

FULL-WAVEFORM INVERSION

Practicalities and Progress

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Outline

- Overview of full-waveform inversion
- Towed-streamer field example
- OBC field example, pre-processing, validation
- Other parameters
- Method
- Pitfalls and practicalities
- Quality assurance
- New directions
- Q & A

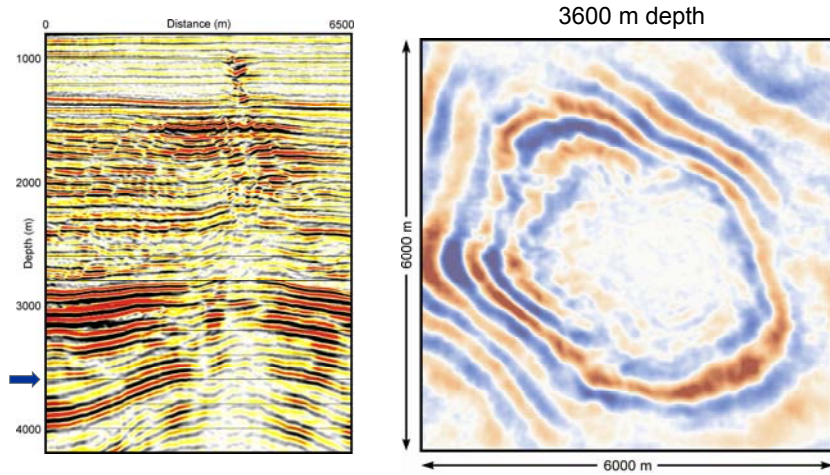
Full Waveform Inversion

- Method for generating high-resolution high-fidelity models of physical properties in the subsurface
- Seeks a model which can predict the entire recorded wavefield, wiggle-for-wiggle
- Has become practical for 3D field datasets within the last few years
 - software advances
 - hardware advances

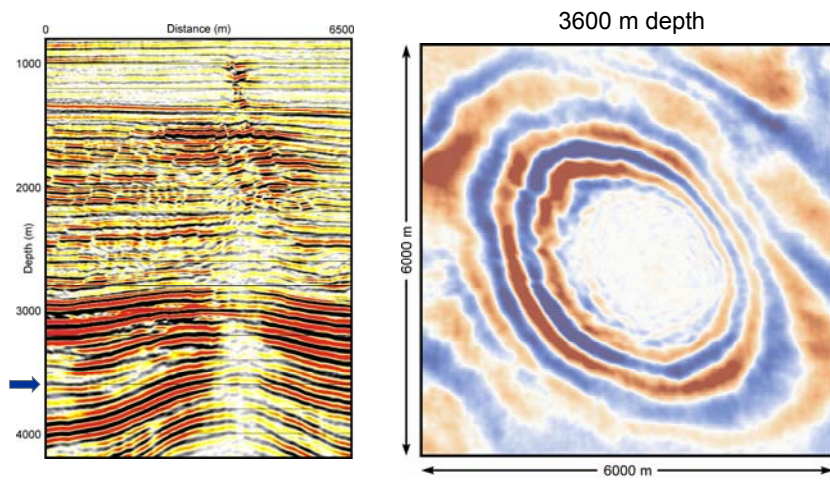
Full Waveform Inversion

- Generates high-resolution model of physical properties
- In principle any property that affects seismic data is possible:
 - p-wave attenuation
 - p-wave anisotropy
 - s-wave velocity
 - density
 - elastic anisotropy
 - anelastic anisotropy
- Commercially → p-wave velocity

RTM with tomography model



RTM with FWI model



Full Waveform Inversion

Most of what you know about conventional imaging will not apply to FWI workflows

- uses low frequencies
- uses transmitted arrivals
- iterative inversion from starting model
- details can be critical → does not fail elegantly

Travel-time tomography

- travel times
- ray theory
- cheap
- robust
- low resolution
 - ~ Fresnel zone
 - ~ $\sqrt{\lambda d}$
 - ~ 700 m

Full Waveform Inversion

- raw wavefield
- wave theory
- expensive
- still developing
- high resolution
 - ~ half wavelength
 - ~ $\lambda / 2$
 - ~ 140 m

Reverse Time Migration

- uses primary reflections only
- does not deal with multiples
- does not deal with transmitted arrivals
- semi-quantitative imaging
- needs a velocity model
- details may not be critical

Full Waveform Inversion

- uses the entire unprocessed wavefield
- inverts the multiples
- inverts the transmitted arrivals
- fully-quantitative inversion
- builds the velocity model
- details can be vital

Practicalities

- FWI is not yet robust
- Requires an accurate starting model
 - local minima
 - cycle skipping
- Careful QC is essential
- Synthetic testing desirable
- Different implementations and practitioners will affect outcomes

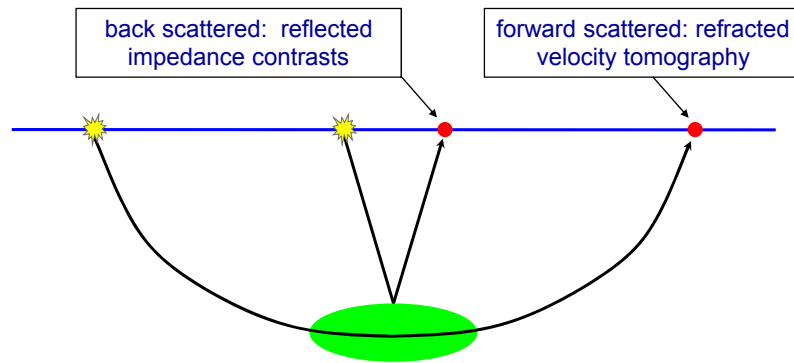
Applications

- Shallow
 - drilling hazards
 - land statics → dynamic corrections
- Intermediate
 - depth migration through heterogeneous overburden
 - delineation of salt flanks
- Deep
 - applied directly at the reservoir

Cost

- Full 3D acoustic FWI
 - commercialised and affordable
 - with TTI anisotropy
- Lower in cost/hardware than RTM
 - many iterations
 - but reduced bandwidth
 - compute scales as at least n^4

Two types of Imaging



Migration and Tomography

FWI uses both reflected and transmitted data:

- tomography from forward-scattered waves
- depth migration of back-scattered waves

Refractions → macro-velocity model

Reflections → impedance contrasts

Refraction *vs* Reflection FWI

There are currently two ways to formulate FWI:

- Use all incident angles to build a velocity model at all length scales
 - needs wide-angle, refracted, long-offset data
- Use near-normal-incident reflections to build a band-limited impedance model
 - reflection FWI needs a simple structure, clean data, and a superb starting model

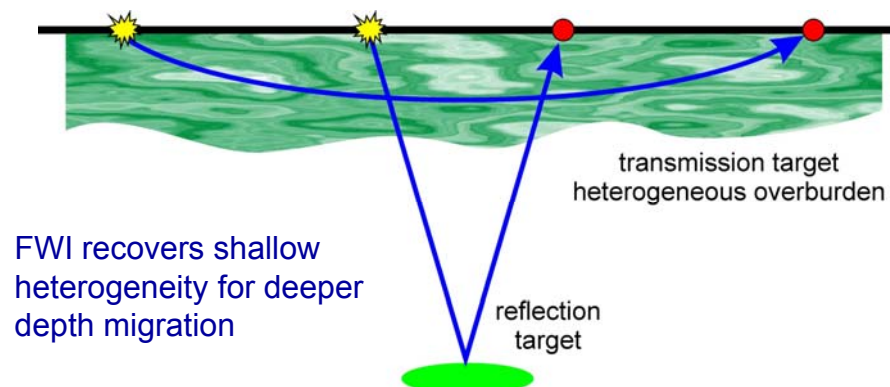
Acquisition for FWI

- Long offsets
 - 3 to 6 times target depth necessary
- Low frequencies
 - 2 to 3 Hz desirable
- Many azimuths desirable
 - narrow azimuth possible
- Dense acquisition not necessary

Common FWI workflow

1. Conventional acquisition, processing, model building & depth imaging
2. Use FWI to improve velocity model in top ~ 2 km of heterogeneous overburden
3. Re-migrate using RTM with the shallow FWI velocity model

Heterogeneous overburden



Field example

Samson Dome, Barents Sea

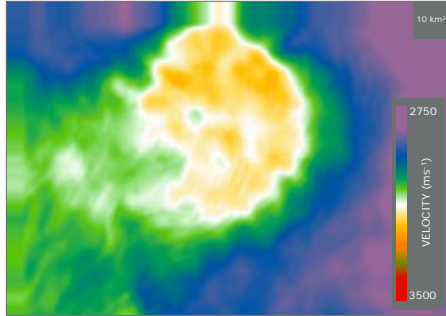
Morgan et al, 2013. *Next-generation seismic experiments*.
Geophysical Journal International, 195, 1657–1678.

Data courtesy of BG-Group and PL 534 partners

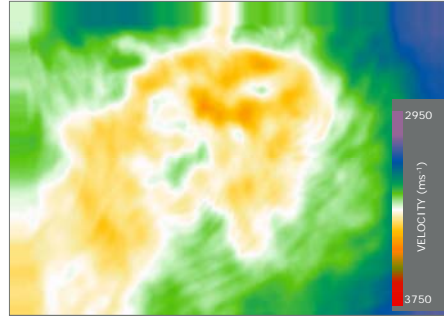
Samson Dome, Barents Sea

- Complex geological setting:
 - Faulted dome + erosional unconformity overlain by Quaternary
- FWI area ~ 1000 km²
- Acquisition parameters:
 - 10 streamers, 6km cable, 100m cable separation, 12.5m flip-flop, no low-cut in recording system, shot depth 5m, receiver depth 7m
- Pre FWI processing:
 - Swell noise attenuation, linear radon de-noise, bandpass 2-7 Hz

