

Comparison of numerical seismic modeling results with acoustic water-tank data: multi-offset experiment

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ROSE meeting

Outline

- 1 Introduction**
- 2 Multi-offset experiment
- 3 Tip-Wave Superposition Method
- 4 Comparison
- 5 Conclusions

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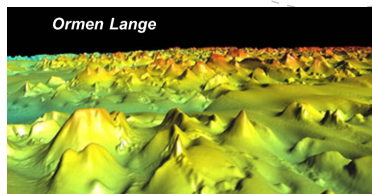
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- 5 **Conclusions**

Motivation

- ▶ 3D seismic modeling is an important tool nowadays
- ▶ Difficulties in simulating 3D wave propagation due to the presence of shadow zones, head waves, diffractions and edge effects
- ▶ How to check the validity of the results?



Benchmarking of numerical modeling methods

- ▶ Against analytical solutions for simple canonical problems.
- ▶ Against other numerical modeling methods (e.g. SEAM project).
- ▶ Via direct comparison with real data acquired in situ.
- ▶ With data obtained in the laboratory under controlled conditions (small-scaled modeling)

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Seismic modeling vs. Ultrasonic laboratory experiment

Main assumption: scaled physical mechanisms are identical to field physical mechanisms ([Ebrom and McDonald, 1994](#))

$$\text{Scale ratio } \mu = 2 \cdot 10^4$$

Table : scale ratio between parameters at seismic scale and laboratory scale

Distance (m)	d_{seis}	=	μd_{lab}
Wavelength (m)	λ_{seis}	=	$\mu \lambda_{lab}$
Time (s)	t_{seis}	=	μt_{lab}
Frequency (Hz)	f_{seis}	=	$\mu^{-1} f_{lab}$
Velocity (m/s)	v_{seis}	=	v_{lab}
Density (kg/m^3)	ρ_{seis}	=	ρ_{lab}
Quality factor (adim.)	Q_{seis}	=	Q_{lab}

The BENCHIE project

Main goal: reveal the strong points and limitations of numerical methods (accuracy and computational cost)

Methods in the project:

- ▶ Tip-Wave Superposition Method
- ▶ Spectral-Element Method
- ▶ Discontinuous Galerkin
- ▶ Born-Integral Method

Link

<http://www.benchie.cnrs-mrs.fr>

Synthetic data vs. Laboratory data

- ▶ Laboratory data for zero- and multi-offset experiments obtained in the Laboratoire de Mécanique et d'Acoustique in Marseille, France
- ▶ Numerical seismic modeling carried out using the Tip-wave Superposition Method (Ayzenberg et al., 2007 Geophysics 72)

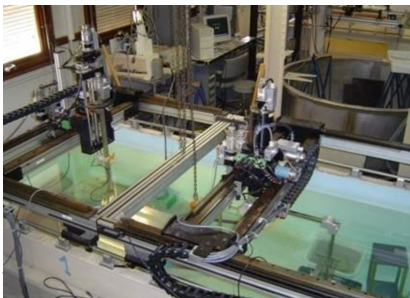


Figure : Zero-offset acquisition

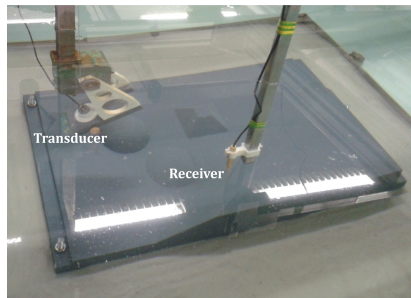


Figure : Multi-offset acquisition

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Marseille model

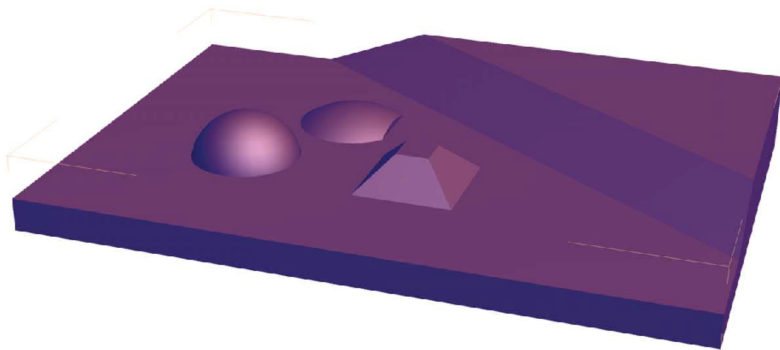
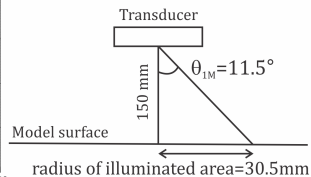
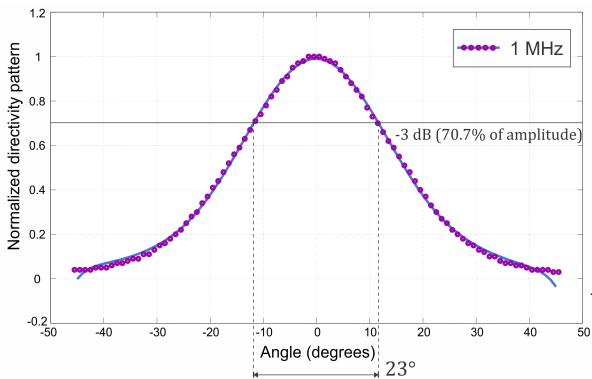


