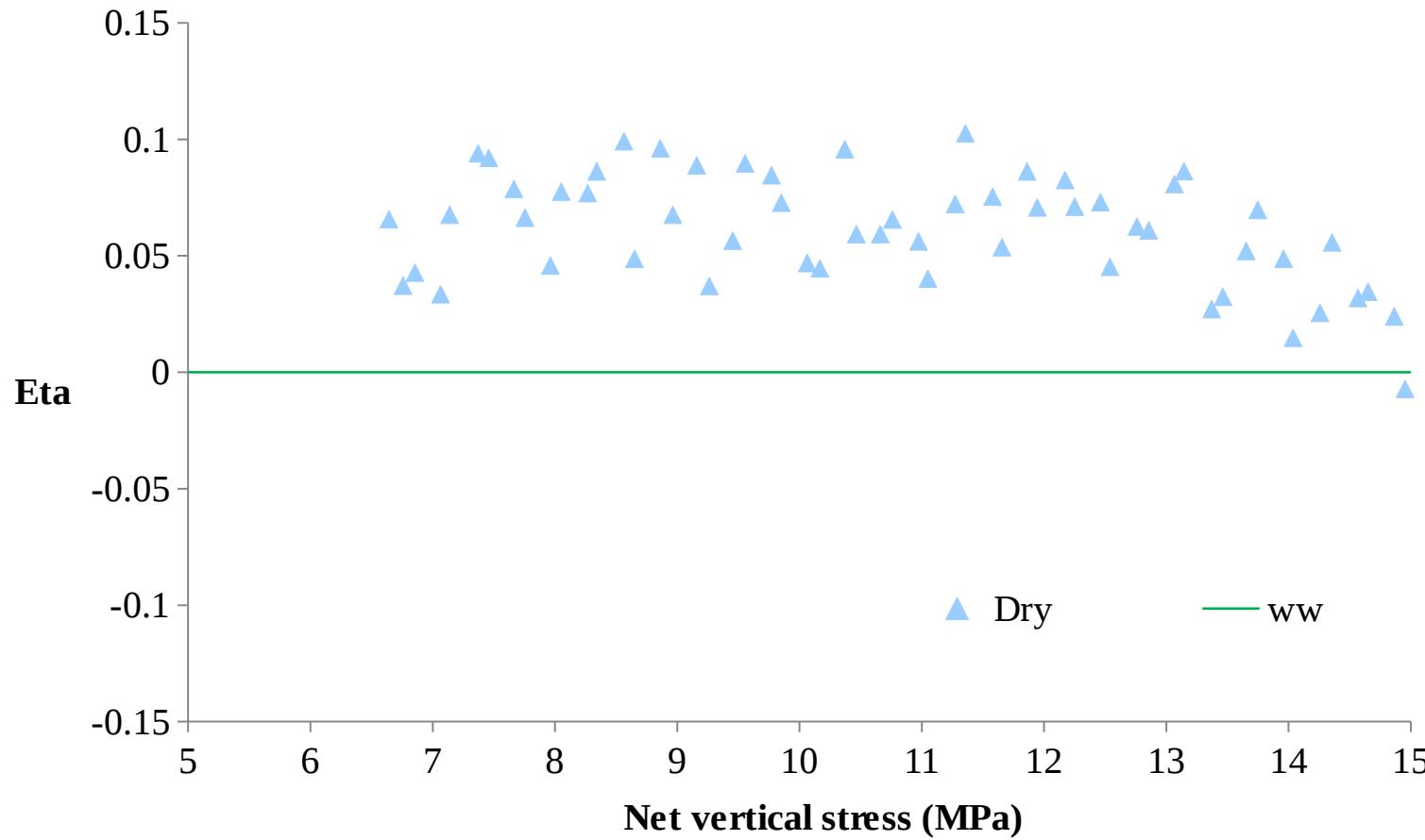
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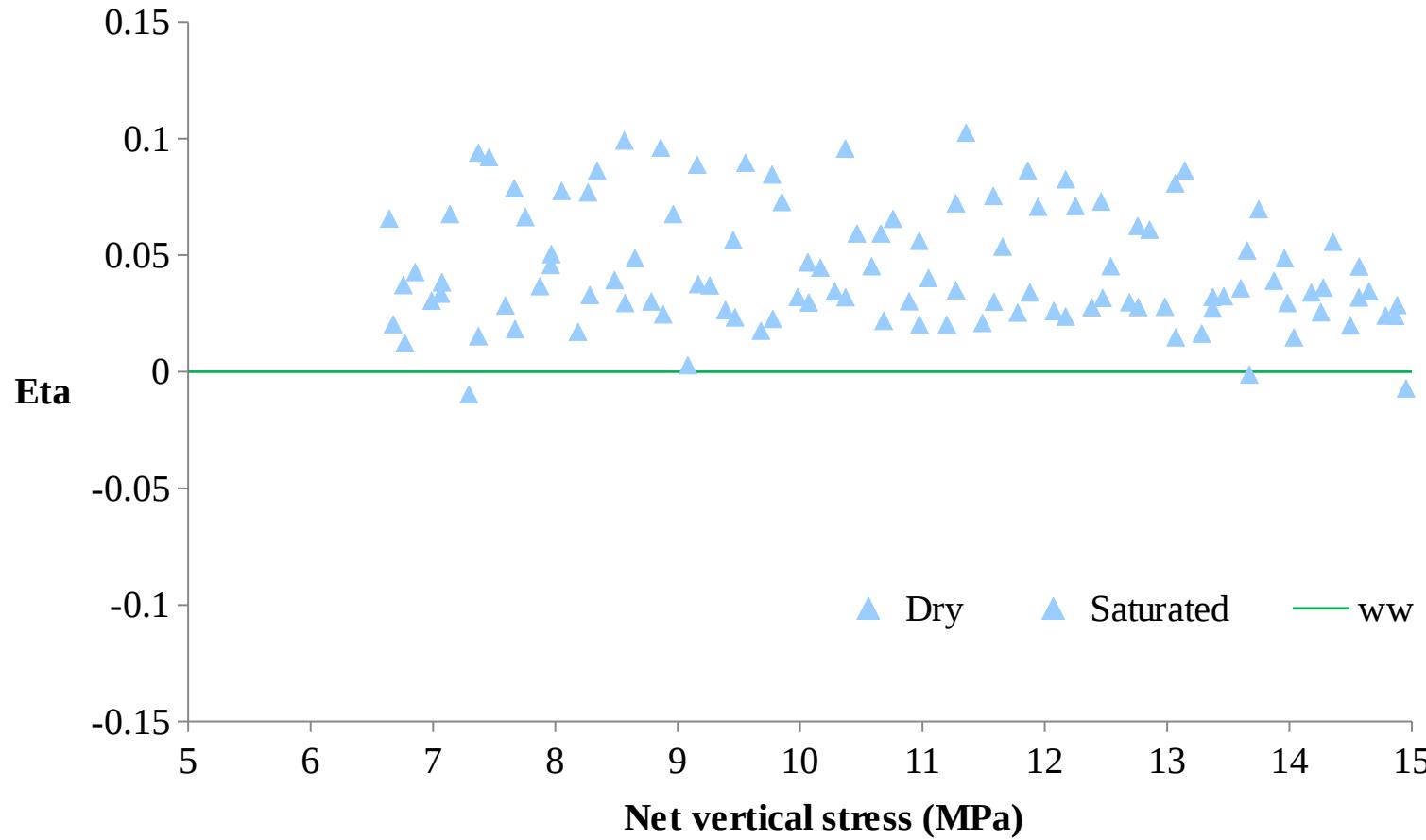
Effect of fluid on Eta (Uniaxial strain condition)