Starting velocity model



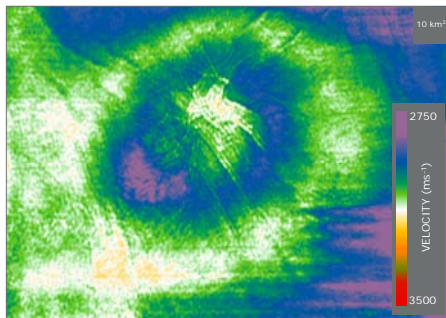
1100 m depth



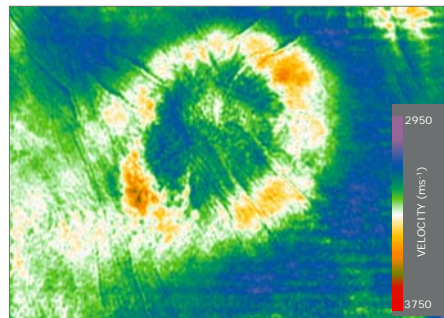
1350 m depth

faulted dome

FWI velocity model



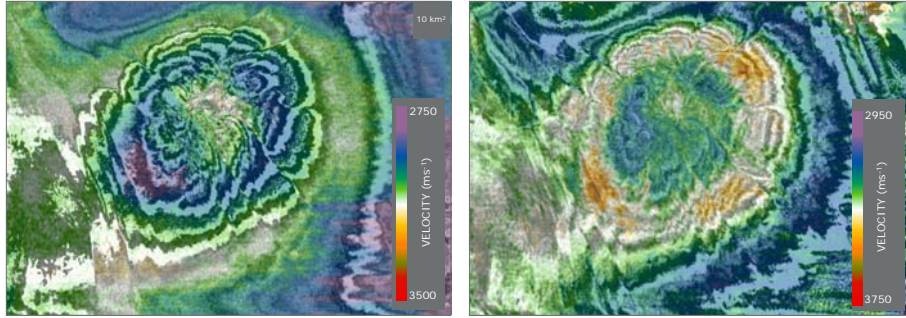
1100 m depth



1350 m depth

faulted dome

FWI velocity model with seismic overlay

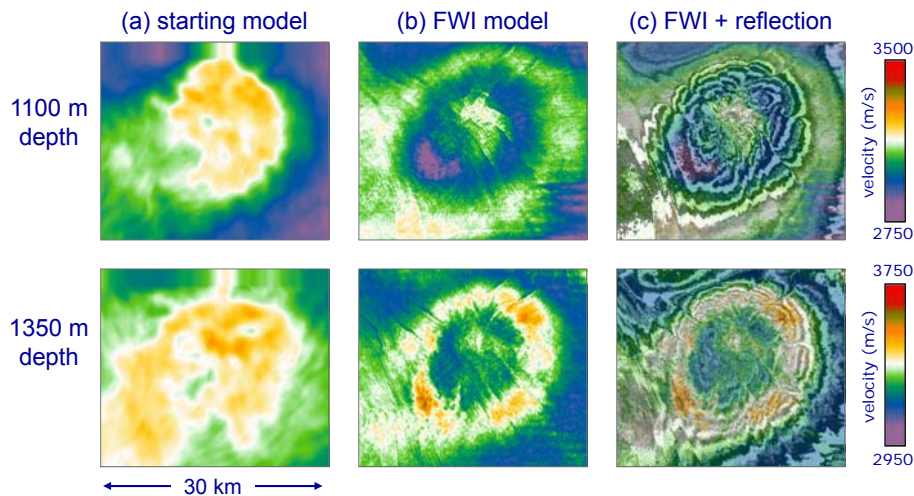


1100 m depth

1350 m depth

faulted dome

Surface streamer FWI



1100 m
depth

1350 m
depth

← 30 km →

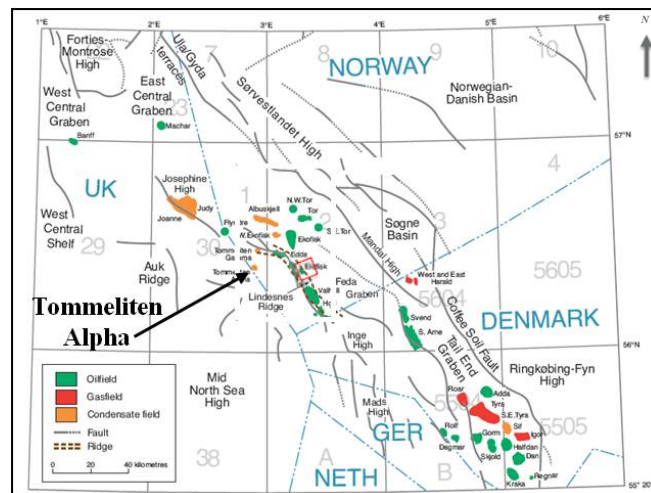
Field example

Tommeliten

Warner et al (2013) *Anisotropic 3D full-waveform inversion*.
Geophysics, 78, No 2, R59-R80.

Data courtesy of ConocoPhillips and PL 044 partnership

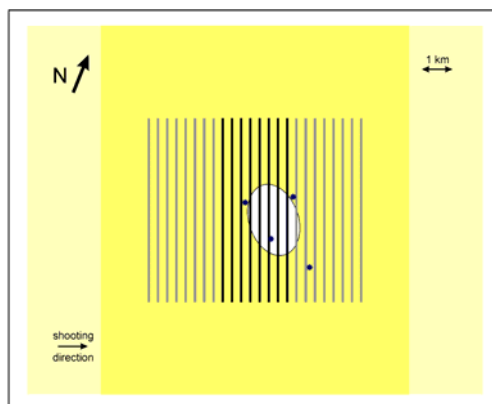
Tommeliten



Tommeliten

- 4-component OBC
- invert pressure data
- Vp model above reservoir
- shallow gas
- low velocities
- high attenuation
- significant anisotropy

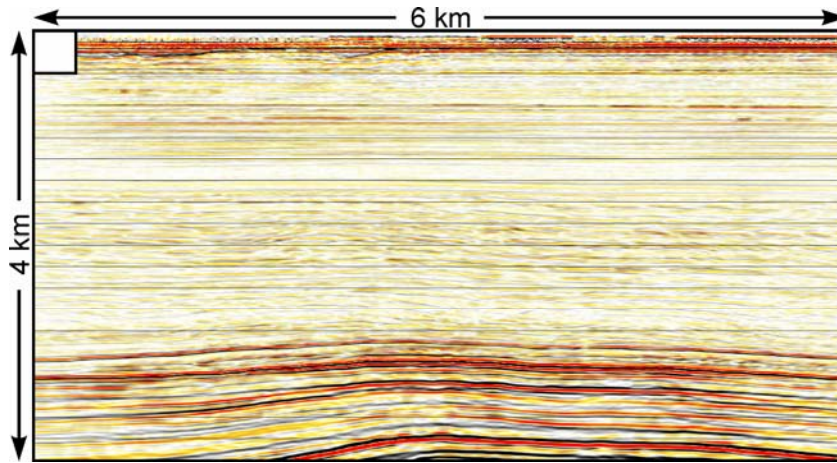
3D OBC field data



acquisition geometry

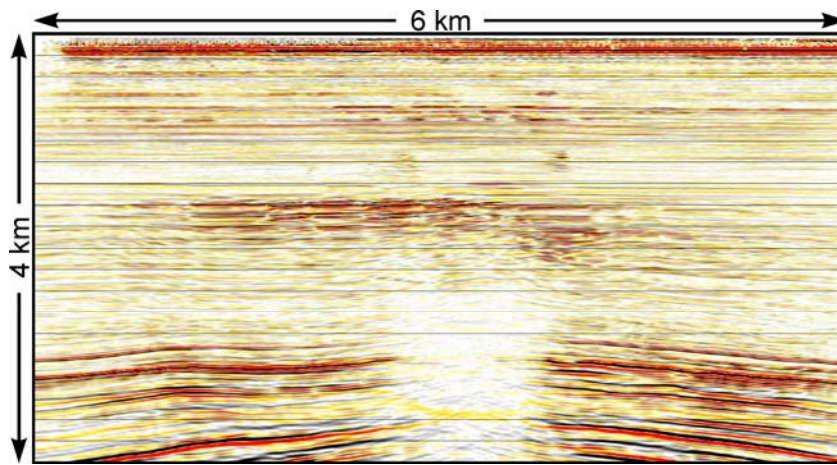
- 4C OBC
- 3 swaths of 8 cables
- 75 m water depth
- 6 km cables
- 25 m receiver spacing
- 300 m cable spacing
- 6000 receivers
- 25 m shot interval
- 75 m shot-line spacing
- 100,000 shots
- full azimuth to 7000 m
- max offset 11,000 m
- 180 sq km