Figure : Based on the French model ([French, 1974](#))

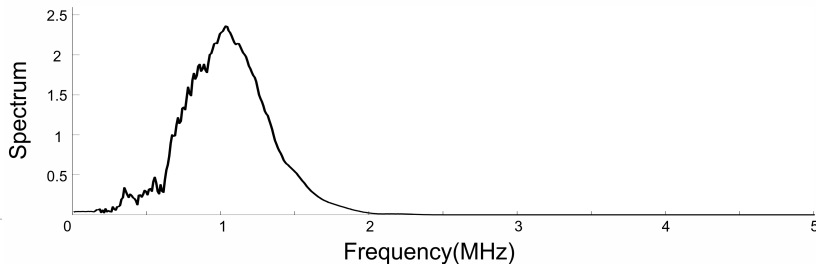
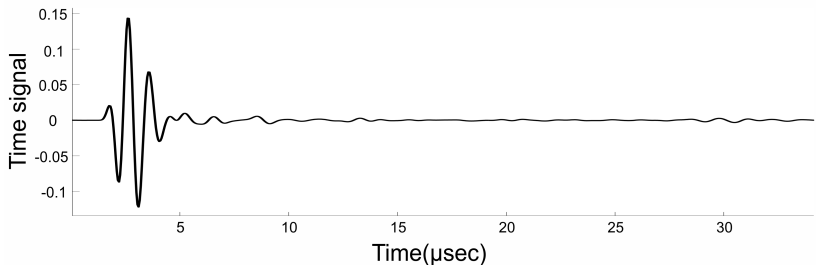
Material properties

	V_p	V_s	ρ	Q_p	Q_s
Water	1476-1493 m/s	-	1000 kg/m ³	-	-
PVC	2220 m/s	1050 m/s	1412 kg/m ³	40-60	27-31
Sand	1660-1675 m/s	50 m/s	2004 kg/m ³	120	-
Aluminum	6440 m/s	3170 m/s	2700 kg/m ³	-	-