$$\eta = \frac{\varepsilon - \delta}{1 + 2\delta}$$



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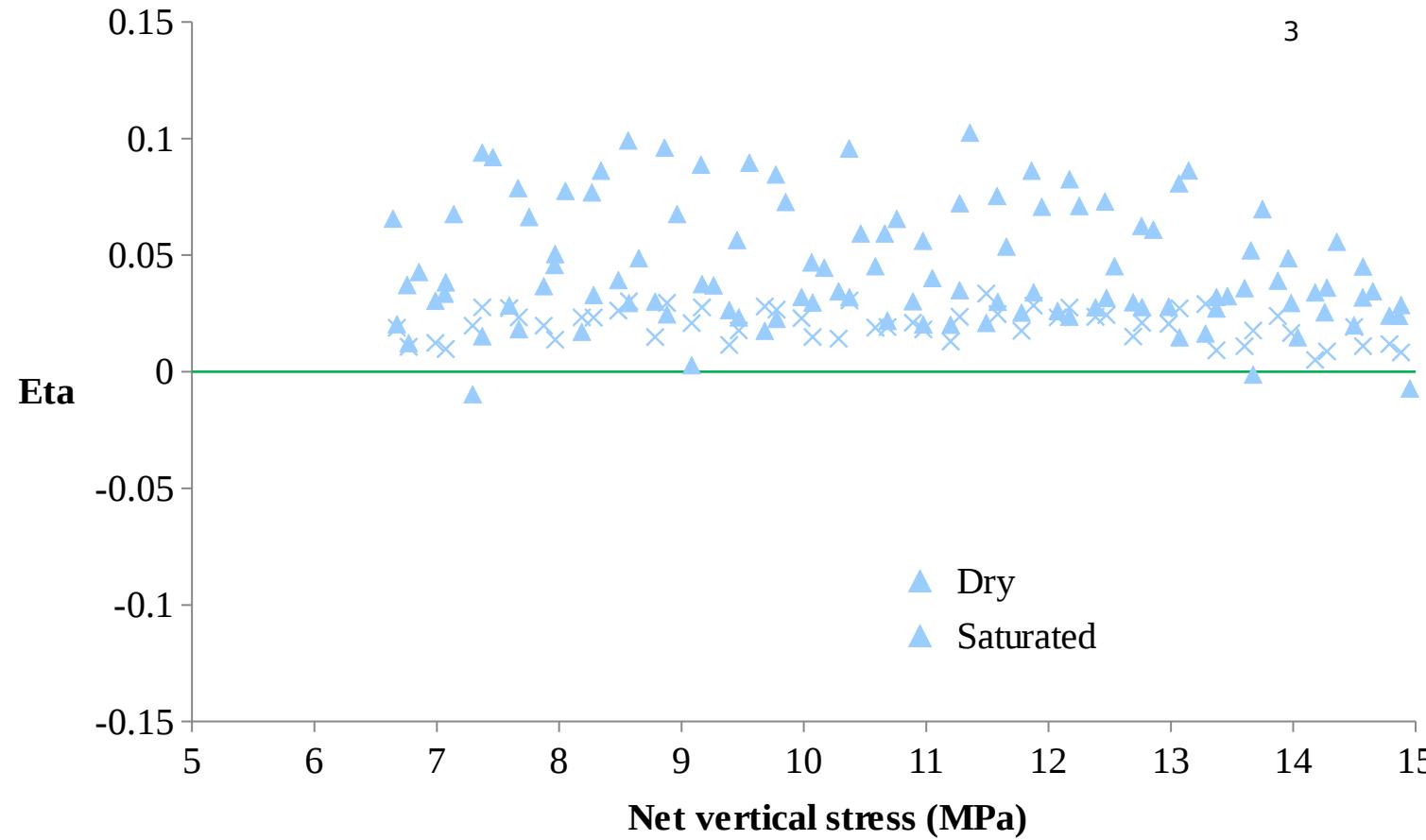


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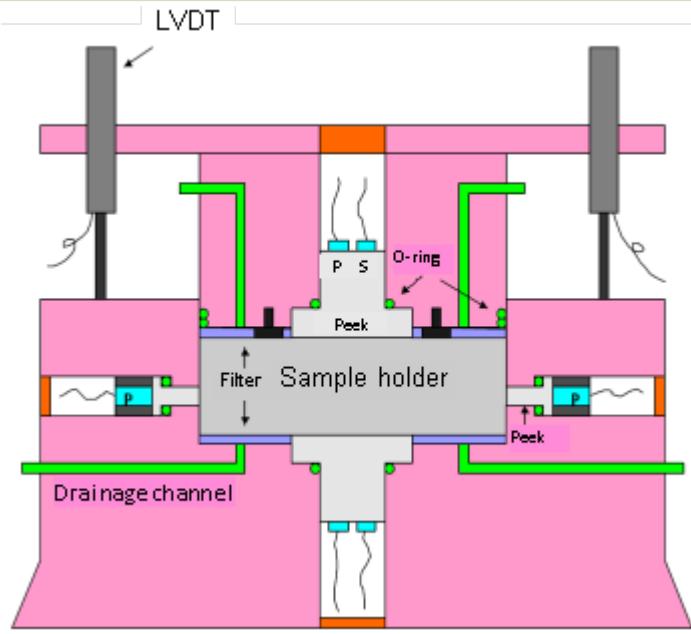
$$\eta^{\text{sat}} = \frac{C_3}{C_3 + \eta}$$

3

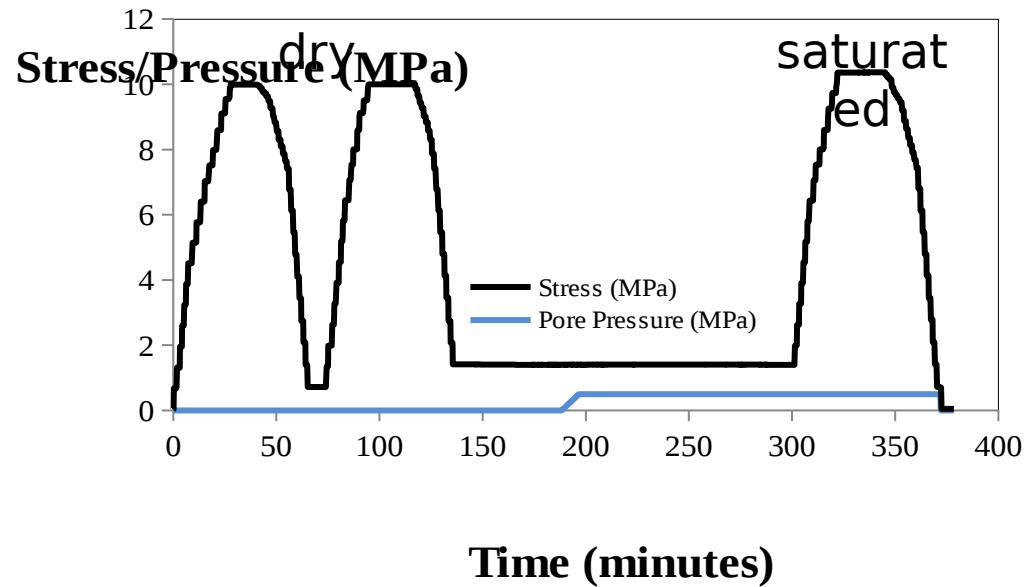
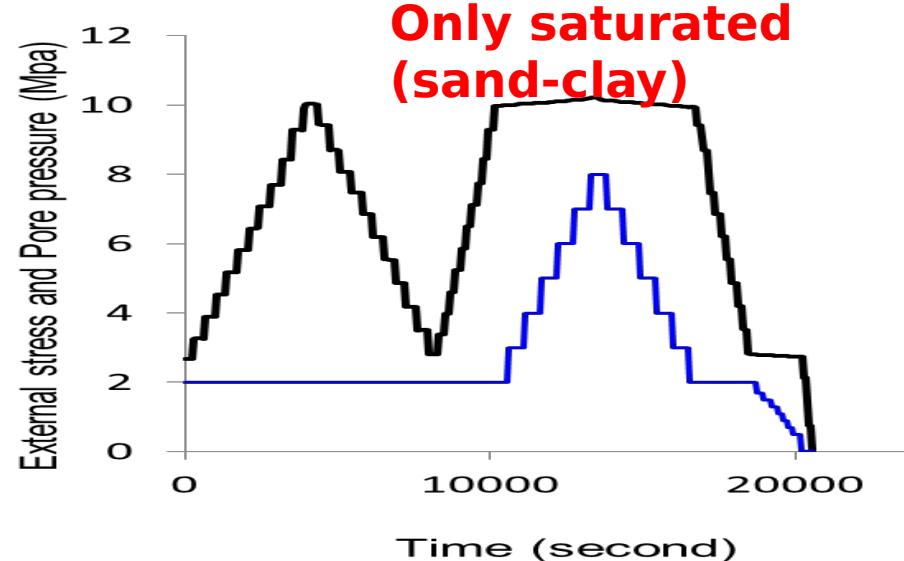