PP PSDM



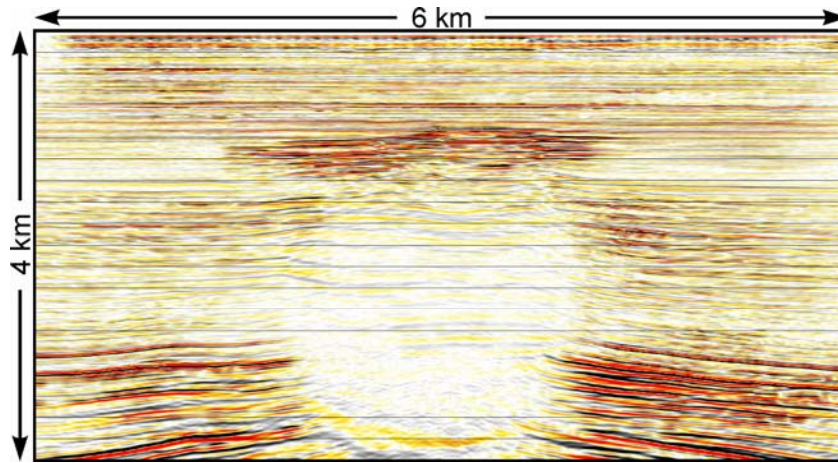
PZ-summed – deghosted and demultiplied

PP PSDM



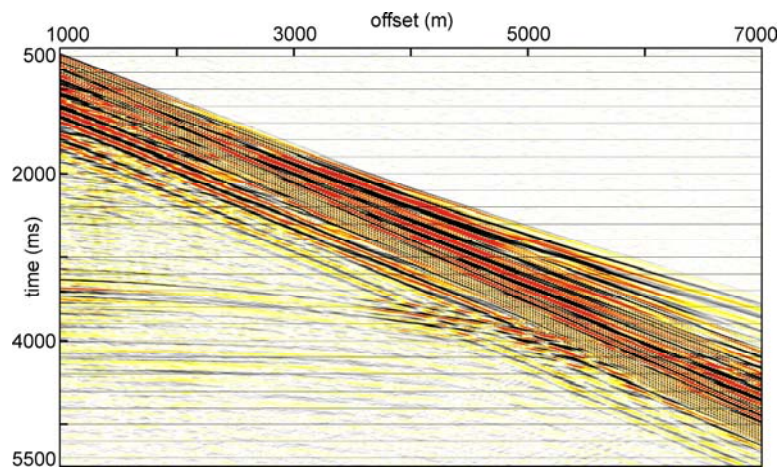
PZ-summed – deghosted and demultiplied

PP PSDM



PZ-summed – deghosted and demultiplexed

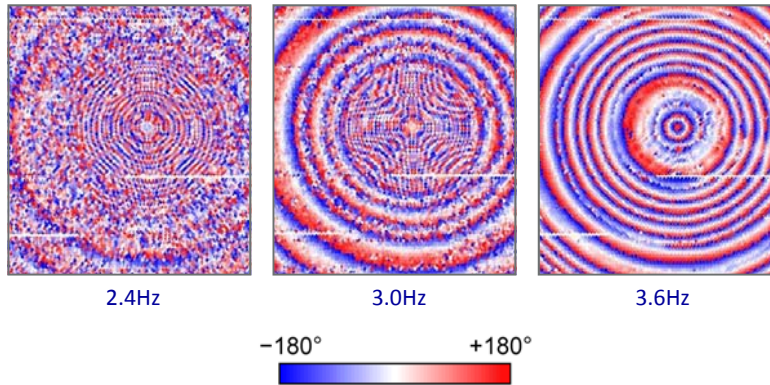
Raw shot record



hydrophone only – include all ghosts and multiples

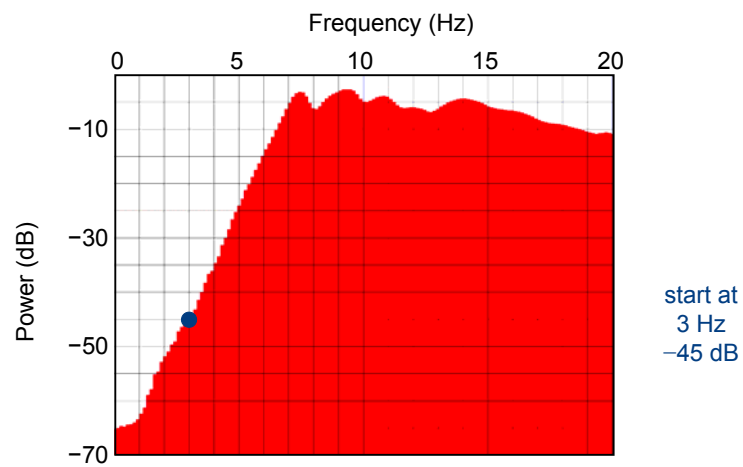
Picking the starting frequency

single-frequency phase



common receiver gather

Picking the starting frequency



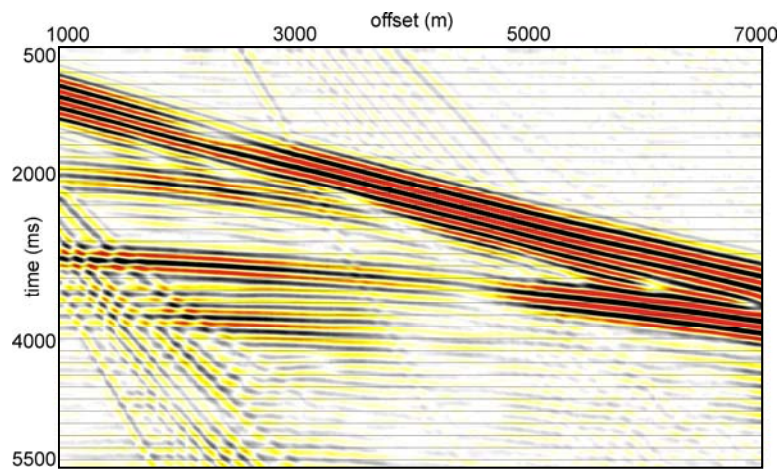
raw data – amplitude spectrum

Pre-processing

- No deghost
- No demultiple
- No debubble
- No wavelet shaping
- No low-cut filter
- No deconvolution
- No PZ sum
- No AGC
- No divergence correction

Usually essential to return to raw field data

Scholte waves at lowest frequencies



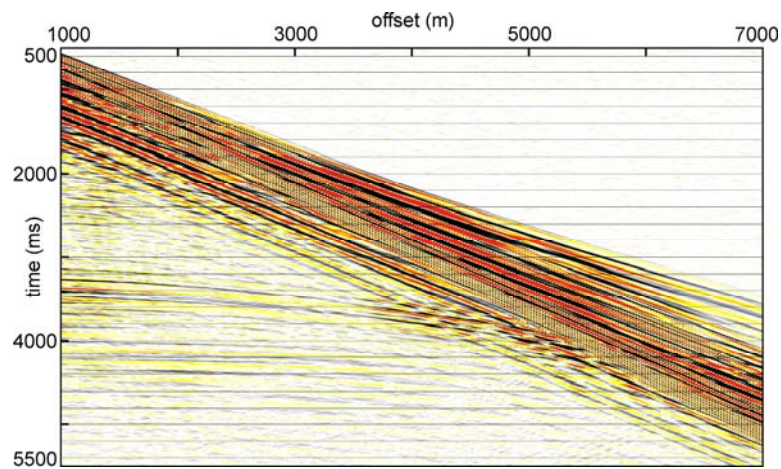
hydrophone

Pre-processing

- Mute ahead of first breaks
- Mute Scholte waves
- Truncate to 5500 ms
- Cut frequencies above 8 Hz
- Delete three quarters of receivers
- Delete two thirds of sources
- Delete offsets < 100 m
- Delete geophones, retain hydrophones only
- Apply source-receiver reciprocity

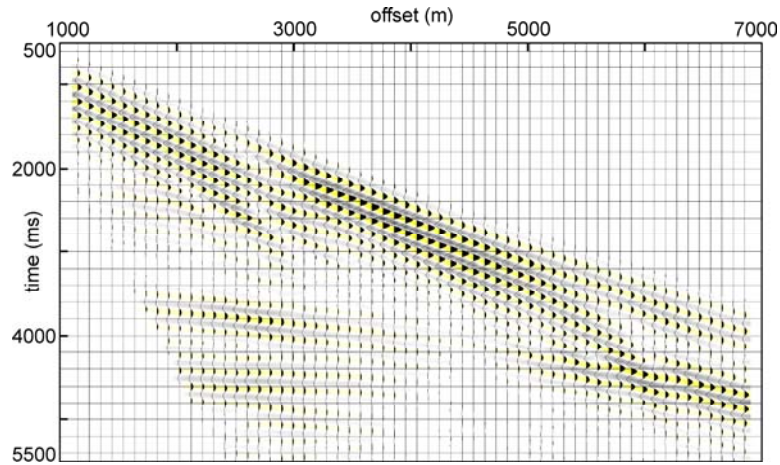
Most of this is to reduce compute time, and to avoid adding noise into the inversion

Raw shot record



hydrophone

Pre-processed for acoustic FWI



hydrophone

Pre-processing

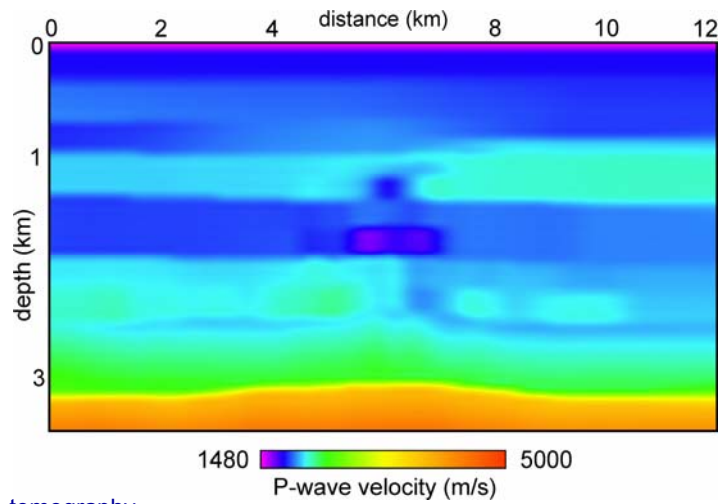
Surface streamer data:

- remove swell noise
- low-frequency de-noise
- shape amplitude spectrum to boost lowest frequencies

Land data:

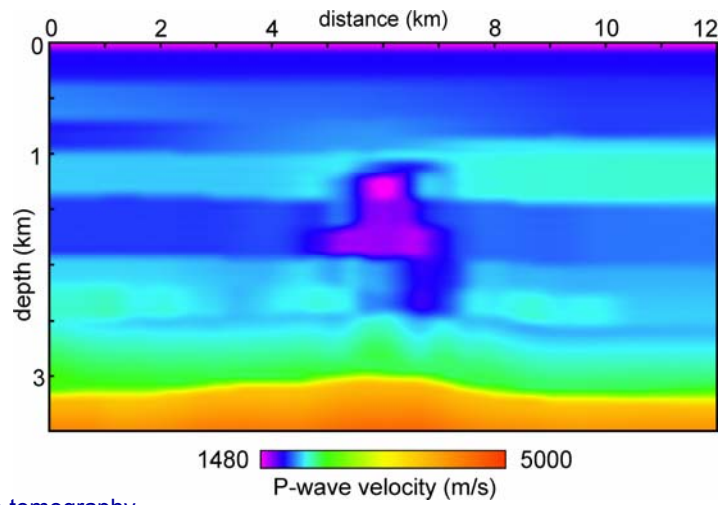
- compensate geophone roll-off at low frequency
- remove shear-waves, converted waves, surface waves
- remove local noise sources
- surface consistent wavelet
- interpolate additional sources
- convert geophones to hydrophones

Starting model



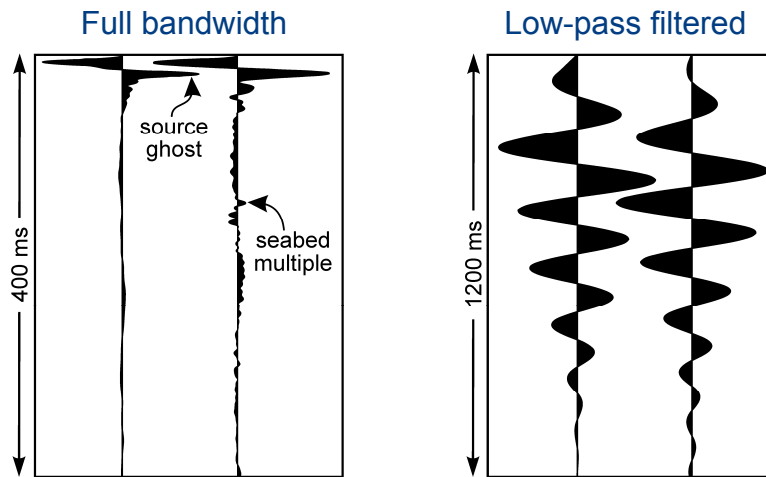
reflection tomography

Starting model



reflection tomography

Source wavelet



Contractor's wavelet vs Near-source OBH

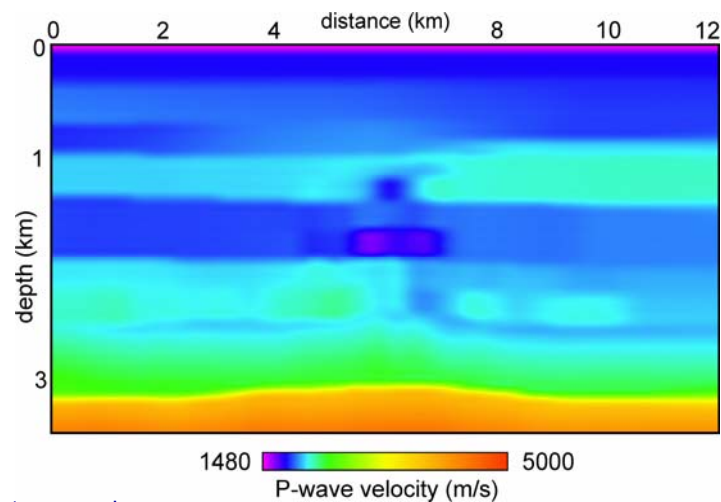
Wavelet

- Low-frequency wavelet
- Same zero-time as pre-processed data
- Same filters as pre-processed data
- Wavelet with no source ghost
- Can be non-causal

