Seismic wavepropagation concepts applied to the interpretation of marine CSEM data

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Outline

Introduction

Theory

Comparing seismic and controlled-source electromagnetic fields

Summary



Seabed seismic nodes





3D CSEM

Source: Electric dipole ~ surface tow or 40 m above seabed Receivers: Voltmeters and coils at the seabed Typical CSEM frequency range: 0.1 Hz – 5Hz



Measure horizontal electric and magnetic fields

Amplitude (Log scale)

 $E \downarrow x (x, \omega) = |E \downarrow x (x, \omega)| e^{\uparrow} i \phi(x, \omega)$

Snohvit 01Tx004ab, Snohvit_3Dinvrot_allTx, 01Rx040a 0.5Hz 0.0001 1e-06 Rx Magnitude [V/Am^2] for E and [1/m^2] for H $\,$ • ÷ 1e-08 Magnetic 1e-10 Electric 1e-12 1e-14 -5,000 5,000 -15,000 -10,000 Ó 10,000 15,000 Offset [m]

Phase



$E \downarrow x (x, \omega), E \downarrow y (x, \omega), H \downarrow x (x, \omega), H \downarrow y (x, \omega)$

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Reflection coefficients Wave propagation Conductivity for EM (diffusive fields/waves)

Review of elastic and electromagnetic wave propagation in horizontally layered media

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ABSTRACT

The objective of this paper is to provide a unified treatment of elastic and electromagnetic (EM) wave propagation in horizontally layered media for which the parameters in the partial differential equations are piece-wise continuous functions of only one spatial variable. By applying a combination of Fourier, Laplace, and Bessel transforms to the partial differential equations describing the elastic or EM wave propagation I obtain a system of 2n linear ordinary differential equations. The $2n \times 2n$ coefficient matrix is partitioned into $4 n \times n$ submatrices. By a proper choice of variables, the diagonal submatrices are zero and the offdiagonal submatrices are symmetric.

mission matrices for two inhomogeneous layers is done by Redheffer's star product. This composition rule has been derived for P-SV waves by Kennett. The inverse of the star product, apparently unknown in seismology, is also given. This is a rule which may be used to remove the effect of an inhomogeneous layer at the top or bottom of a stack of layers. Such layer stripping techniques have possible applications in general inversion schemes. It is also shown that the reflection and transmission matrices of an inhomogeneous medium can be found by solving a matrix Riccati equation.

For a stack of inhomogeneous layers bounded above by a

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On the electromagnetic fields produced by marine frequency domain controlled sources

A. D. Chave

Forced oscillations of energy in a diffusive medium such as (12) and (13) describe are sometimes called diffusion waves (Mandelis 2006), and it is common in the geophysical literature to refer to CSEM fields using wave equation terminology. However, both (12) and (13) are parabolic diffusion equations rather than hyperbolic wave equations. In one dimension, a parabolic equation has only a single family of characteristic curves (lines of constant t), whereas a hyperbolic equation has two such families (lines of constant $x \pm ct$, where c is the phase velocity). Because they are not invariant under the transformation $t \rightarrow -t$, solutions to parabolic equations evolve unidirectionally forward in time simultaneously at all points away from a source. This set of traits precludes the existence of reflection (and concomitantly, refraction) at interfaces, as well as the use of ray physics. Mandelis *et al.* (2001) summarize the arguments. Consequently, terminology from and analogies to wave phenomena will be avoided in the sequel.

Seismic wavepropagation concepts are useless!

Or maybe not?



The acoustic wave equation

$$\rho \partial \downarrow t \, \boldsymbol{v} = -\nabla P + \boldsymbol{f} \, \boldsymbol{f} \, \boldsymbol{S}$$
 Newton's second law

 $\kappa \partial \downarrow t P = -\nabla \cdot \boldsymbol{v}$

Hooke's law for acoustic medium

Pressure: *P* Particle velocity: \boldsymbol{v} Density: ρ Compliance: $\kappa = 1/M$ Source force density: *f*1*S*

These two equations can be combined and give a wave equation.

Assuming constant density:

 $\nabla 12 P(\mathbf{x},t) - \rho \downarrow 0 \kappa(\mathbf{x}) \partial \downarrow t 12 P(\mathbf{x},t) = \nabla f \uparrow S(\mathbf{x},t)$



The electromagnetic (Maxwell) field equations

 $\varepsilon \partial \downarrow t \mathbf{E} + \sigma \mathbf{E} = \nabla \times \mathbf{H} - \mathbf{J} \uparrow S$

Ampere's law

 $\mu \downarrow 0 \ \partial \downarrow t H = -\nabla \times E$

Faraday's law

Electric field: *H* Magnetic field: *H* Conductivity: σ Resistivity: $\rho=1/\sigma$ Electric permittivity ε Magnetic permeabillity of vaccum: $\mu l 0 = 4\pi \times 10 \ tau - 7$ H/m Source current density: *J1S*