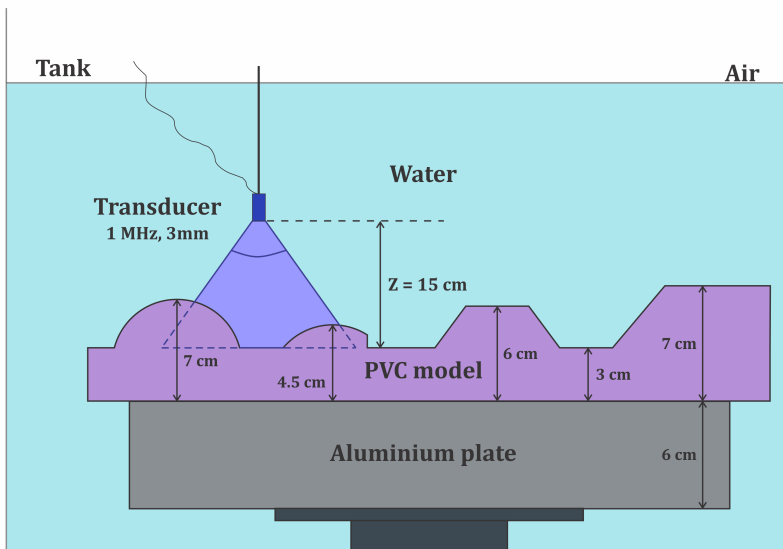
Directivity pattern



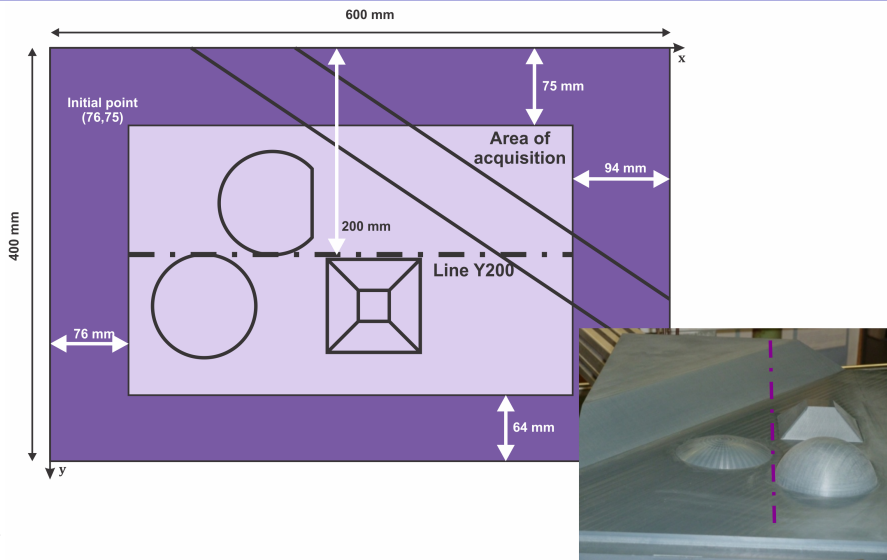
Broad-beam transducer (1 MHz, $\varnothing = 3$ mm)