Vp-Vs (sand-clay)

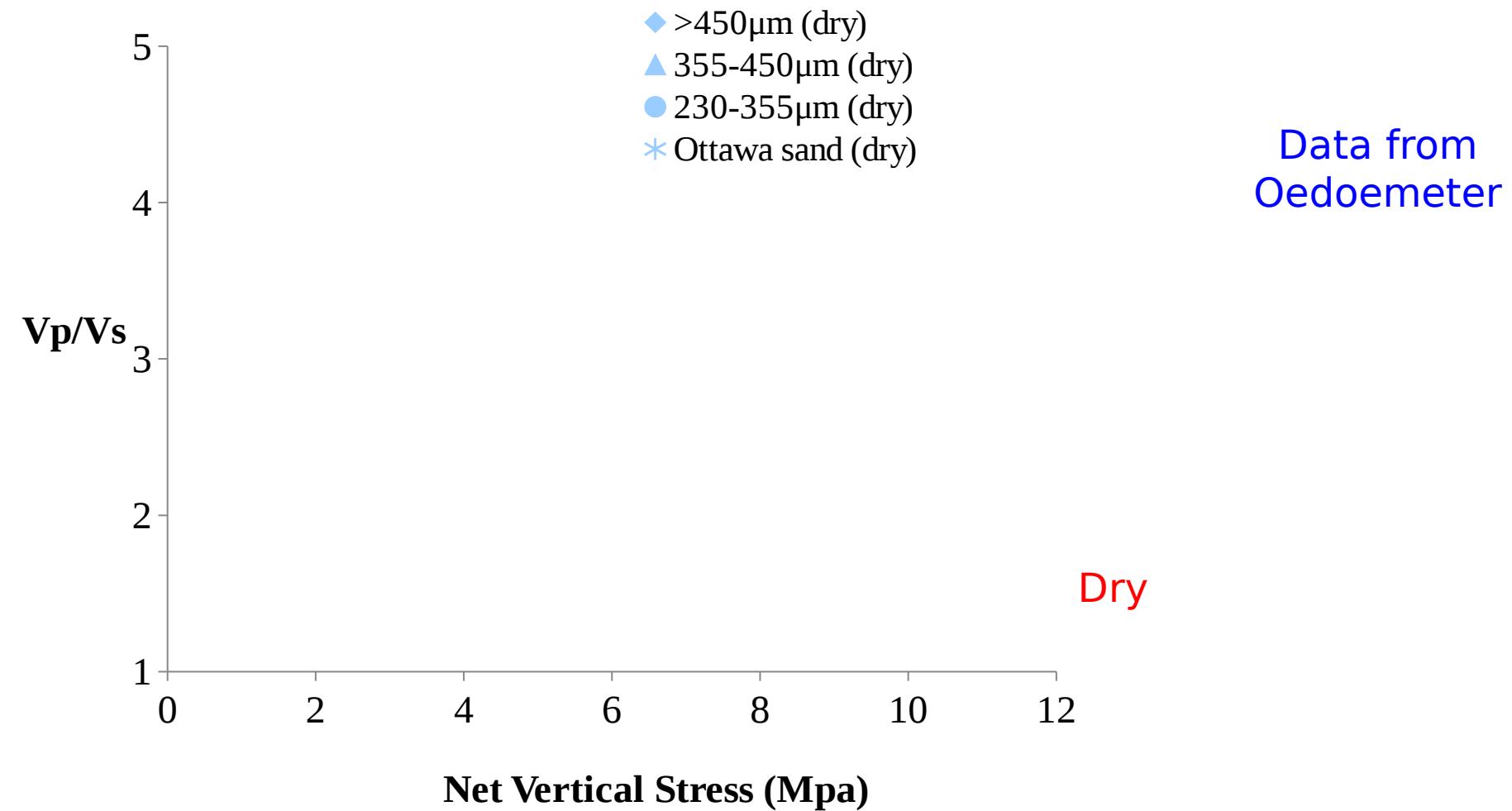
Lab tests in Oedometer



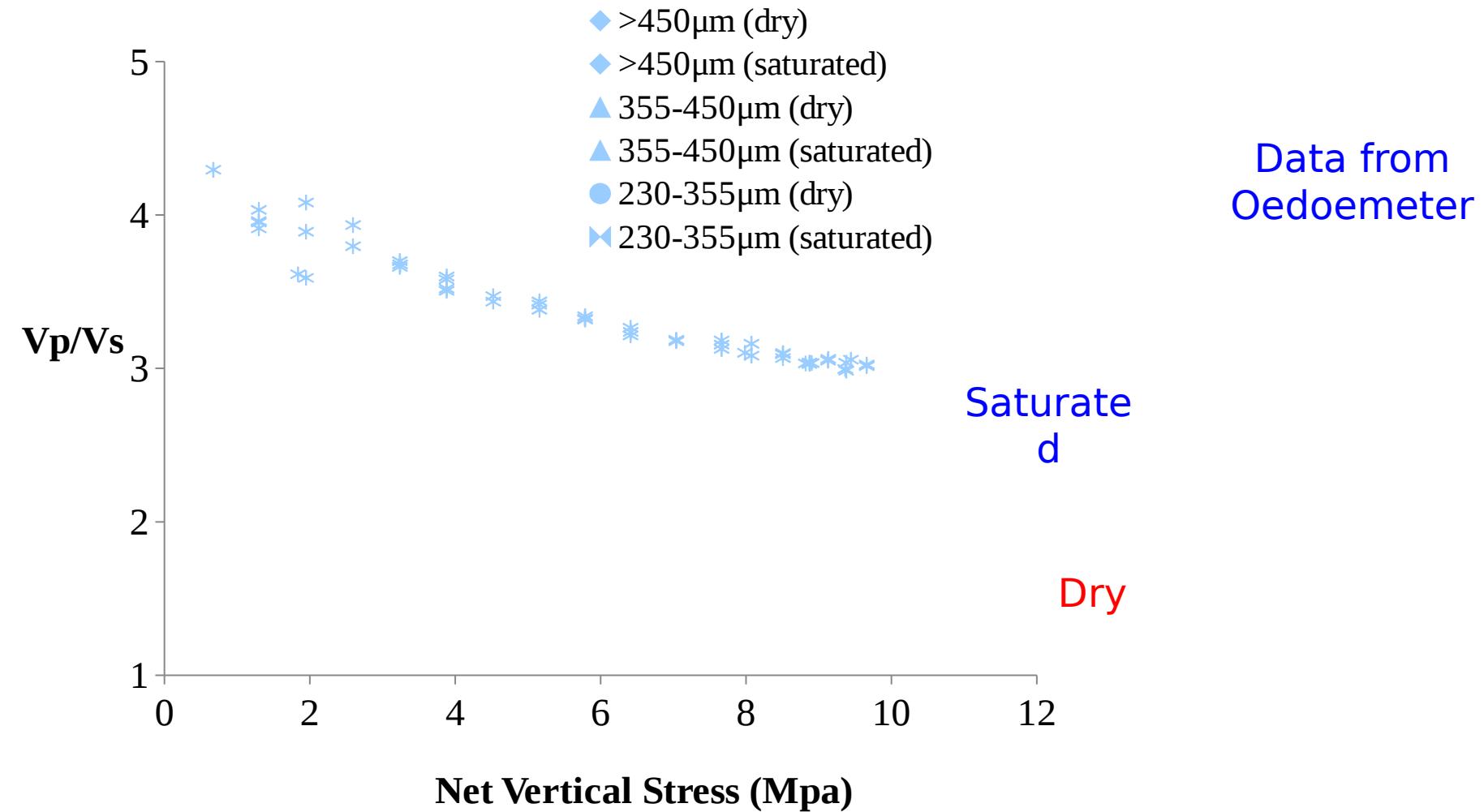
Fluid effects →
(only sand)