Inversion parameters

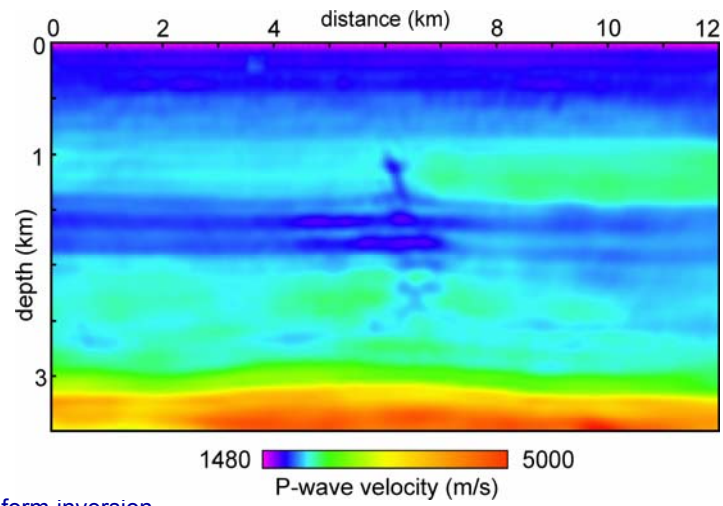
- Time domain, acoustic 3D, VTI anisotropy
- Hydrophones only → include ghosts and multiples
- Apply reciprocity
- 6000 → 1440 sources
- 80 sources per iteration
- Six frequency bands from 3.0 → 6.5 Hz
- 18 iterations per frequency
- Each source used once per frequency
- Amplitude equalisation
- Conjugate gradients
- Approximate diagonal Hessian

Starting model



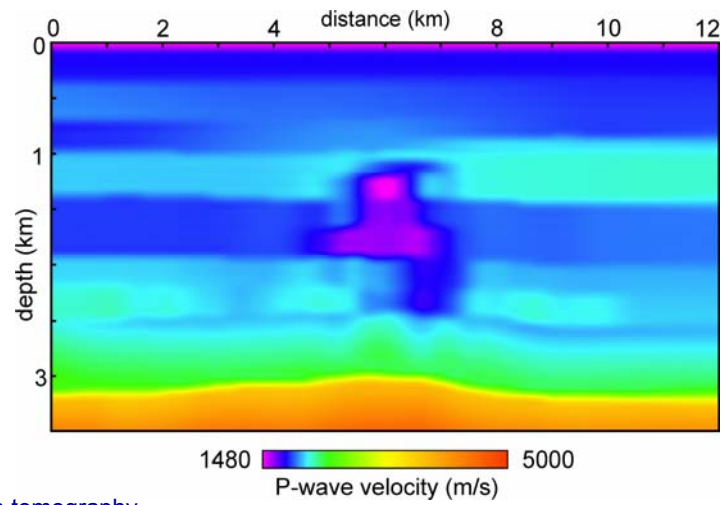
reflection tomography

FWI model



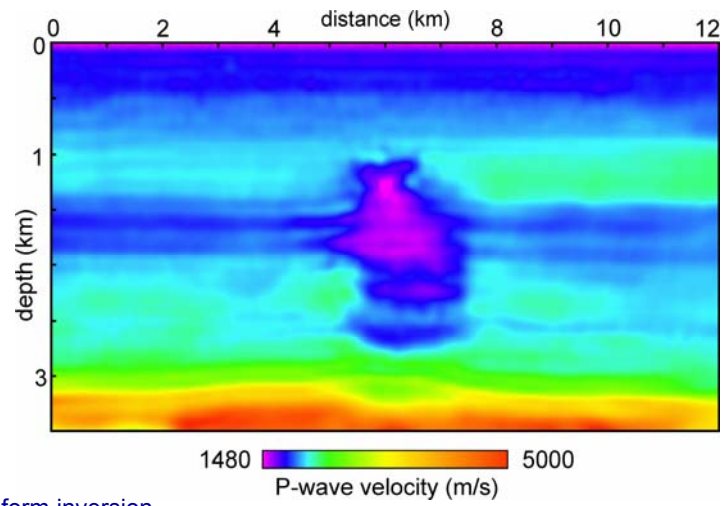
full-waveform inversion

Starting model



reflection tomography

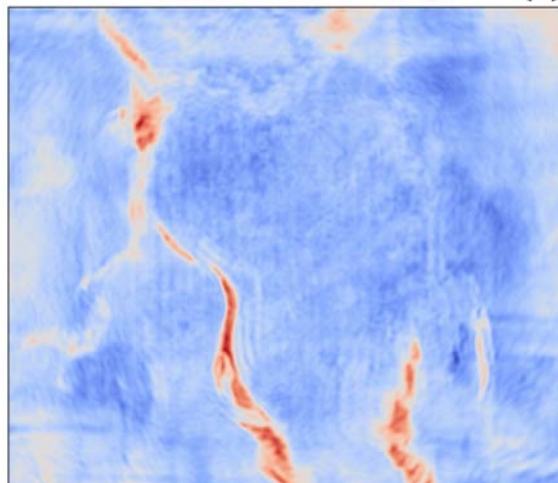
FWI model



FWI results

from homogeneous
start model

P-wave velocity (m/s)
1720 1950
1 km



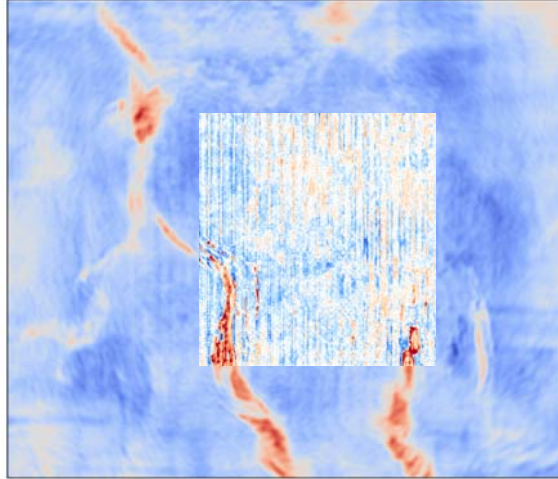
250 m depth

horizontal
depth slice

FWI results + original PSDM

from homogeneous
start model

P-wave velocity (m/s) 1720 1950 1 km

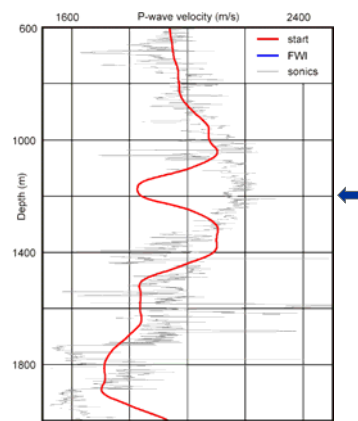
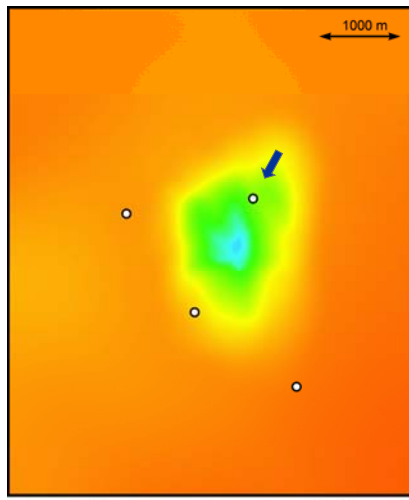


250 m depth

horizontal
depth slice

Starting model

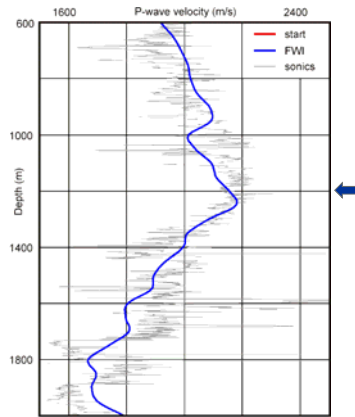
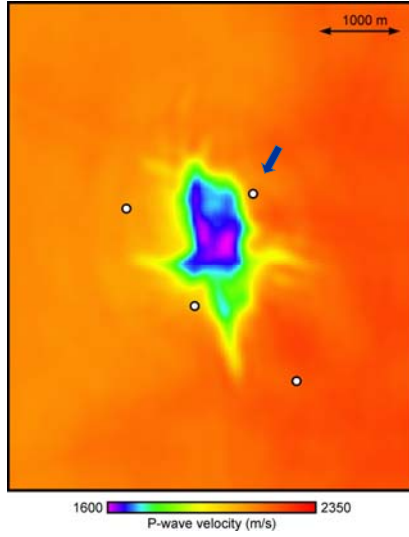
1200 m
depth



well log

FWI model

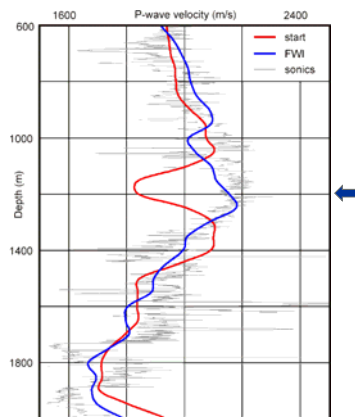
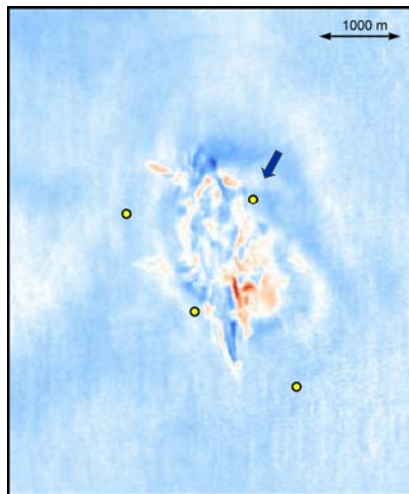
1200 m
depth