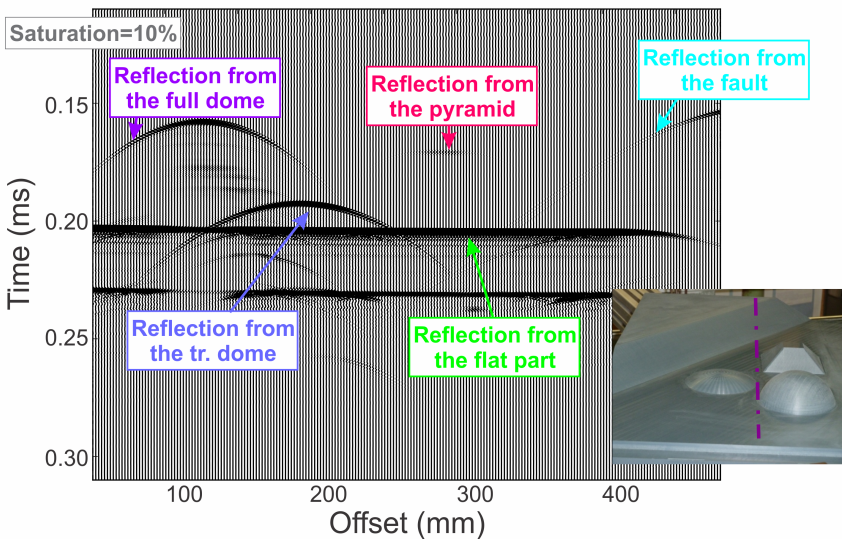
Zero-offset experimental set-up



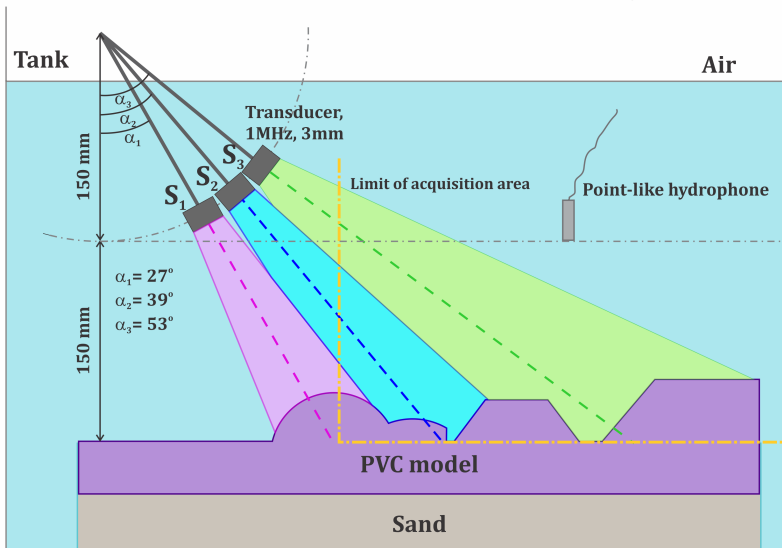
Zero-offset acquisition



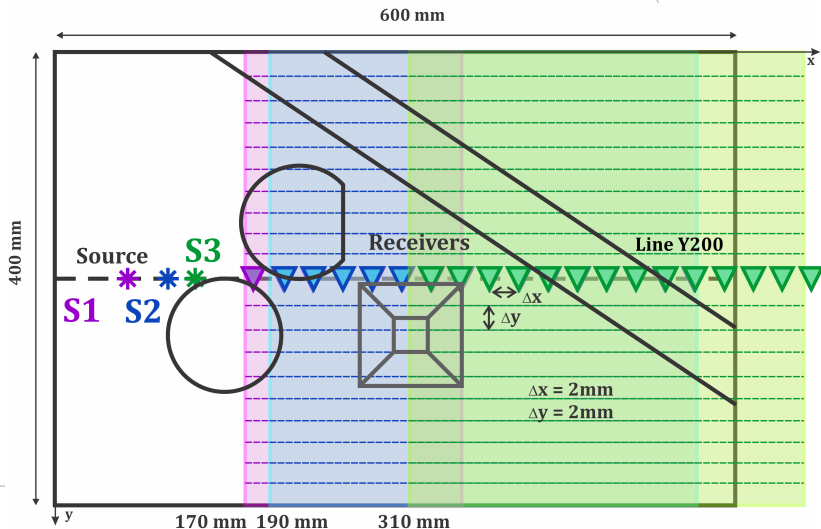
Laboratory data, zero-offset



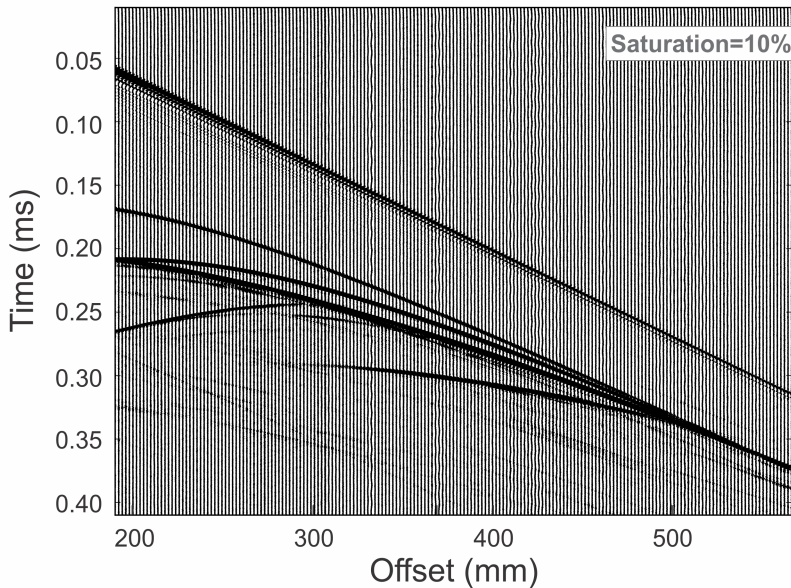
Multi-offset experimental set-up



Multi-offset acquisition



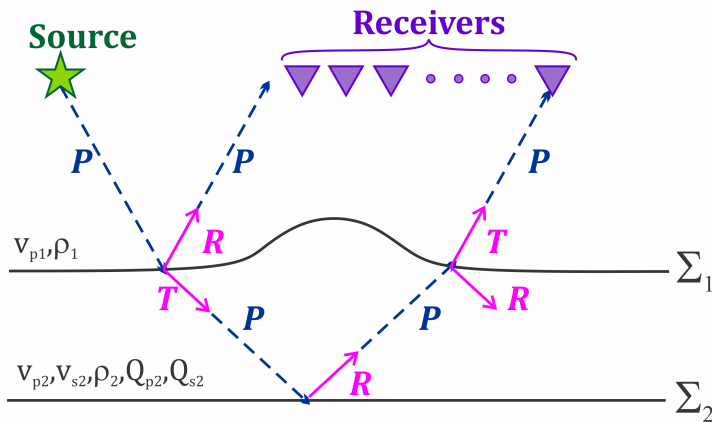
Laboratory data, multi-offset



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Tip-wave Superposition Method



Tip-Wave Superposition Method

The surface integral propagator **P**

$$\mathbf{P}(\mathbf{x}; \mathbf{s}) \langle \dots \rangle = \frac{1}{4\pi} \iint_{\Sigma} \left[\frac{\partial G(\mathbf{x}; \mathbf{s})}{\partial \mathbf{n}(\mathbf{s})} \langle \dots \rangle - G(\mathbf{x}; \mathbf{s}) \frac{\partial}{\partial \mathbf{n}(\mathbf{s})} \langle \dots \rangle \right] d\Sigma(\mathbf{s}) \quad (1)$$