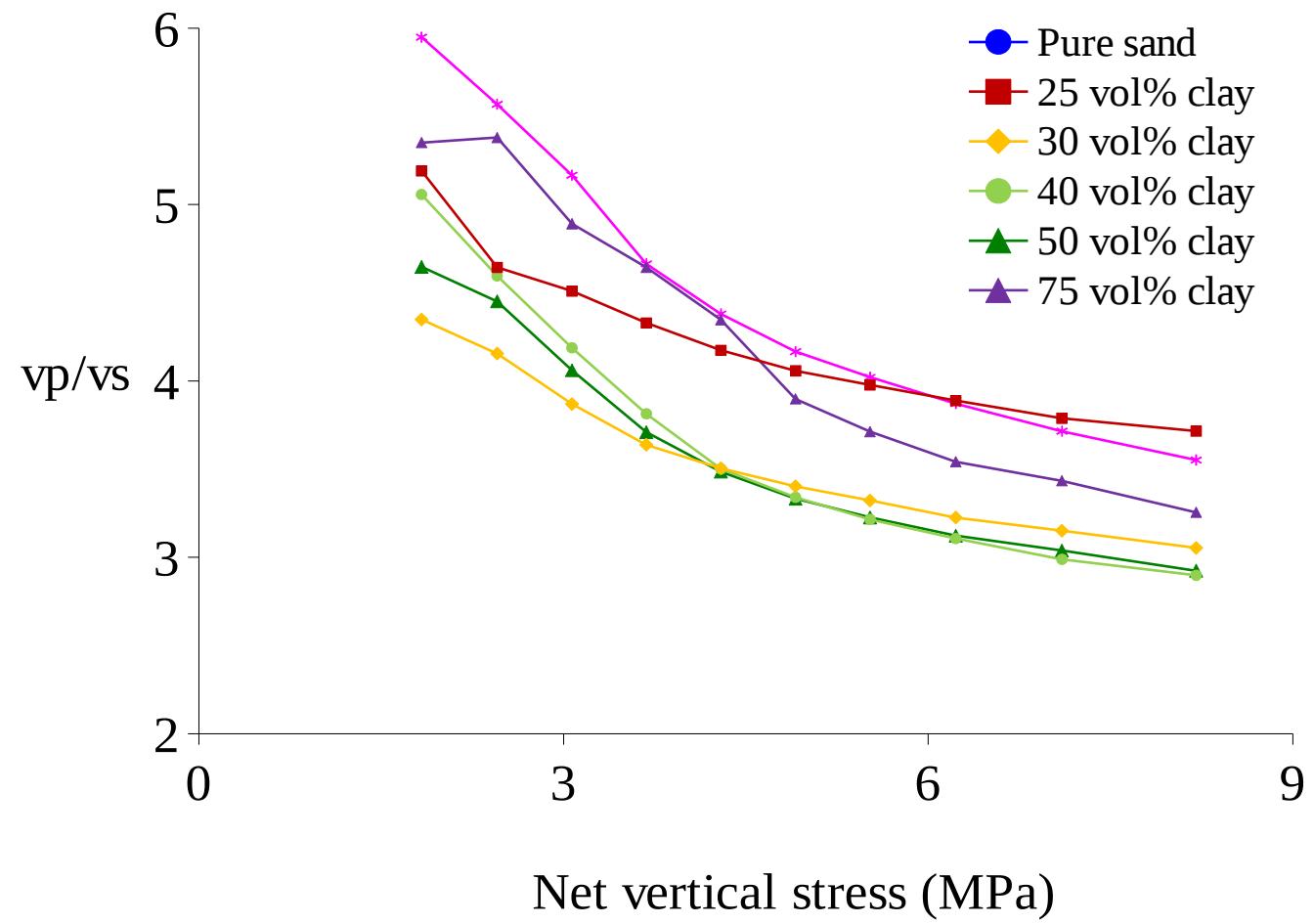
V_p/V_s : Role of fluid (only sand data)



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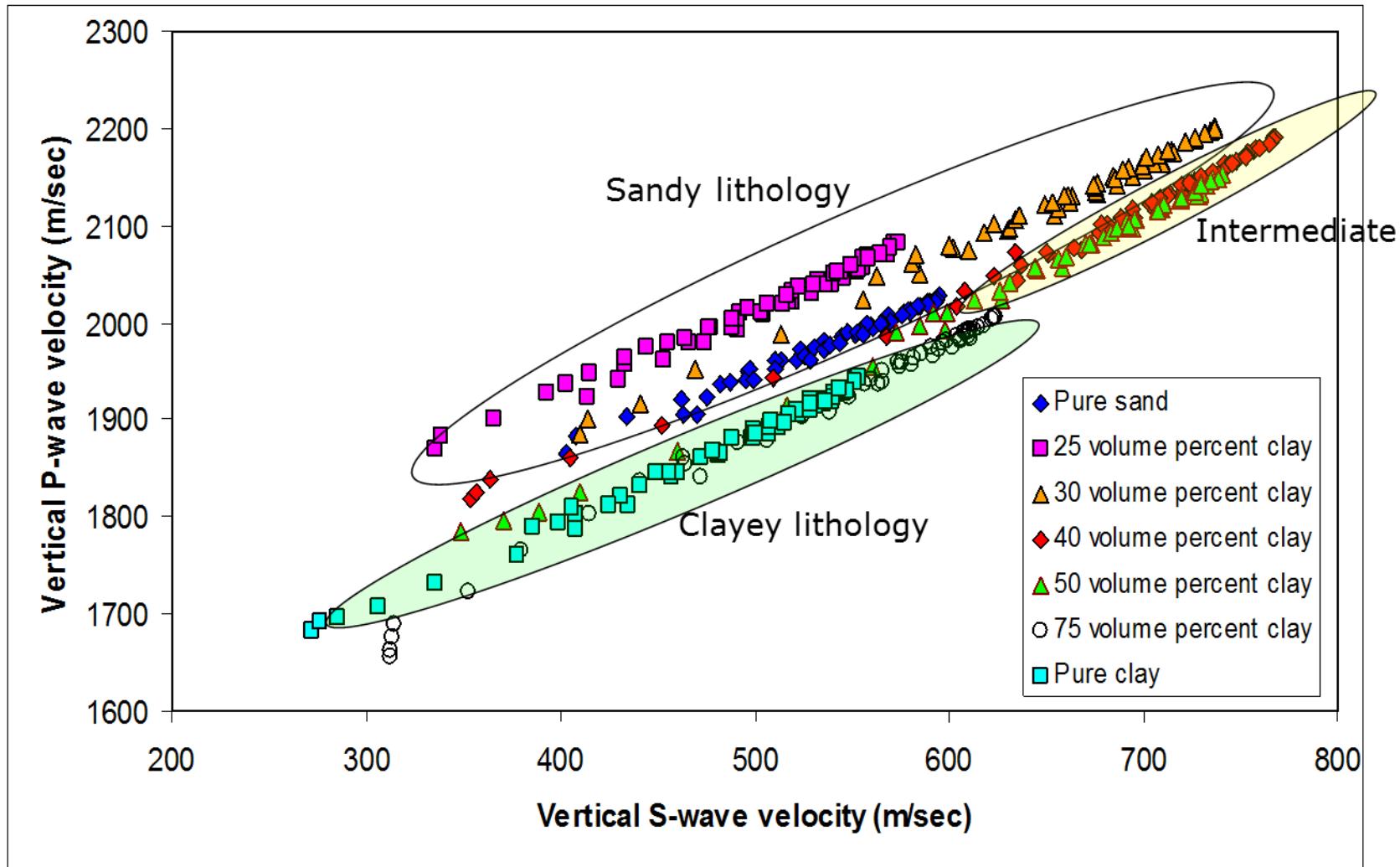
V_p/V_s : The role of clay content and stress



Data from tests with brine-saturated sand, clay (kaolinite) and sand:clay mixtures