well log

PSDM

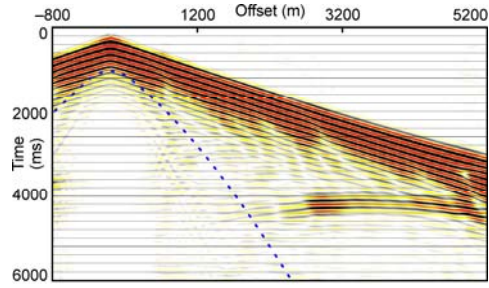
1200 m
depth



well log

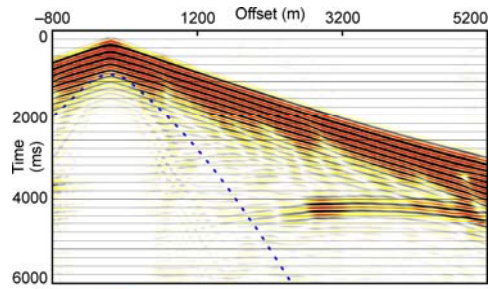
Field data

Field data

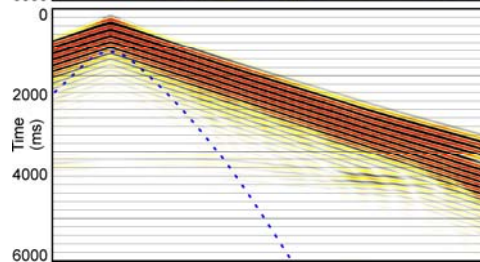


Start model

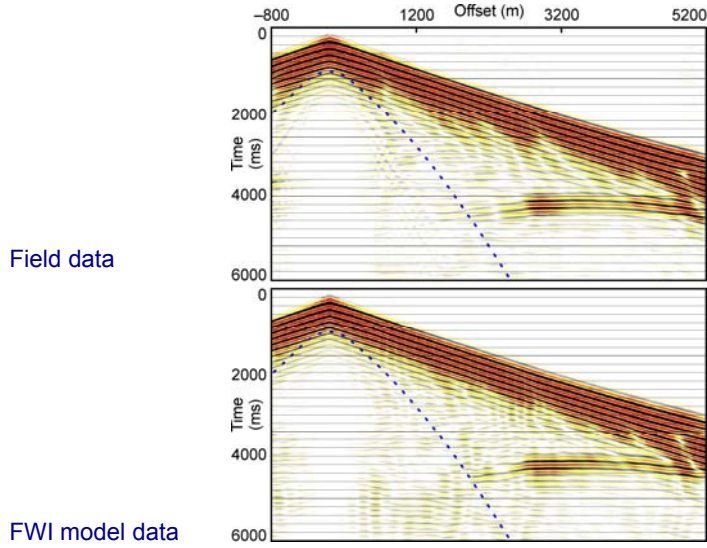
Field data



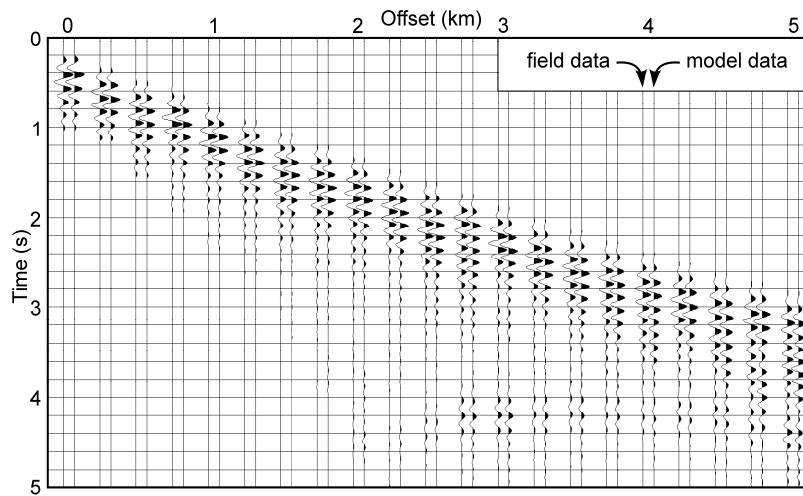
Start model data



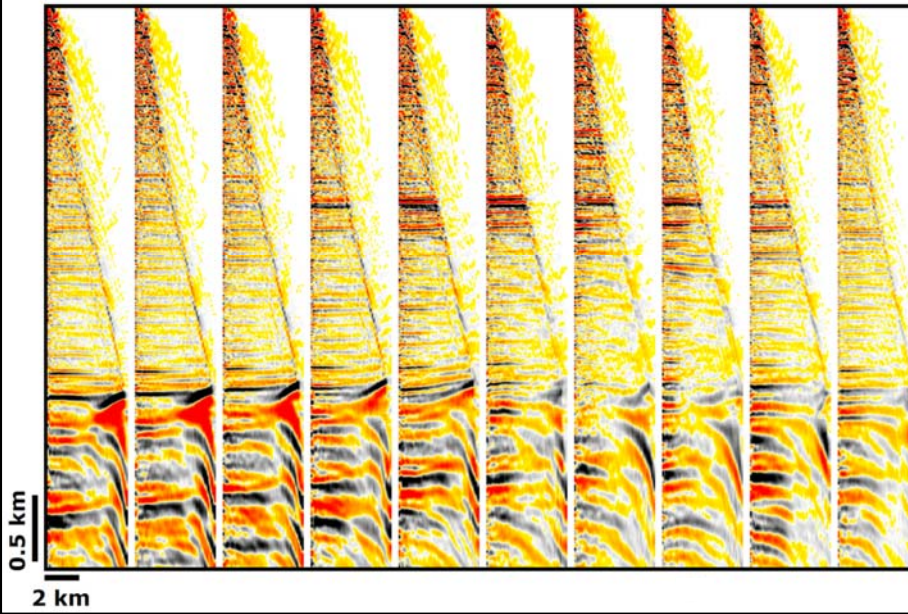
FWI model



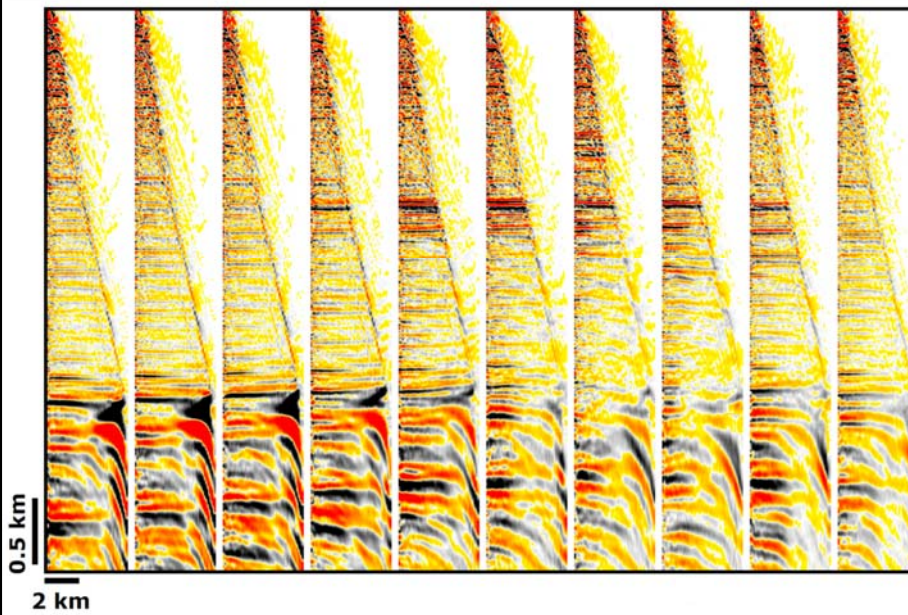
Match to Synthetics



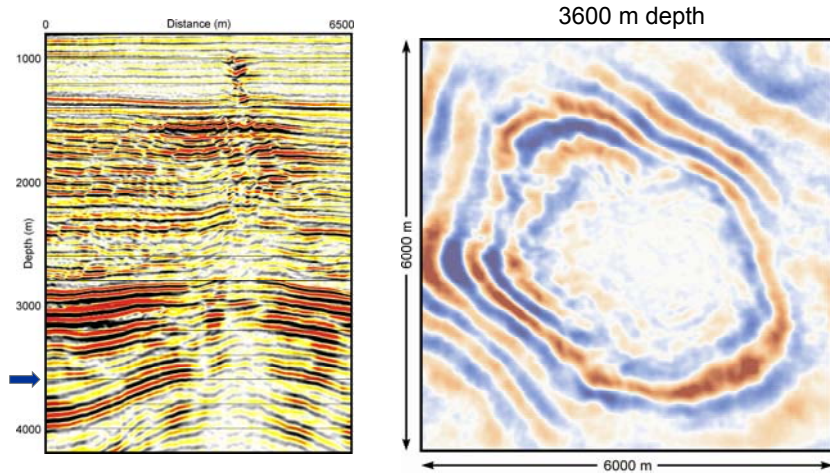
VTI Kirchhoff CIG's using starting velocity model



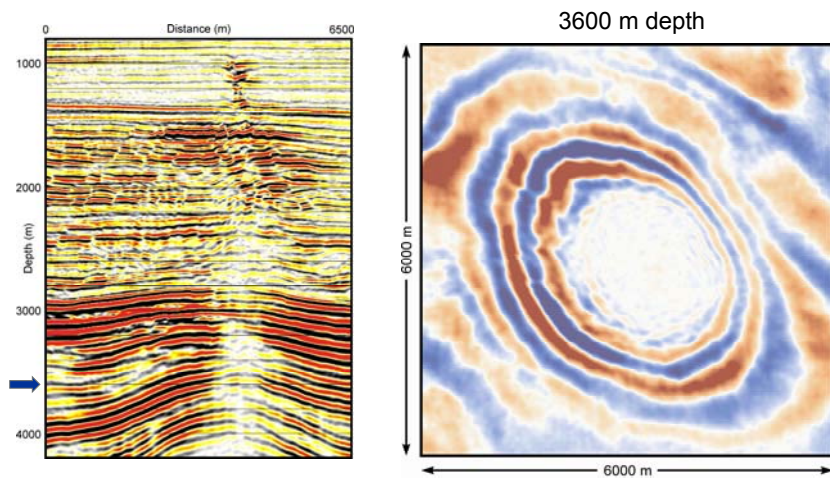
VTI Kirchhoff CIG's using FWI velocity model



RTM with PSDM model

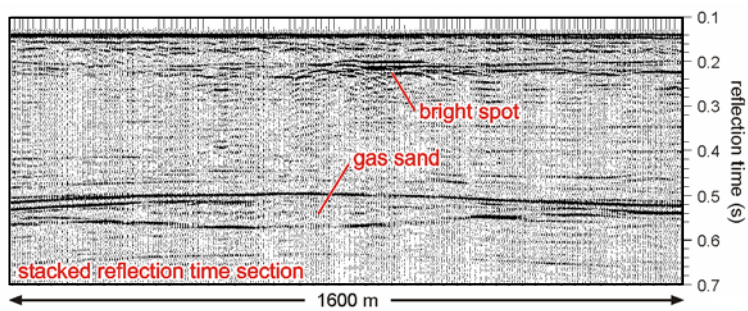


RTM with FWI model



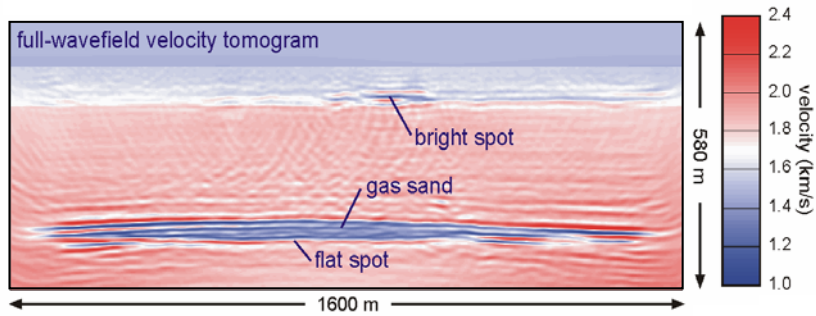
Other parameters

Field data – site survey



Hicks & Pratt (2001) Geophysics, v66, p598.