Induction current can be neglected for low frequency geophysical applications



The electromagnetic (Maxwell) field equations

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Electric field: *E* Magnetic field: *H* Conductivity: σ Resistivity: $\rho=1/\sigma$ Electric permittivity ε Magnetic permeabillity of vaccum: $\mu \downarrow 0 = 4\pi \times 10 \ tau - 7$ H/m Source current density: *J*tauS

Induction current neglected for low frequency geophysical applications



Solution by transforming PDE

 $\sigma(\boldsymbol{x})\boldsymbol{E}(\boldsymbol{x},t) = \boldsymbol{\nabla} \times \boldsymbol{H}(\boldsymbol{x},t) - \boldsymbol{J} \boldsymbol{\uparrow} \boldsymbol{S}(\boldsymbol{x},t)$

 $\mu \downarrow 0 \; \partial \downarrow t \; \boldsymbol{H}(\boldsymbol{x},t) = - \boldsymbol{\nabla} \times \boldsymbol{E}(\boldsymbol{x},t)$

Analytical transform

 $\varepsilon'(\mathbf{x})\partial \downarrow t' \mathbf{E}'(\mathbf{x},t') = \nabla \times \mathbf{H}'(\mathbf{x},t') - \mathbf{J} \uparrow' \uparrow s(\mathbf{x},t')$

 $\mu \downarrow 0 \; \partial \downarrow t' \; \boldsymbol{H}'(\boldsymbol{x},t') = - \boldsymbol{\nabla} \times \boldsymbol{E}'(\boldsymbol{x},t')$

$$\varepsilon \ell'(\mathbf{x}) = \sigma(\mathbf{x})/2\omega \ell 0 \quad \omega \ell 0 > 0$$

Fields and parameters for fictitious (transformed) time domain is primed.

Transform back to real time domain given by:

 $\boldsymbol{E}(\boldsymbol{x},t) = \int 0 \uparrow T \, dt \, \uparrow' \, W(t,t \uparrow',\omega \downarrow 0) \boldsymbol{E} \uparrow' \, (\boldsymbol{x},t \uparrow') H(t)$

 $W(t,t\uparrow',\omega\downarrow 0) = -1/2\omega\downarrow 0 \; \partial\downarrow t' \; (1/2\;\sqrt{2}\omega\downarrow 0\;/\pi\;\;t'/t\uparrow 3/2\;\;e\uparrow -2\omega\downarrow 0\;t'\uparrow 2\;/4t\;)$

Solution by transforming PDE

$$\varepsilon'(\boldsymbol{x}) \partial \downarrow t' \boldsymbol{E}'(\boldsymbol{x},t') = \boldsymbol{\nabla} \times \boldsymbol{H}'(\boldsymbol{x},t') - \boldsymbol{J} \boldsymbol{f}' \uparrow \boldsymbol{s}(\boldsymbol{x},t')$$

 $\mathcal{E}\mathcal{N}(\mathbf{x}) = \sigma(\mathbf{x})/2\omega \mathbf{1}0$

 $\mu \downarrow 0 \; \partial \downarrow t' \; \boldsymbol{H}'(\boldsymbol{x},t') = - \boldsymbol{\nabla} \times \boldsymbol{E}'(\boldsymbol{x},t')$

 $c(\mathbf{x}) = \sqrt{1/\mu} \sqrt{0} \varepsilon t'(\mathbf{x})$

Propagation velocity:

$$c(\mathbf{x}) = \sqrt{2\omega \downarrow 0} \rho(\mathbf{x}) / \mu \downarrow 0$$

Transform from fictitous time to real time.

 $\boldsymbol{E}(\boldsymbol{x},t) = \int 0 \uparrow T \, dt \, \uparrow' \, W(t,t \uparrow',\omega \downarrow 0) \boldsymbol{E} \uparrow' \, (\boldsymbol{x},t \uparrow') H(t)$

Transform is simple going from fictitous time to «real» frequency.

 $\boldsymbol{E}(\boldsymbol{x},\omega) = \int 0 \uparrow T \, dt \, \boldsymbol{t}' \, \boldsymbol{E}'(\boldsymbol{x},\boldsymbol{t}') \, e \uparrow -\sqrt{\omega\omega \downarrow 0} \, t \, \boldsymbol{t}' \, e \uparrow i \sqrt{\omega\omega \downarrow 0} \, t \, \boldsymbol{t}'$



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A general correspondence principle for time-domain electromagnetic wave and diffusion fields

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To obtain the time-domain expressions for each Γ , the Schouten–Van der Pol theorem in the theory of Laplace transformation is applied. This theorem relates time-domain results that are associated with the replacement of the Laplacetransform parameter s by a function of s, subject to some restrictions. For the present case, the result for the replacement of s by $(\alpha s)^{1/2}$ is needed. Using eqs (A6), (A9) and (A10) from Appendix A, it is found that