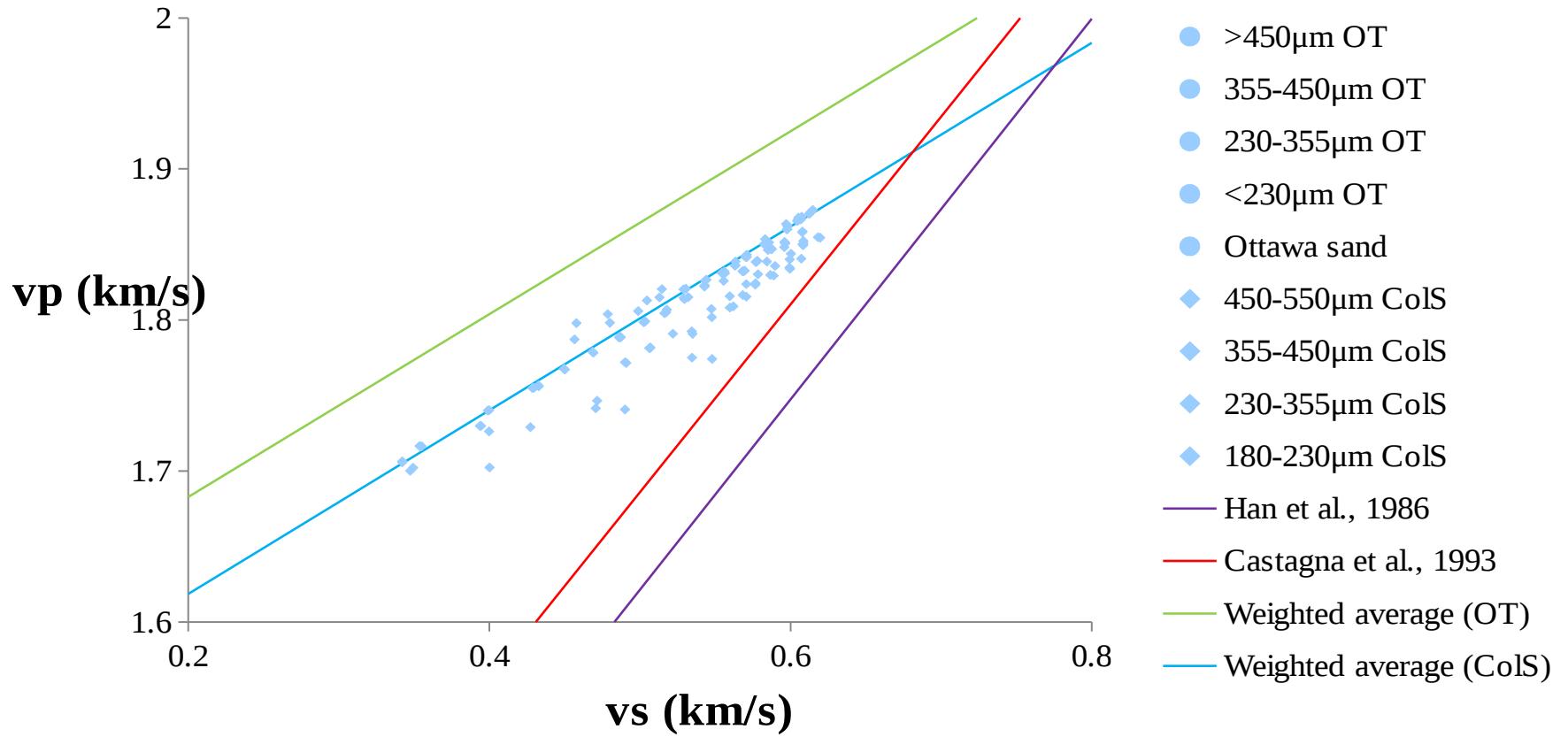
v_p/v_s decreases with stress, more in clay than in sand

V_p/V_s trends



Oedometer tests performed with brine-saturated sand, clay (kaolinite) and sand:clay mixtures have been used to address v_p vs. v_s trends (here: only axial velocities)

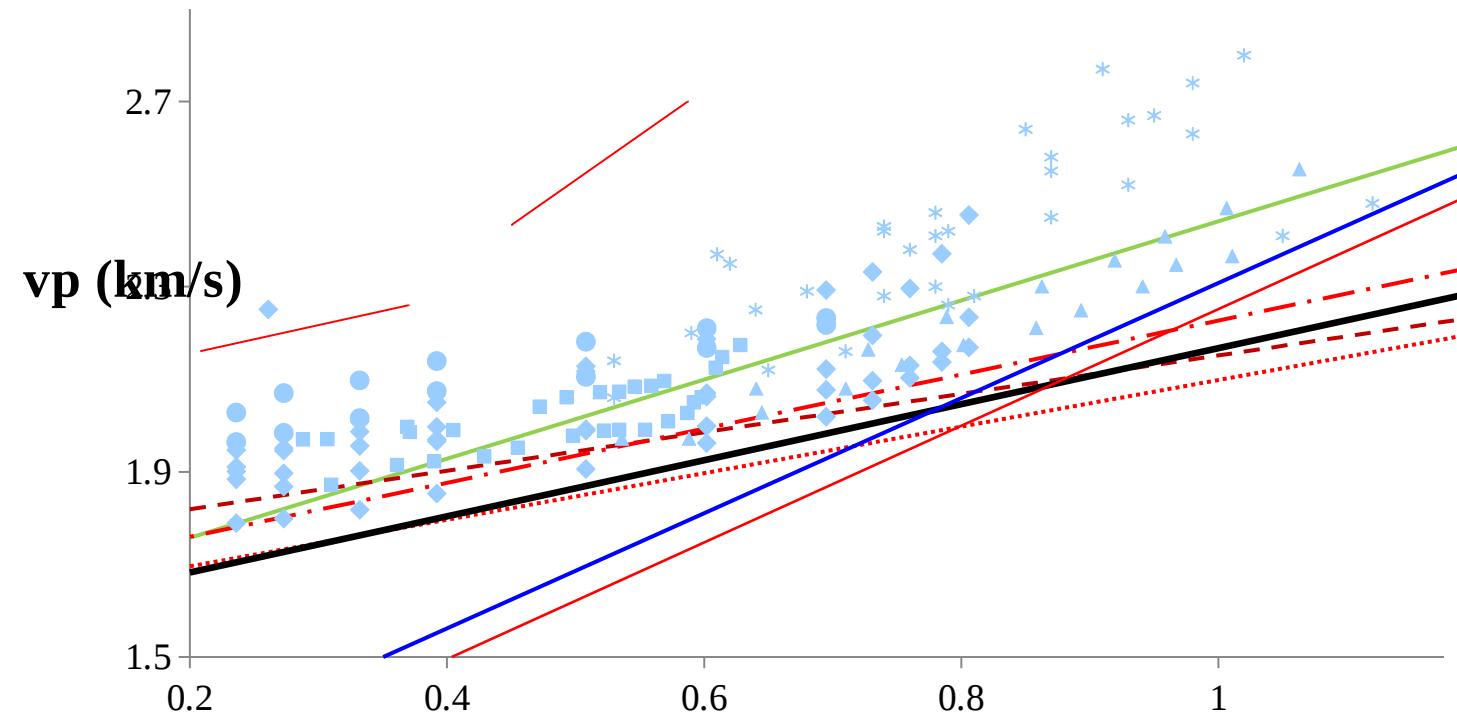
v_p/v_s : trends for sand



Higher velocities for Ottawa than for angular Columbia sand, but similar v_p - v_s trends