The reflection and transmission operators **R** and **T**

$$\mathbf{R}(\mathbf{s}, \mathbf{s}') = \tilde{\mathfrak{F}}^{-1}(\mathbf{s}, \mathbf{q}) \hat{\mathbf{R}}(\mathbf{q}) \tilde{\mathfrak{F}}(\mathbf{q}, \mathbf{s}') \quad (2)$$

and

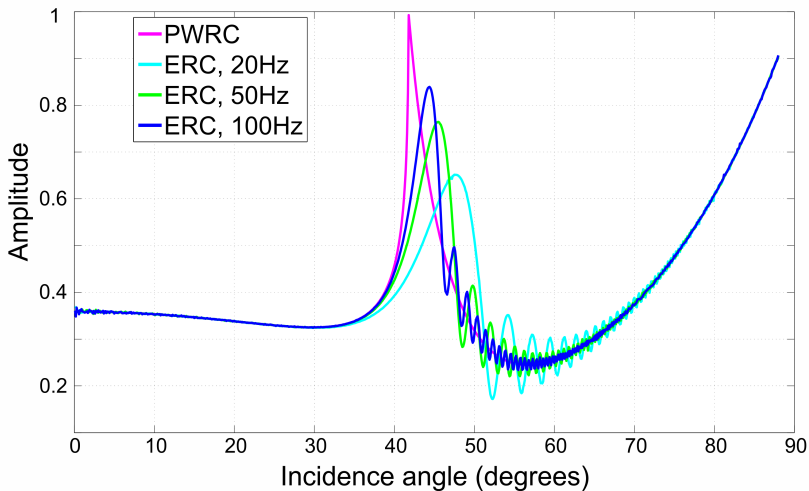
$$\mathbf{T}(\mathbf{s}, \mathbf{s}') = \tilde{\mathfrak{F}}^{-1}(\mathbf{s}, \mathbf{q}) \hat{\mathbf{T}}(\mathbf{q}) \tilde{\mathfrak{F}}(\mathbf{q}, \mathbf{s}') \quad (3)$$

- ▶ Interface split into small elements, propagation operator approximated by propagation matrix.
- ▶ Reflection operator approximated by effective or plane-wave reflection/transmission coefficients.

Tip-Wave Superposition Method

- ▶ Plane-wave reflection coefficient (PWRC) \implies conventional Kirchhoff modeling
 - ◊ Fast and accurate
 - ◊ Artificial diffractions
- ▶ Effective reflection coefficients (ERC)
 - ◊ Slower, but high accuracy
 - ◊ Seismic frequency range
 - ◊ Head waves
- ▶ Effective coefficients on dominant frequency (DRC)
 - ◊ Trade-off between speed and quality
 - ◊ No artificial diffractions
 - ◊ No head waves

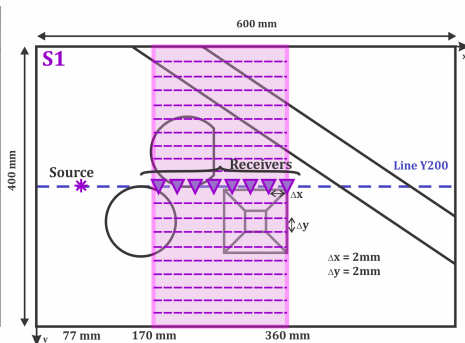
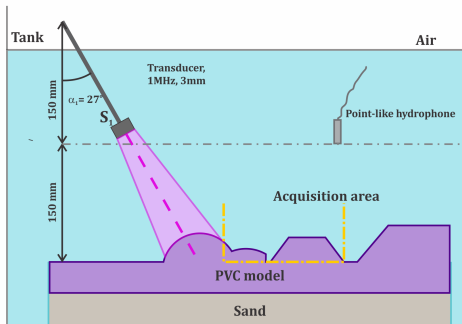
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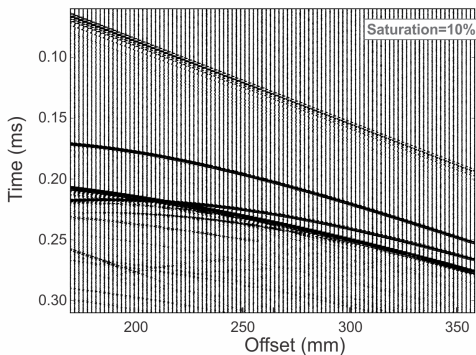
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Multi-offset experiment, S1