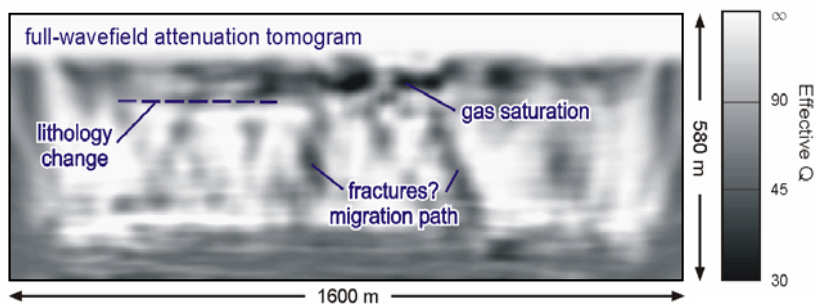
Acoustic wavefield tomography



Hicks & Pratt (2001) Geophysics, v66, p598.

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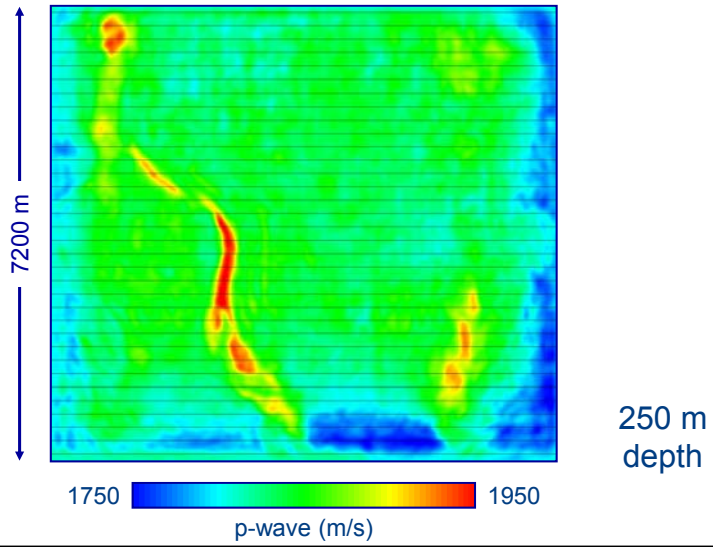
Attenuation tomography



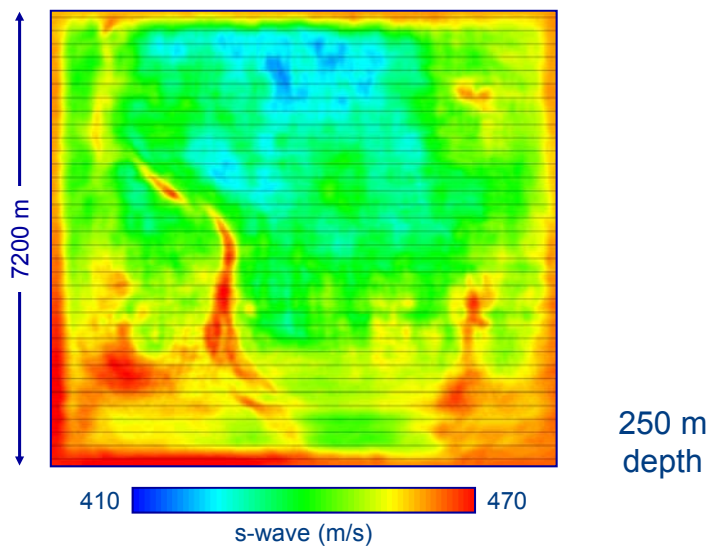
Hicks & Pratt (2001) Geophysics, v66, p598.

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Elastic FWI: P-wave



Elastic FWI: S-wave



Difficulties with elastic FWI

- S-wave starting model
- Cross talk to p-wave velocity
- Cross talk to density & attenuation
- Elastic anisotropy – s-wave splitting
- Compute cost

Elastic FWI

- Genuine elastic inversion is difficult...
...but is possible on 3D hydrophone data
- For p-wave RTM...
... not clear that elastic FWI is helpful
- For reservoir characterisation...
... need elastic, anisotropy & attenuation

Pitfalls & Practicalities

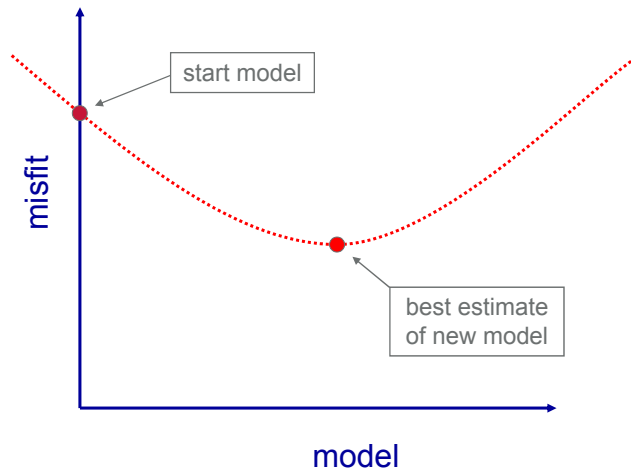
Pitfalls

- local minima
- cycle skipping
- inadequate low frequencies
- inadequate starting model

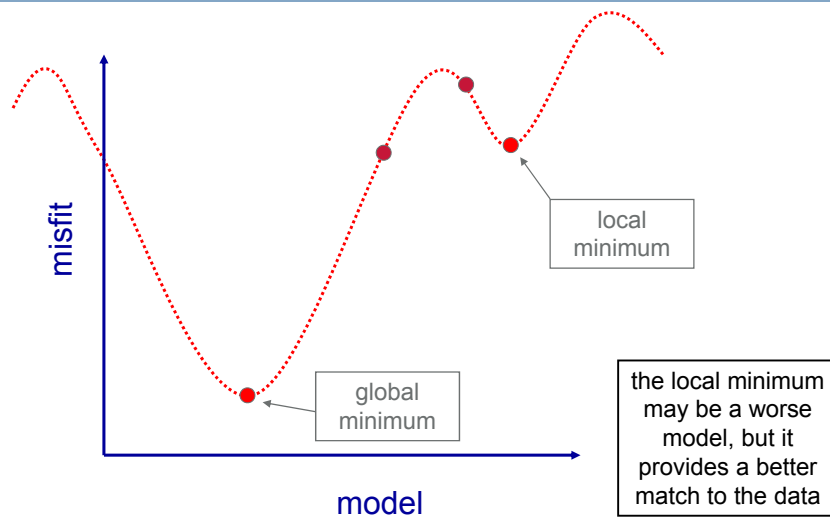
Essential that starting model is not cycle skipped

- low frequencies
- high-quality start model
- rigorous QC

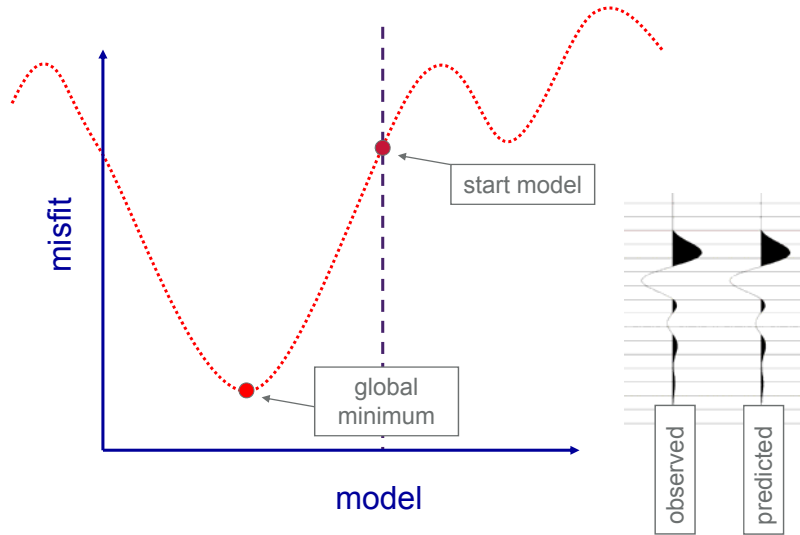
Local inversion



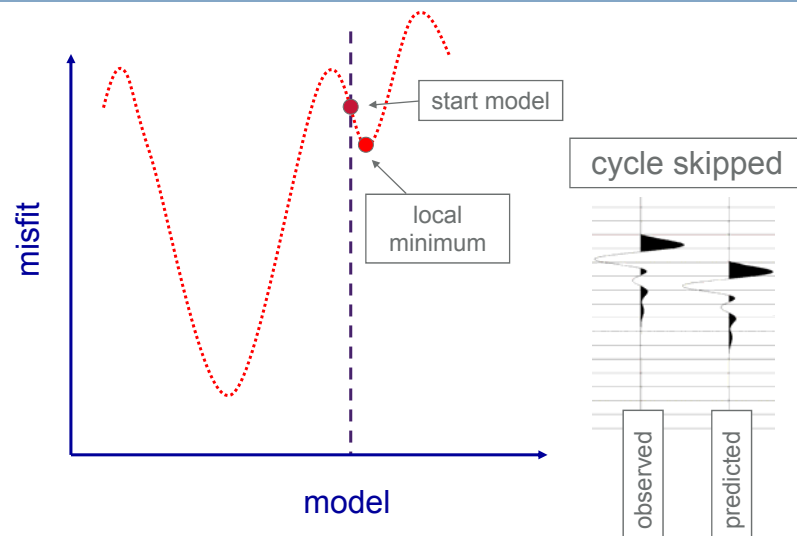
Local inversion



Low frequency



High frequency



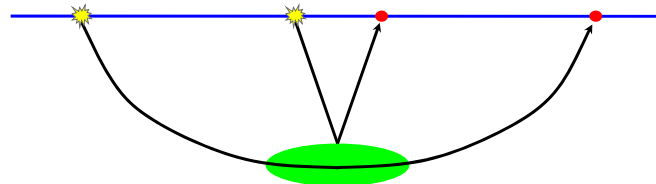
Free surface strategy

- The free surface:
 - generates ghosts
 - generates free-surface multiples
 - suppresses direct arrival
- Must match field data and FWI modelling

Free surface strategy

- Marine: put free surface in model,
use deghosted source,
leave all multiples in data,
leave all ghosts in data,
get the seabed correct.
- Land: put absorbing boundary in model,
remove free-surface multiples from data,
include ghosts and remnant multiples in
the source wavelet,
deal with synthetic direct arrival.