Plotting v_p vs v_s gives a better picture than showing v_p/v_s alone

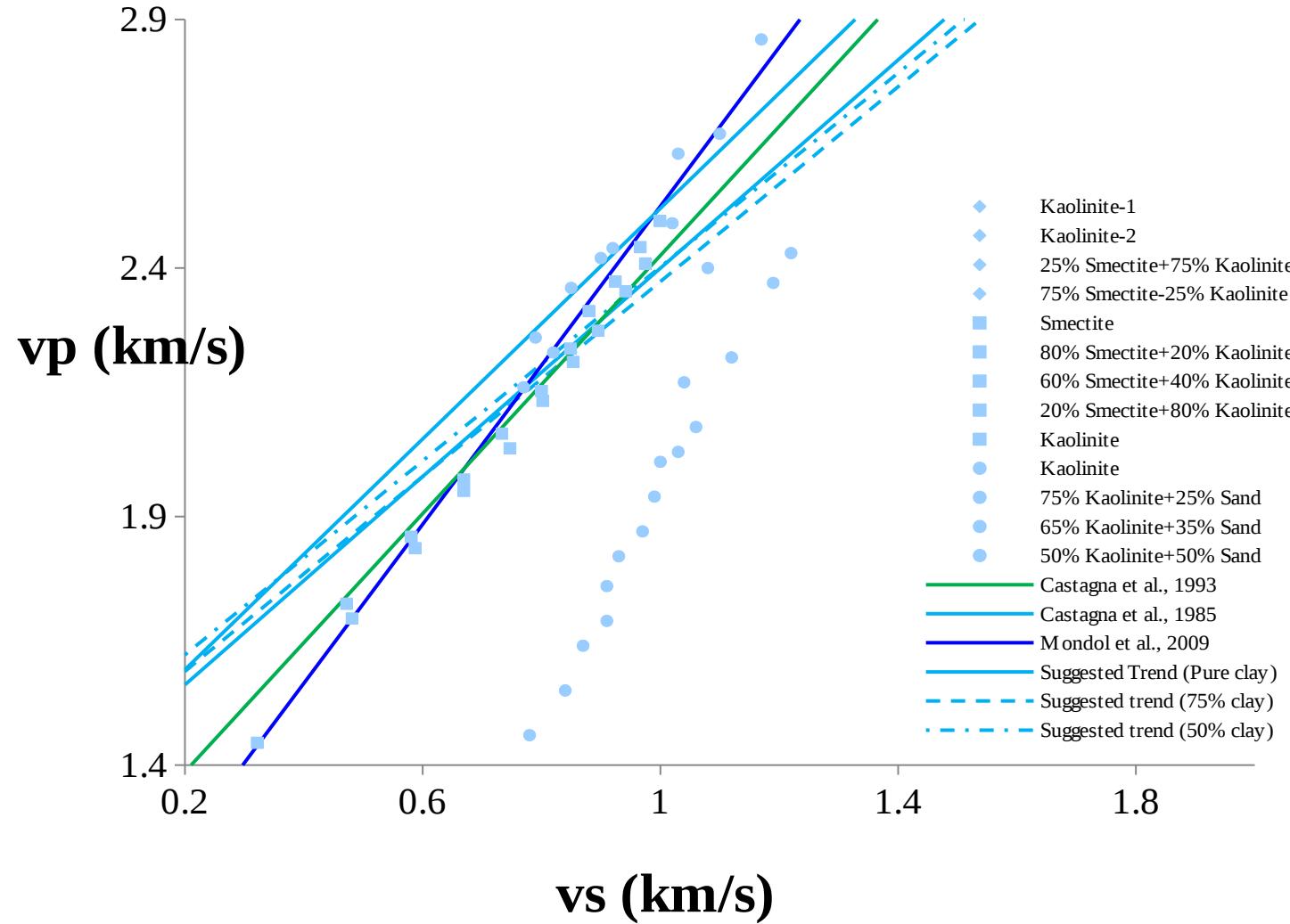
v_p/v_s : global trends for sand



The trends are different from data at low stress (< 10 MPa) and above

Data from
Zimmer, 2003
(Diamond);
Domenico,
1977 (circular),
Prasad, 1988
(square);
Mondol et al.,
2010 (triangle)
and Yin, 1992
(star)

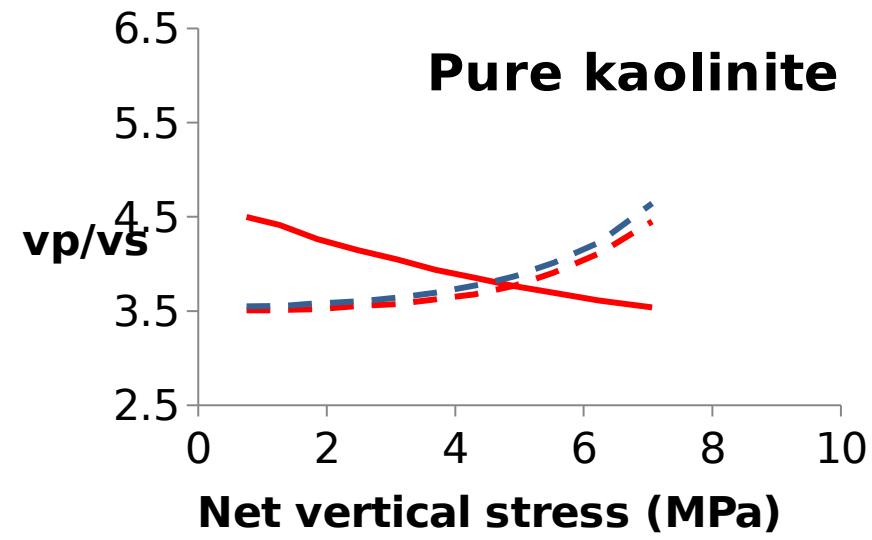
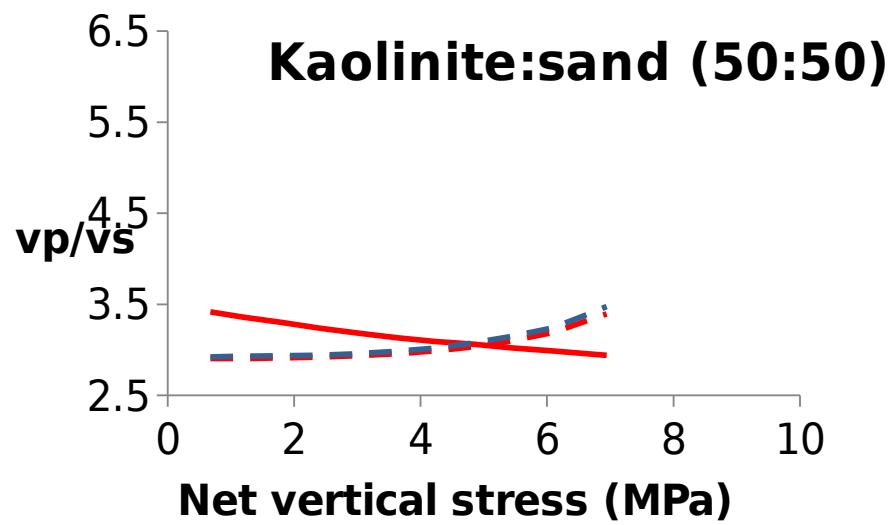
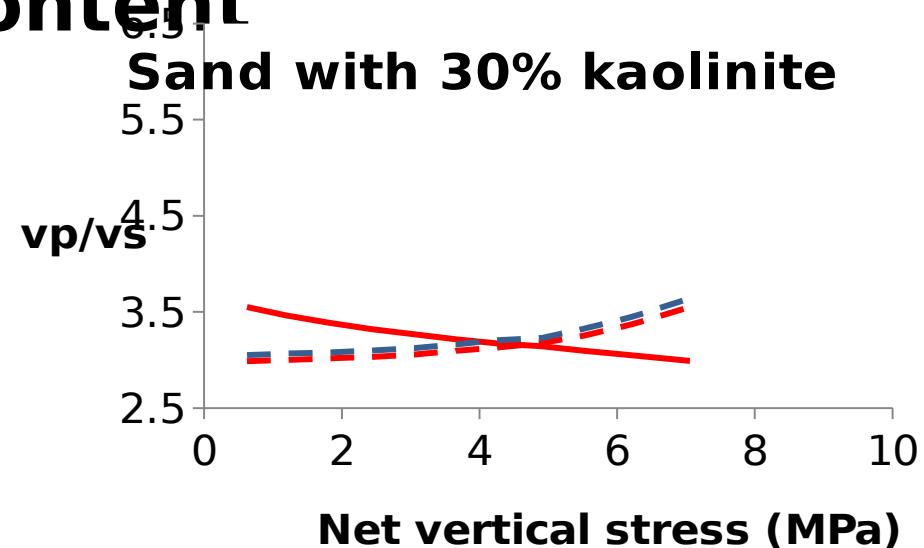
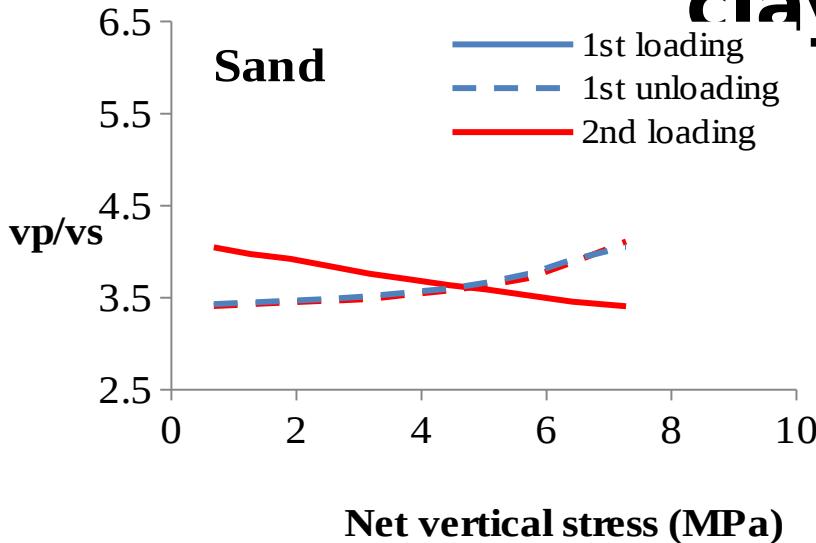
v_p/v_s : trends for clays