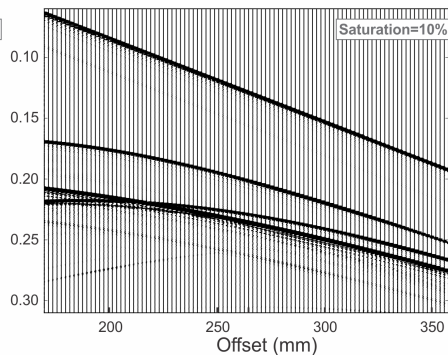


Comparison of laboratory and synthetic data, S1

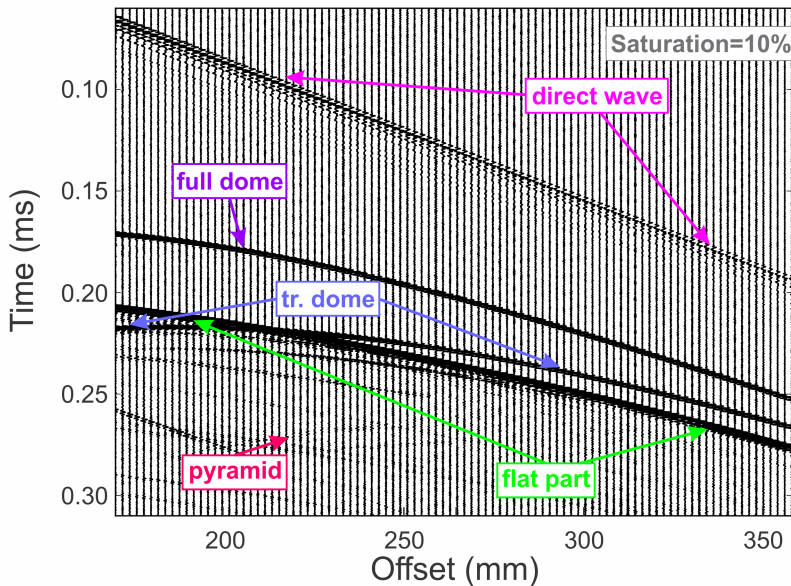
Laboratory data



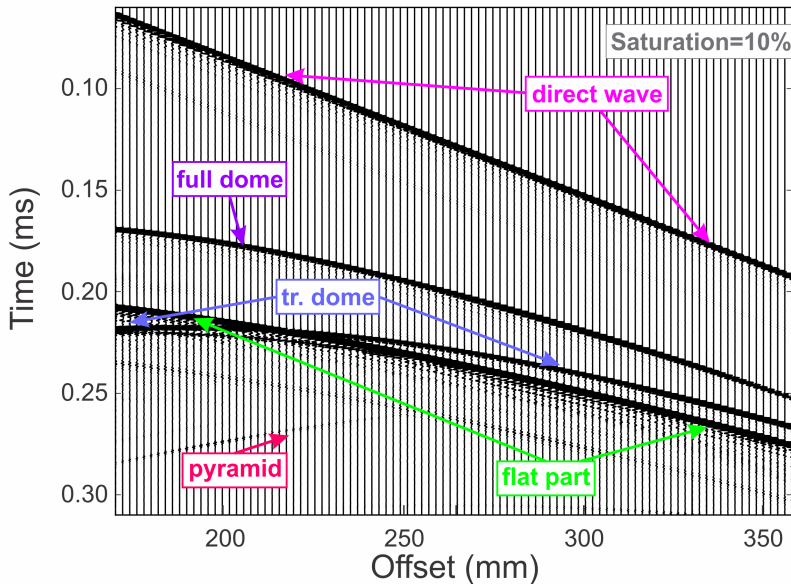
Synthetic data



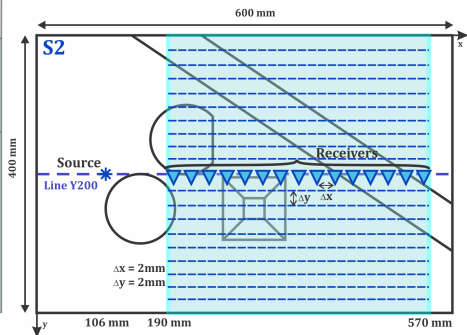
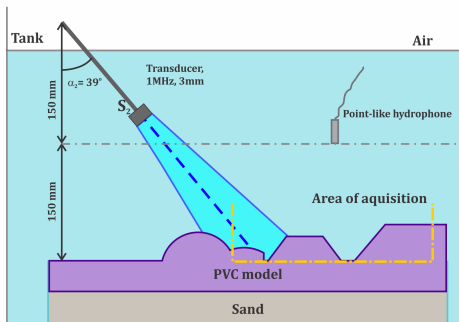
Laboratory data, S1