Insufficient offset



- Without long offsets:
FWI → least-squares reverse-time migration

FWI strategy

- low → high frequencies
- smooth → rough
- shallow → deep
- refractions → reflections
- phase → amplitude
- early → late arrivals
- primaries → multiples
- acoustic → elastic
- use variable sub-set of sources each iteration

QC often

**Test with
synthetics**

Workflow

- choose the right problem & acquire the right data
- determine start frequency
- build start model + anisotropy
- check adequacy of model, wavelet & field data
- pre-process & reduce data volume
- modelling & inversion strategy
- run FWI with QA
- check synthetic against field data
- check geometry, wells, image gathers,...
- run RTM on broadband reflection data

Quality Assurance

Quality assurance

- Is start model adequate?
- Is offset adequate?
- FWI result:
 - synthetics match field data
 - match improves
 - geometry matches reflectors
 - flattens gathers
 - matches wells
 - migrates reflections

Cycle skipping in FWI

Cycle skipping is the main limitation on FWI

- drives requirement for low frequencies
- drives requirement for good start model
- limits applicability
- requires rigorous QC & QA
- can lead to (unsuspected) spurious results

Quality assurance

- Given the data that we have, is the starting model good enough?
- Are we converging towards the global minimum?

Common QC tools in FWI

- data residuals decrease
- correlation with field data increases
- time-domain data match
- FWI model and PSDM image correlate
- flat gathers & improved RTM
- model is geologically plausible

All of these can fail to detect cycle skipping

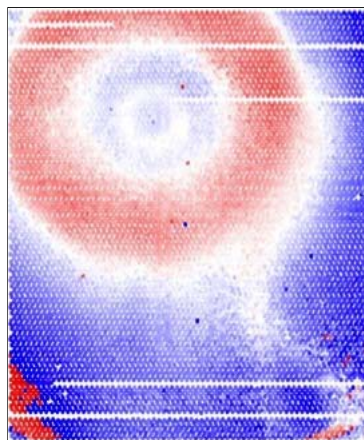
QC for cycle skipping

Generate phase residual plots at starting frequency:

- for start model
- after one iteration
- after final iteration
- for all offsets and azimuths
- for many sources/receivers

Phase residual is the phase difference between observed and predicted data (NOT the phase of the residual)

Phase residual in full-azimuth survey

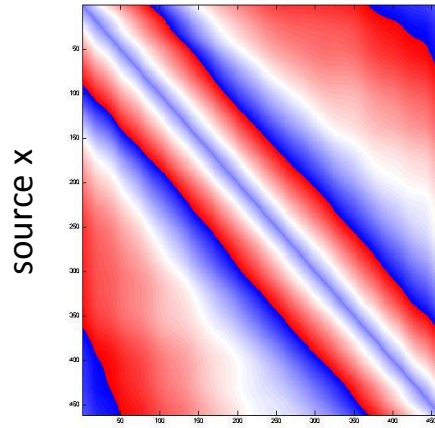


red means
model is
too fast

COMMON RECEIVER GATHER

Phase
-180° 180°

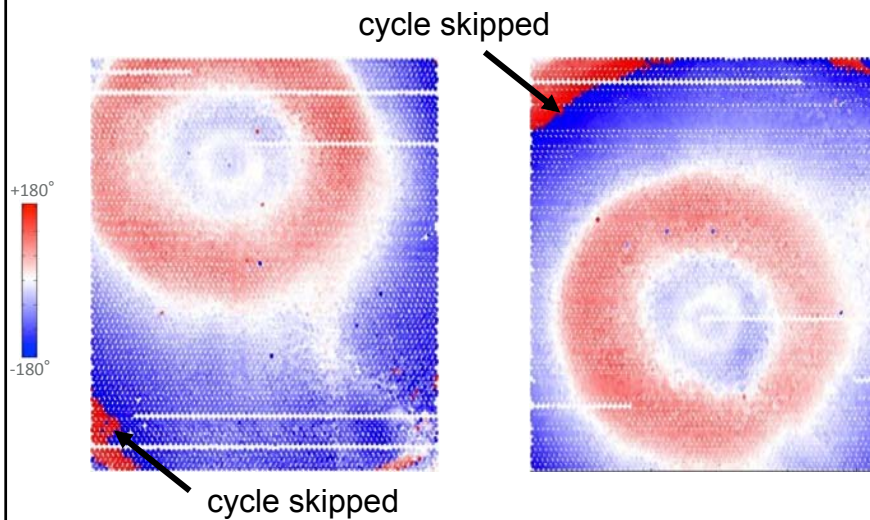
Phase residual in narrow-azimuth survey



*stacking diagram for one cable
and one sail line*

receiver x

3Hz phase residual – shallow water OBC

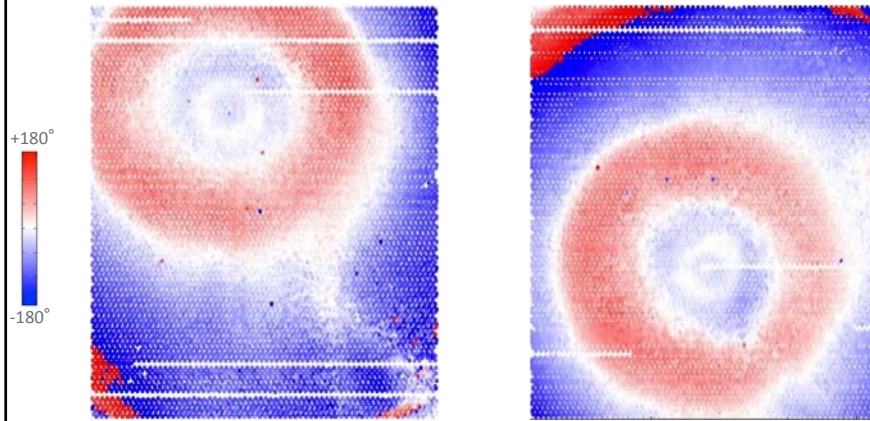


cycle skipped

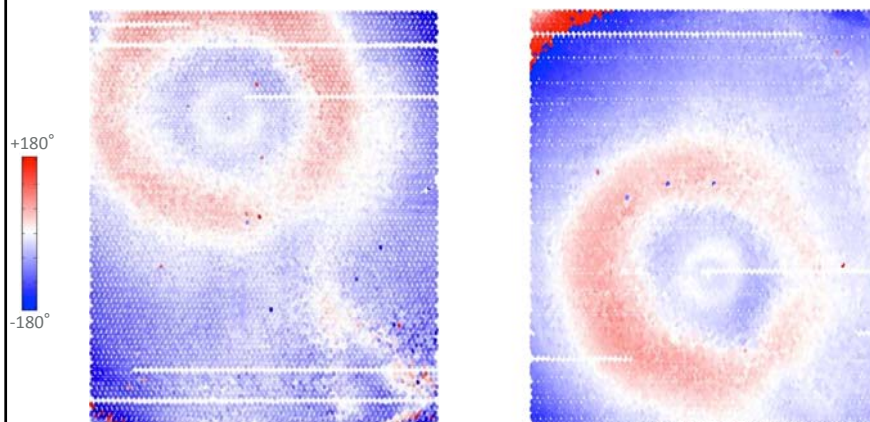
+180°
-180°

cycle skipped

3Hz phase residual – start model

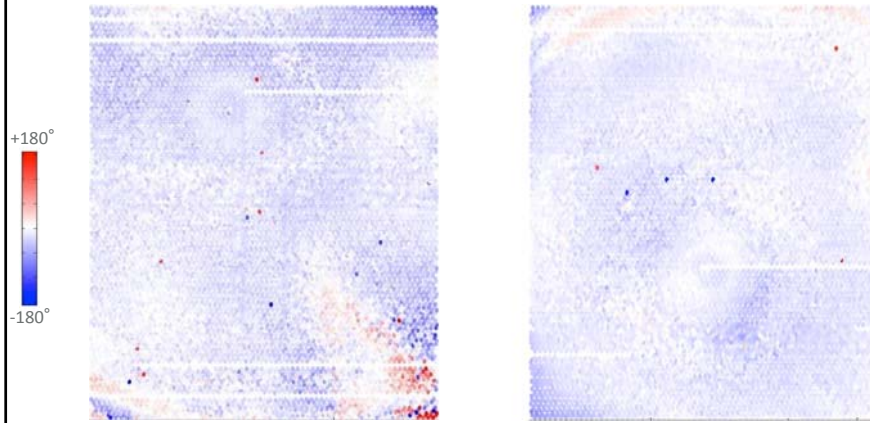


3Hz phase residual – after 1 iteration



CYCLE-SKIPPED REGION **SHRINKS**

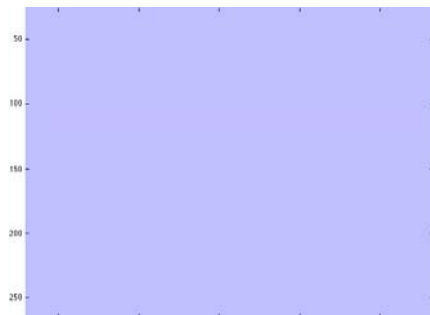
3Hz phase residual – after 18 iterations