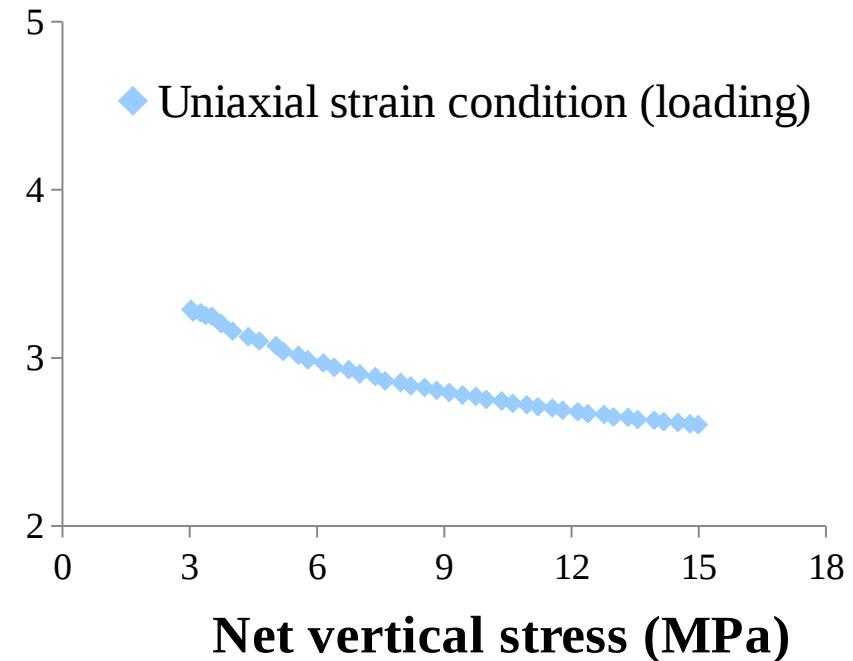
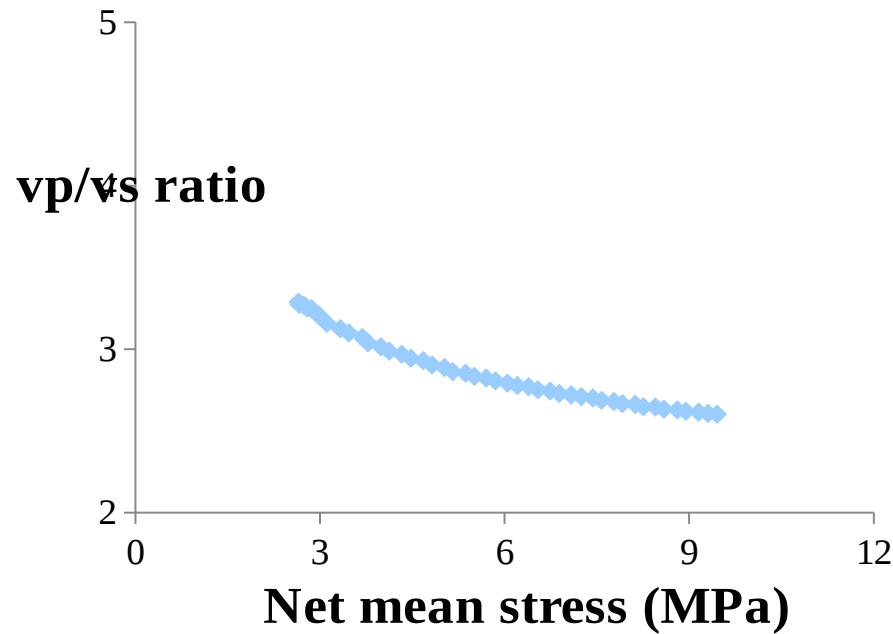
The trends are different from sand + again for data at low stress (< 10 MPa) vs. above

Diamonds:
This study
Squares:
Mondol et al.
(2009)
Circles: Yin
(1992)
(hydrostatic
data)

Vp/Vs: Role of state of consolidation and clay content

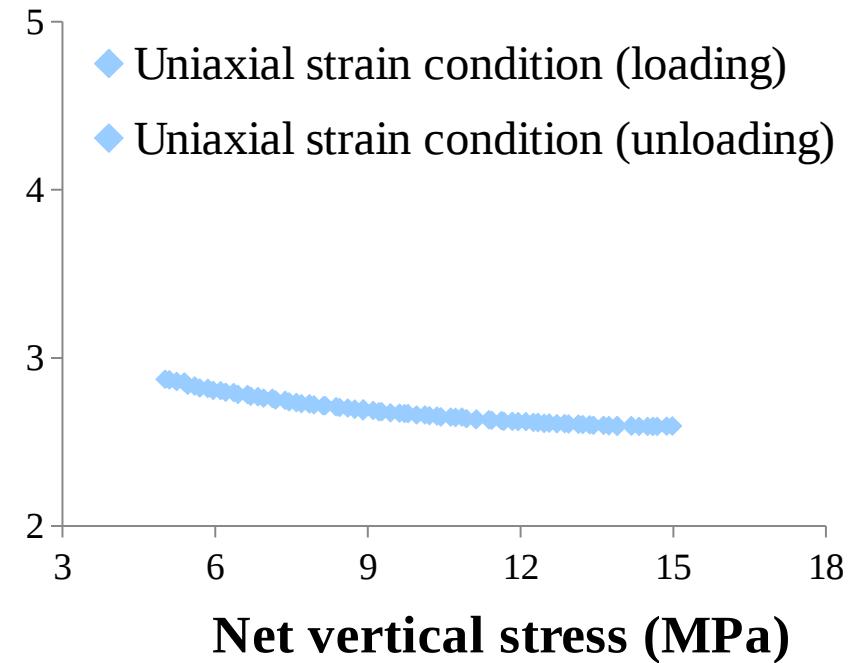
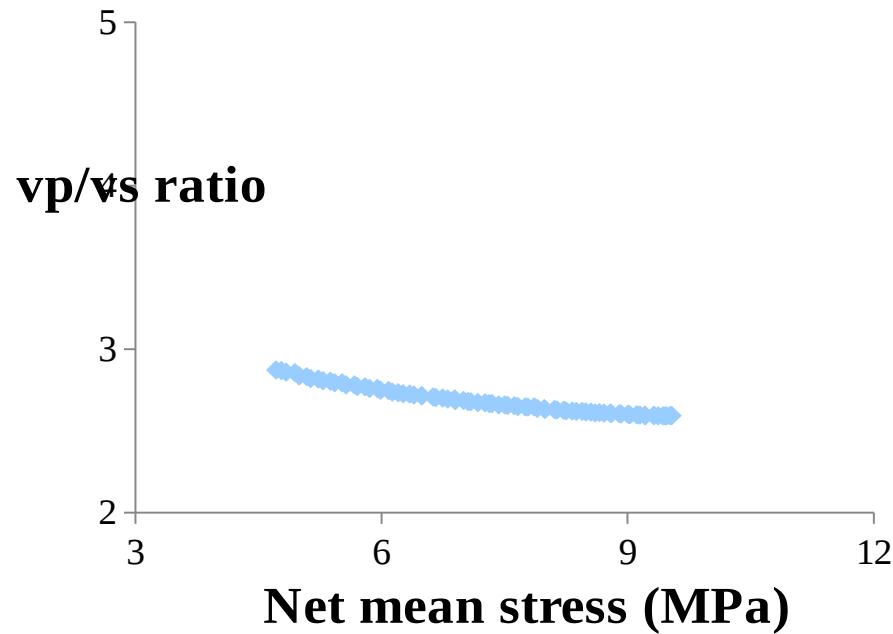


v_p/v_s : The role of Stress Path (only for sand)