Synthetic data, S1

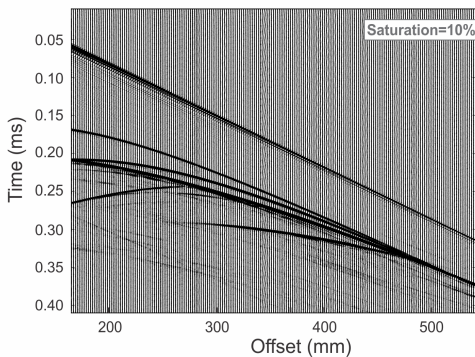


Multi-offset experiment, S2

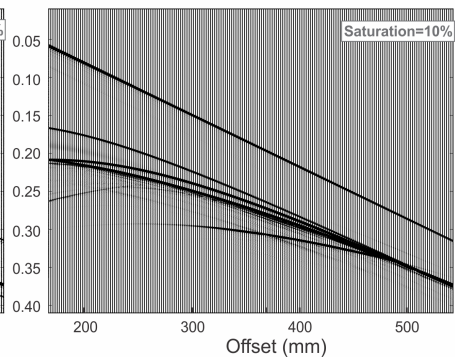


Comparison of laboratory and synthetic data, S2

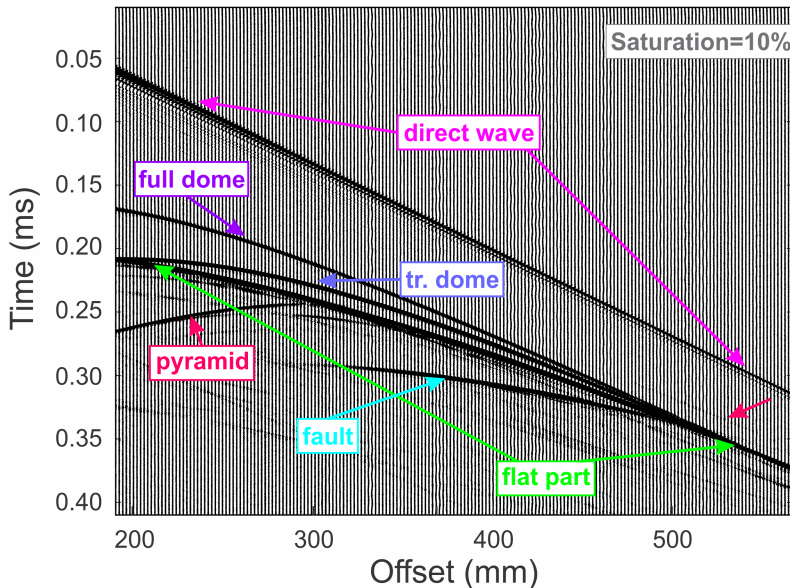
Laboratory data



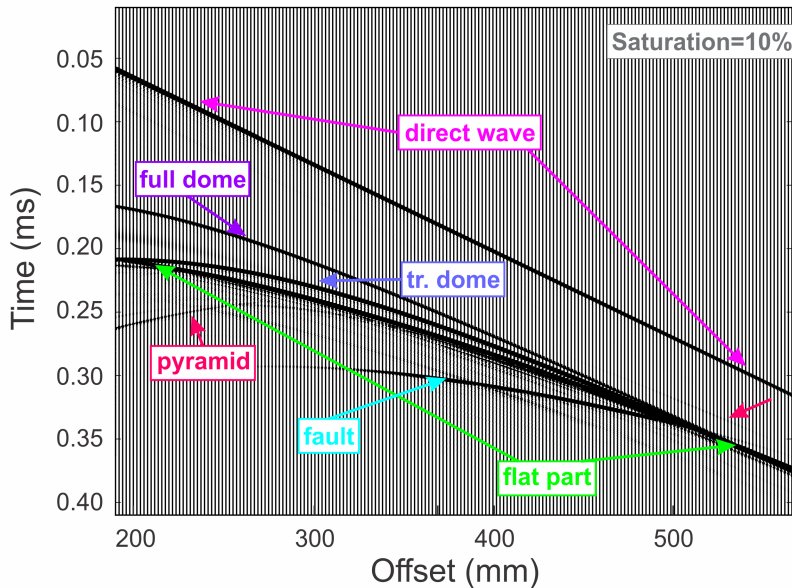
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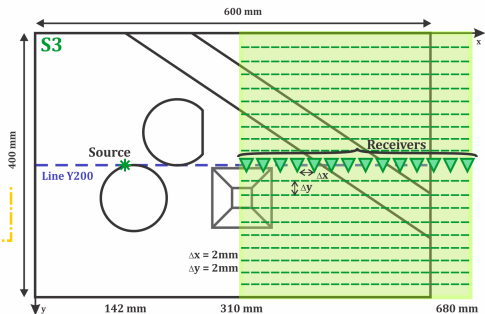
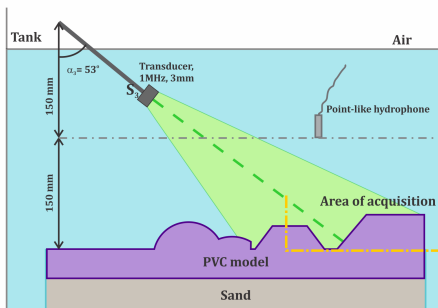
Laboratory data, S2