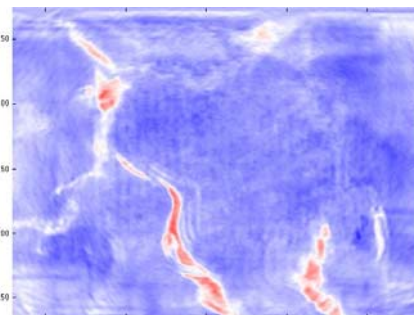
CYCLE-SKIPPED REGION **VANISHED**

FWI result – 250 m

Start



After 108 iterations

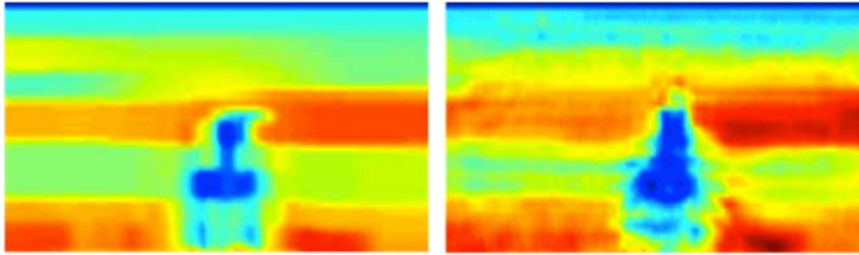



1700  2000

FWI result

Start

After 108 iterations

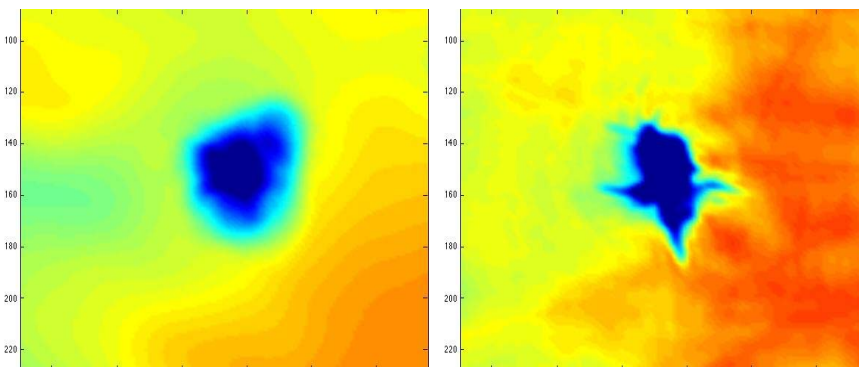


1450  2350

FWI result – 1200 m

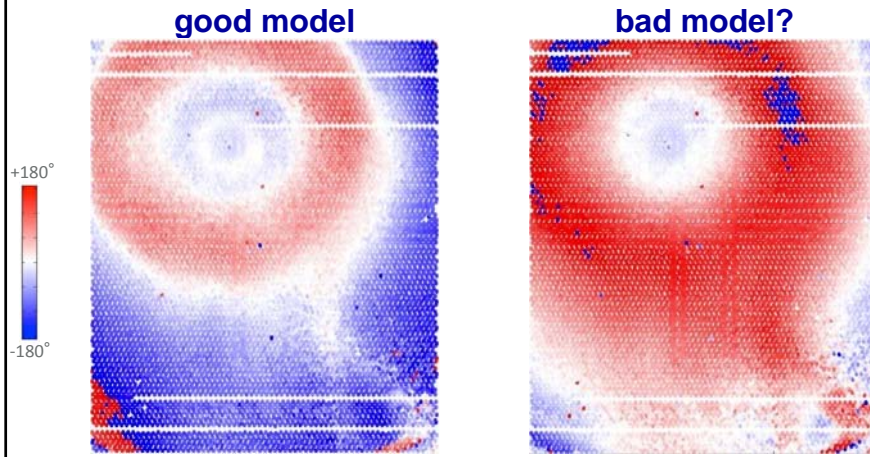
Start

After 108 iterations

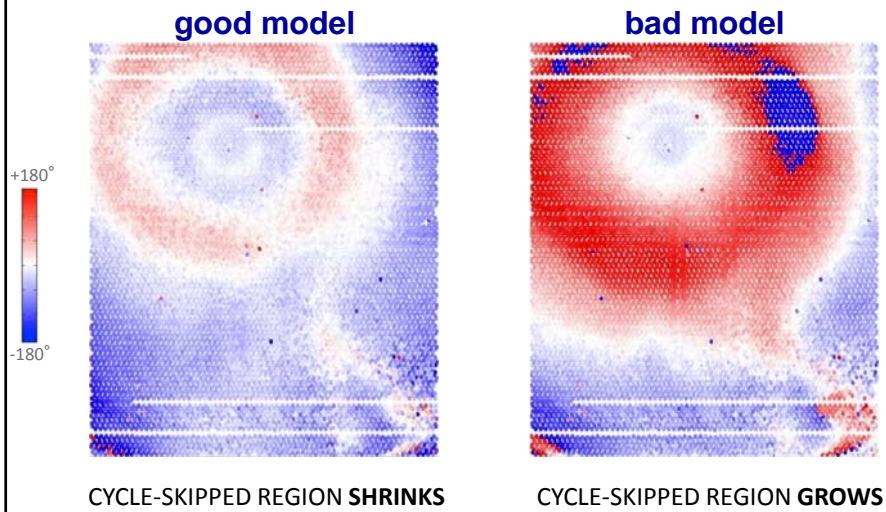


1700  2300

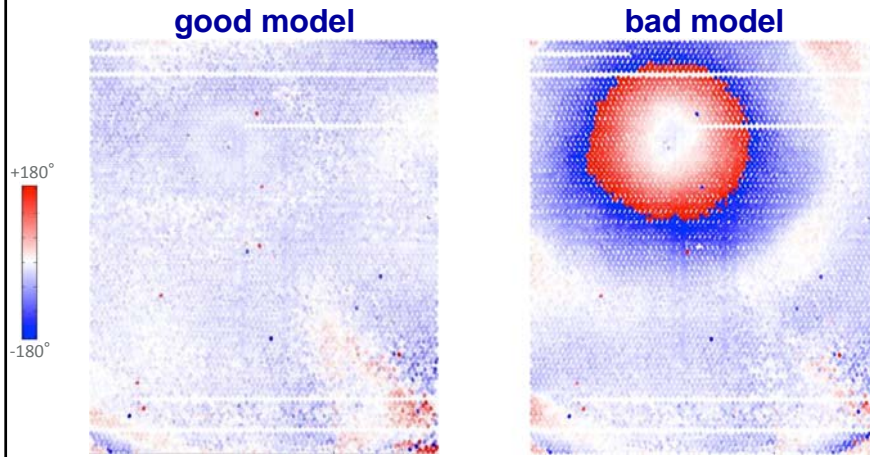
3Hz phase residual



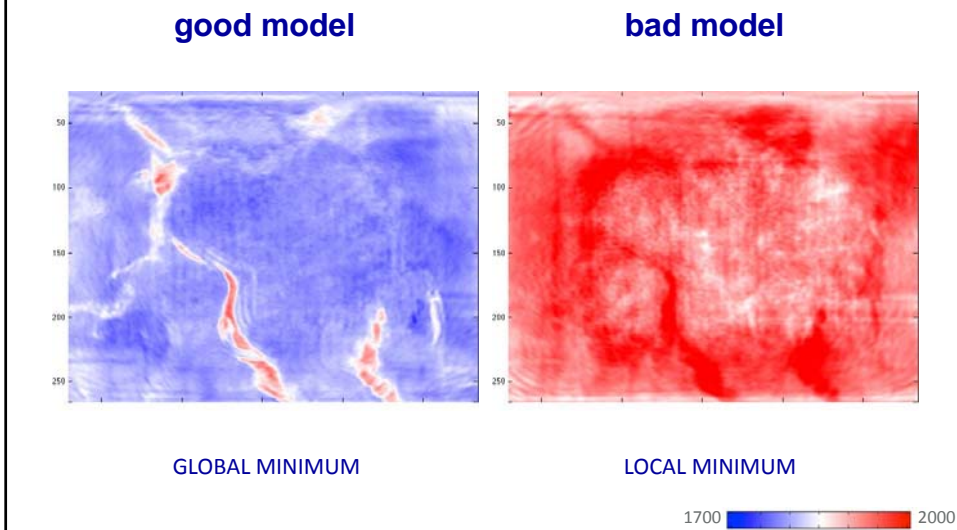
3Hz phase residual - after 1 iteration



3Hz phase residual – after 18 iterations



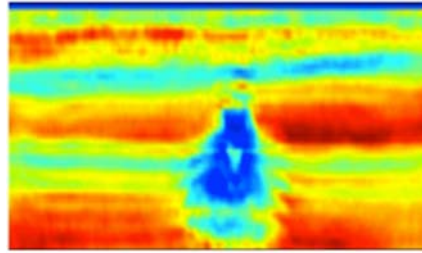
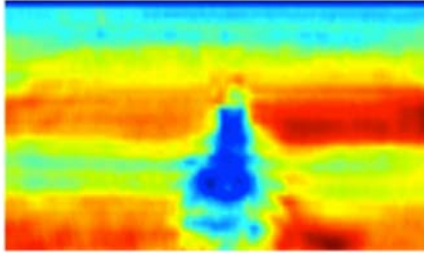
FWI result - after 108 iterations



FWI result - after 108 iterations


good model

bad model



GLOBAL MINIMUM

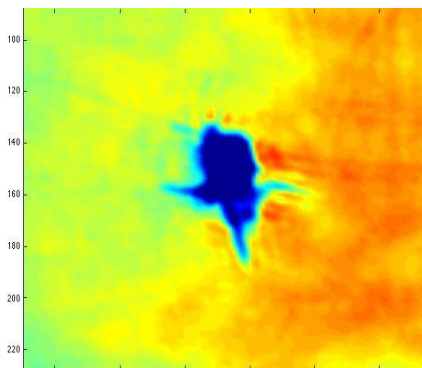
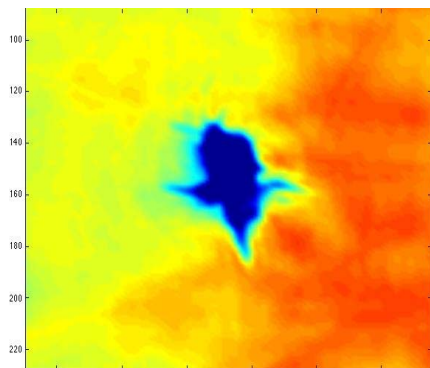
LOCAL MINIMUM

1450  2350

FWI result - after 108 iterations


good model

bad model



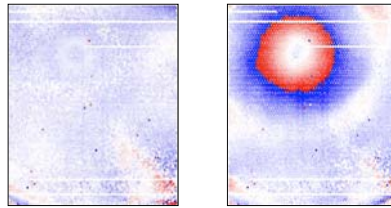
GLOBAL MINIMUM

LOCAL MINIMUM

1700  2300

Conclusion

QA during FWI is essential & easy



Implementation

Implementation

- Efficient wave propagator
 - 3D, heterogeneous, two-way, wave equation
- Appropriate physics
 - acoustic, visco-acoustic, anisotropic, elastic
- Numerical method
 - finite differences, finite elements, spectral elements
- Domain
 - time, frequency, hybrid, Laplace, Fourier-Laplace

Implementation – time domain

- CPU proportional to
 - model size $\sim n^3$
 - number of time steps $\sim n$
 - number of sources $\sim N$
- So CPU $\sim n^4 N$
 - maximise grid spacing
 - maximise time step
 - minimise number of sources
 - minimise local domain

Implementation – time domain

- parallelised on multi-core clusters
- one source per node
- multiple cores per source
- feasible on GPUs

Implementation – resources

- RAM and CPU for explicit-time and iterative-frequency are similar
- TTI anisotropy – RAM & CPU $\times 2$
- Elastic – RAM & CPU $\times 10$ to 1000
(depends upon V_p/V_s)

Implementation – resources

- Run on clusters of multi-core workstations
- Parallelised using Posix threads or OpenMP
- Parallelised using MPI
- Forward modelling on single workstation
- Similar hardware to RTM

Future directions

Future directions

- apply to reservoir
- extend to all acquisition geometries and datasets
- overcome starting model limitations
- more robust & effective FWI
- beyond acoustic
 - elastic, anisotropic, fractures, fluids
- integrate with rock physics & CSEM
- statics → dynamics
- resolution & uncertainty analysis
- modified acquisition
- replace velocity model building, RTM, AVO & DHI

References

Warner et al (2013) *Anisotropic 3D full-waveform inversion*.
Geophysics, **78**, No 2, R59-R80.

Virieux & Operto (2009) *An overview of full-waveform inversion in exploration geophysics*. **Geophysics**, **74**, WCC1-WCC26.

Pratt et al (1998) *Gauss-Newton and full Newton methods in frequency-space seismic waveform inversion*. **Geophysical Journal International**, **133**, 341-362.

Tarantola A (1984) *Inversion of seismic reflection data in the acoustic approximation*. **Geophysics**, **49**, 1259-1266.

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