 $\Gamma^{E,H|J,K}(\mathbf{r},\mathbf{r}',t) = \left[\int_{\tau=0}^{\infty} W^{E,H|J,K}(t,\tau,\alpha) \mathscr{G}^{E,H|J,K}(\mathbf{r},\mathbf{r}',\tau) d\tau\right] H(t), \quad (24)$

where the intervening kernel functions $W^{E,H|J,K}$ are given by

$$W^{E,J} = \frac{1}{2} \left(\frac{1}{\alpha \pi} \right)^{1/2} \frac{1}{t^{3/2}} \left(\frac{\alpha \tau^2}{2t} - 1 \right) \exp\left(-\frac{\alpha \tau^2}{4t} \right) H(t), \quad (25)$$

$$W^{H,J} = \frac{1}{2} \left(\frac{\alpha}{\pi} \right)^{1/2} \frac{\tau}{t^{3/2}} \exp\left(-\frac{\alpha \tau^2}{4t} \right) H(t), \qquad (26)$$

$$W^{E,K} = \frac{1}{2} \left(\frac{\alpha}{\pi} \right)^{1/2} \frac{\tau}{t^{3/2}} \exp \left(-\frac{\alpha \tau^2}{4t} \right) H(t),$$
 (27)

$$W^{H,K} = \left(\frac{\alpha}{\pi t}\right)^{1/2} \exp\left(-\frac{\alpha \tau^2}{4t}\right) H(t), \qquad (28)$$



Acoustic and electromagnetic wave equations

The acoustic wave equation

 $\nabla 12 P(\mathbf{x},t) - 1/c 12 (\mathbf{x}) \partial \downarrow t 12 P(\mathbf{x},t) = \nabla f f S(\mathbf{x},t)$

 $c(\mathbf{x}) = \sqrt{1}/\rho \downarrow 0 \kappa(\mathbf{x})$

Acoustic velocity

The electromagnetic wave equation

 $\nabla \uparrow 2 \boldsymbol{E}'(\boldsymbol{x},t\uparrow') - \nabla (\nabla \cdot \boldsymbol{E}\uparrow'(\boldsymbol{x},t')) - 1/c\uparrow 2 (\boldsymbol{x}) \partial \downarrow t\uparrow' \uparrow 2 \boldsymbol{E}'(\boldsymbol{x},t') = \mu \downarrow 0 \partial \downarrow t' \boldsymbol{J}\uparrow S(\boldsymbol{x},t')$

 $c(\mathbf{x}) = \sqrt{1/\mu} \sqrt{0} \varepsilon t'(\mathbf{x})$

Electromagnetic velocity

$$c(\mathbf{x}) = \sqrt{2}\omega \downarrow 0 \rho(\mathbf{x}) / \mu \downarrow 0$$

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3D acoustic simulation

Waterdepth 2 km «High velocity» subsurface (2 – 6 km) Source 40 m above seabed (1.96 km) Recording at seabed (2 km)





Vertical component of particle velocity























Air-water reflection at seabed after ~ 2.7 s (4000 m / 1500 m/s)





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Traces normalized to unity



Also diffractions and multiples



3D acoustic simulation and 3D EM simulation









Resistivity/conductivity model maps into velocity model

























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Acoustic

Electromagnetic





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Traces normalized to unity

Acoustic



Electromagnetic



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 $E \downarrow i (\mathbf{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\mathbf{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$









 $E \downarrow i (\boldsymbol{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\boldsymbol{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$





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 $E \downarrow i (\mathbf{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\mathbf{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$





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 $E \downarrow i (\mathbf{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\mathbf{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$





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 $E \downarrow i (\mathbf{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\mathbf{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$





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 $E \downarrow i (\mathbf{x}, \omega) = \int 0 \uparrow T = dt' E \uparrow' \downarrow i (\mathbf{x}, t') e \uparrow - \sqrt{\omega \omega \downarrow 0} t \uparrow'$ $e \uparrow i \sqrt{\omega \omega \downarrow 0} t \uparrow'$





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Summary

Transform from fictitious wave-domain time response to «real-world» frequency response by temporal integral

No spatial integration in transform:

What is a reflection or refraction in the EM wave domain stays a reflection or refraction after the transform to the real frequency domain

No problem using concepts like reflections, refractions, diffractions etc for interpretation of marine CSEM responses Note: «use of ray physics» is in principle possible



Summary

For formation resistivities typical for marine sediments and for typical CSEM frequencies: First arrivals are important - Refractions and (possibly) reflections at small offsets - Refractions and guided events at intermediate and large offsets

Guided field in thin resistor gives relatively large electric (and magnetic) fields at large offset. The effect is so strong that it can be used as a hydrocarbon indicator

Marine CSEM responses can be interpreted by inspecting events in the EM wave domain

Marine CSEM data have common properties with refraction seismic data and this may partly explain the relative success of 3D FWI of CSEM data.

FWI of CSEM data

Typical for 3D CSEM data:

Low frequencies

Large source-receiver offsets

Wide azimuth

Data dominated by refraction (transmission) type events. Reflections «filtered out» by MN.

Source function measured.