Synthetic data, S2

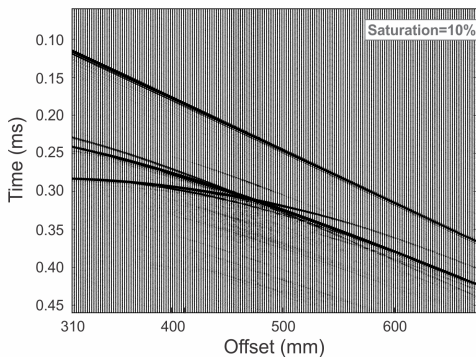


Multi-offset experiment, S3

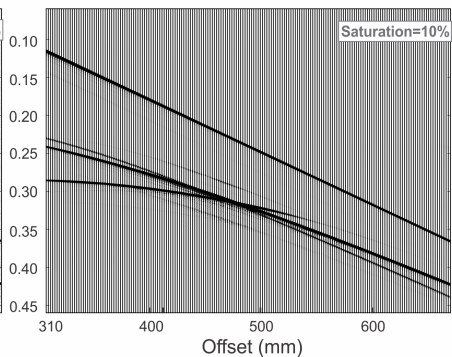


Comparison of laboratory and synthetic data, S3

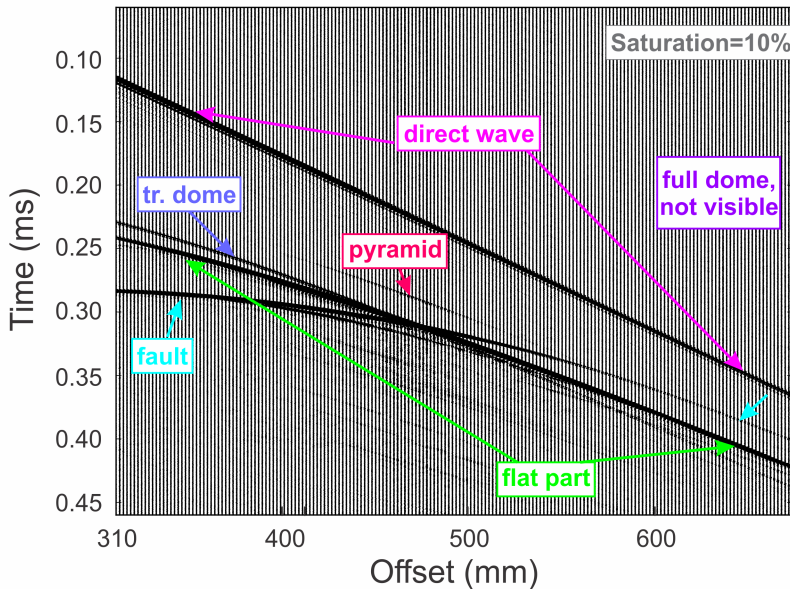
Laboratory data



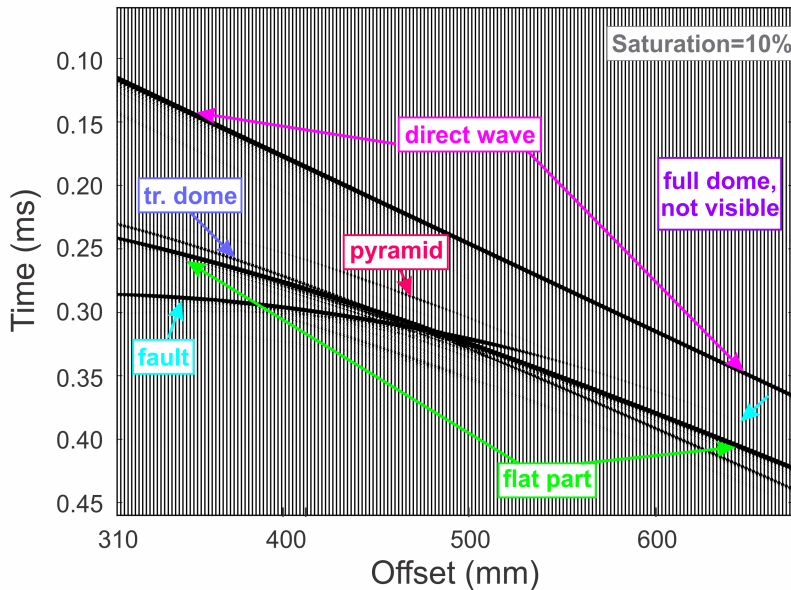
Synthetic data



Laboratory data, S3



Synthetic data, S3



Conclusions

- ▶ **Multi-offset seismic experiments using sources with unfocused beam and 2D array receivers covering the entire model.**
- ▶ Comparisons indicate a good qualitative fit in time arrivals and amplitudes.
- ▶ Synthetic modeling helps in interpretation of the obtained laboratory data.
- ▶ More detailed study of the experiment conditions needed to perform quantitative evaluation of the results.

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Acknowledgements

- ▶ Stephan Devic (LMA Marseille) for his valuable contribution to the conception of the Marseille model
- ▶ For financial support