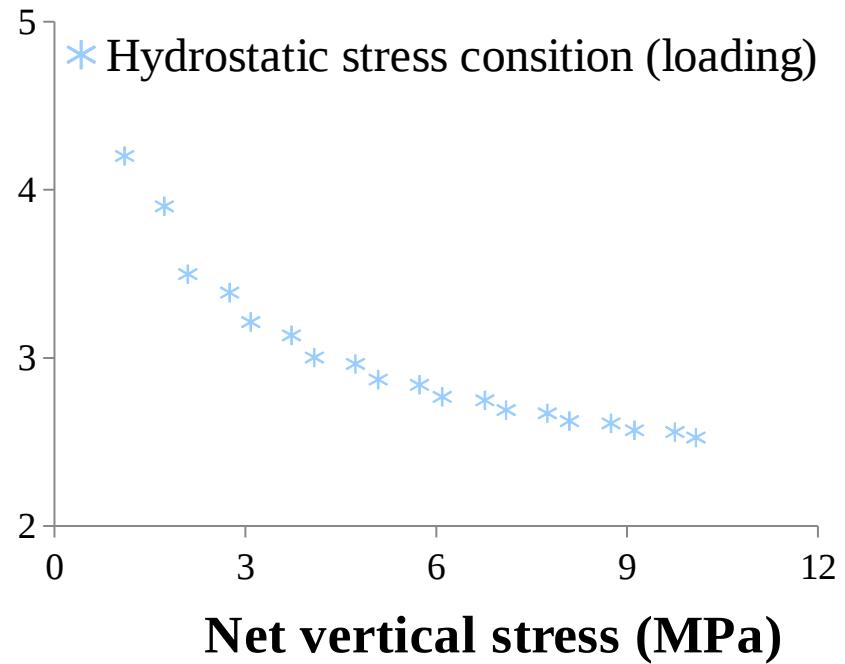
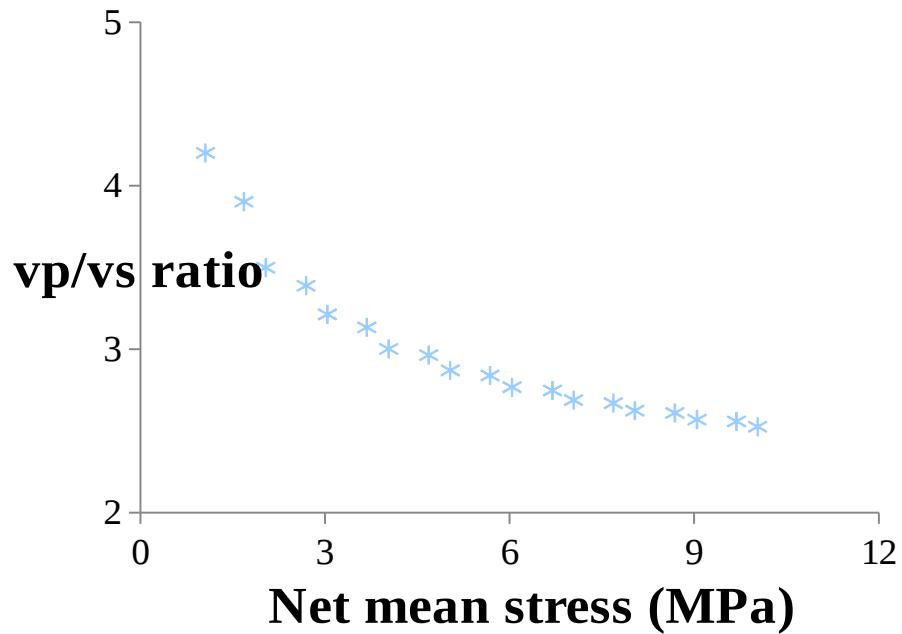
Ottawa sand data from triaxial set-up, showing apparent data collapse when v_p/v_s is plotted against net mean stress

v_p/v_s : The role of Stress Path (only for sand)



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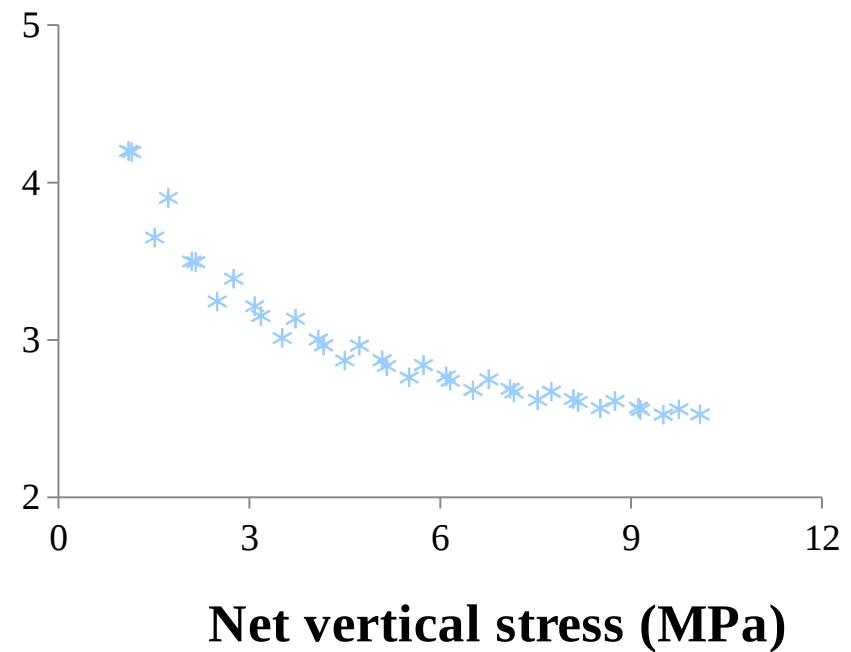
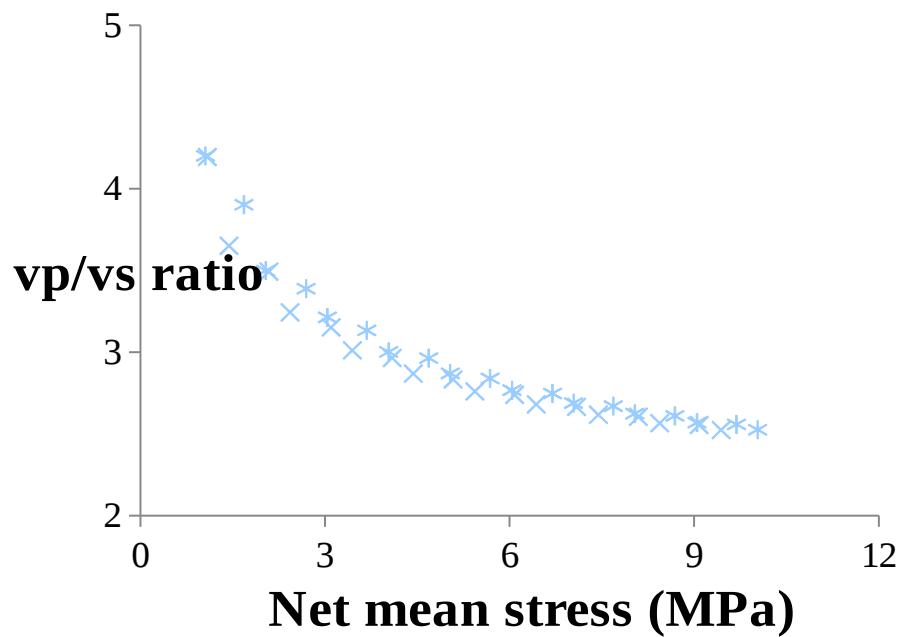
v_p/v_s : The role of Stress Path (only for sand)



Ottawa sand data from triaxial set-up, showing apparent data collapse when v_p/v_s is plotted against net mean stress

v_p/v_s : The role of Stress Path (only for sand)

- * Hydrostatic stress condition (loading)
- * Hydrostatic stress condition (unloading)



Ottawa sand data from triaxial set-up, showing apparent data collapse when v_p/v_s is plotted against net mean stress

Conclusions

- Comparison between measured dry and saturated anisotropy parameters are conformable with theory within experimental uncertainty
- v_p/v_s relation is sensitive to fluid saturation, stress, lithologies and state of consolidation.
- Well known v_p/v_s trends fail to explain v_p/v_s relation for unconsolidated sandy lithologies but fairly capture for clayey lithologies.

Acknowledgements

ROSE Program at NTNU for financial support

Jørn Stenebråten & others in the Formation Physics
Laboratory at SINTEF & NTNU