

Effect of anelastic sands layers on R/T responses of a periodically layered medium

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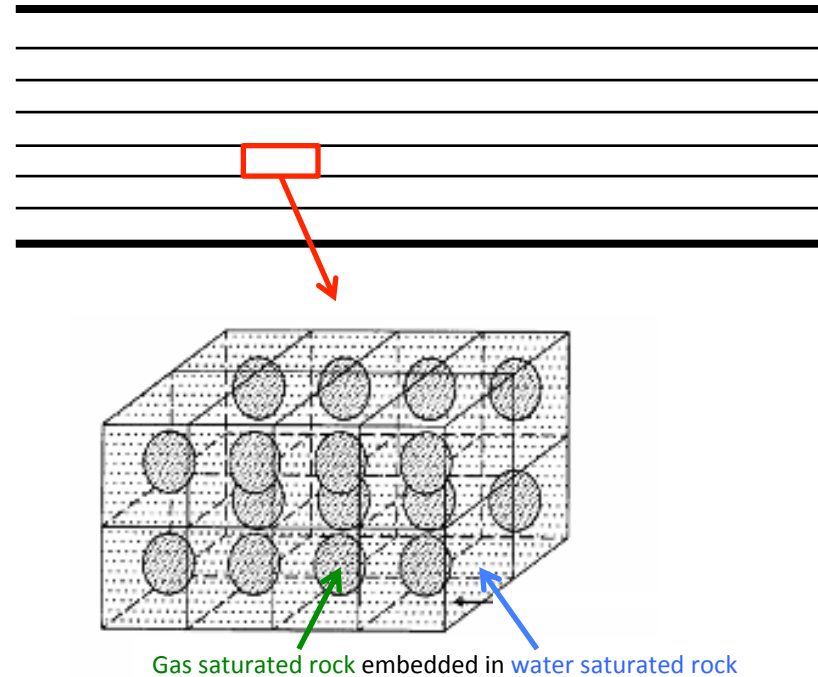
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Idea

- Paper of Alexey Stovas and Bjørn Ursin on: *Equivalent time-average and effective medium for periodic layers*, **Geophysical Prospecting**, 2007
- ➔ The reflection and transmission (R/T) responses from a layered periodic medium are frequency-dependent. This dispersion and attenuation of the effective medium is controlled by the layering and the medium parameters.
- What could happen if we mix the frequency dependence due to the layering with the one coming from patchy saturated porous media ?

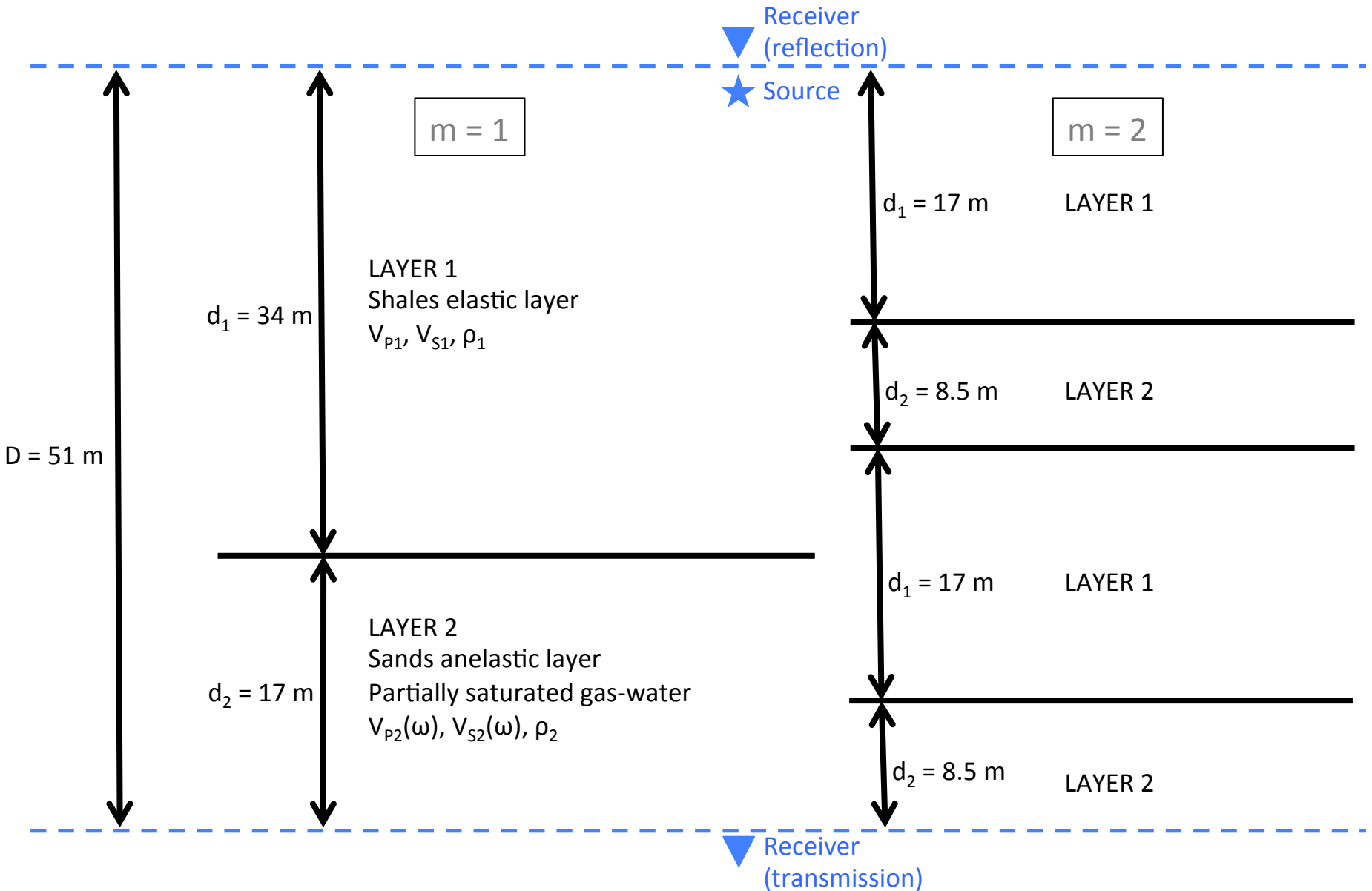
Two scales of periodicity

- Layering → macroscale (wavelength)
- Patchy saturation → mesoscale (gas inclusions)



→ Both can affect wave propagation (dispersion, attenuation...) at seismic frequencies (1 to 1000 Hz)

Layout



Model

Layers 1 = shales

$$V_p = 2550 \text{ m/s}$$

$$V_s = 1450 \text{ m/s}$$

$$\rho = 2300 \text{ kg/m}^3$$

Elastic

Layers 2 = partially saturated sandstones

Gas saturation = 10 %

Patchy saturation: ANELASTIC

OR

Equivalent medium: ELASTIC

3 porosity models (= 3 levels of dispersion)

$$\phi = 32 \%$$

$$V_p = 2211 \text{ m/s}$$

$$V_s = 1227 \text{ m/s}$$

$$\rho = 2144 \text{ kg/m}^3$$

$$\phi = 40 \%$$

$$V_p = 2256 \text{ m/s}$$

$$V_s = 1282 \text{ m/s}$$

$$\rho = 2007 \text{ kg/m}^3$$

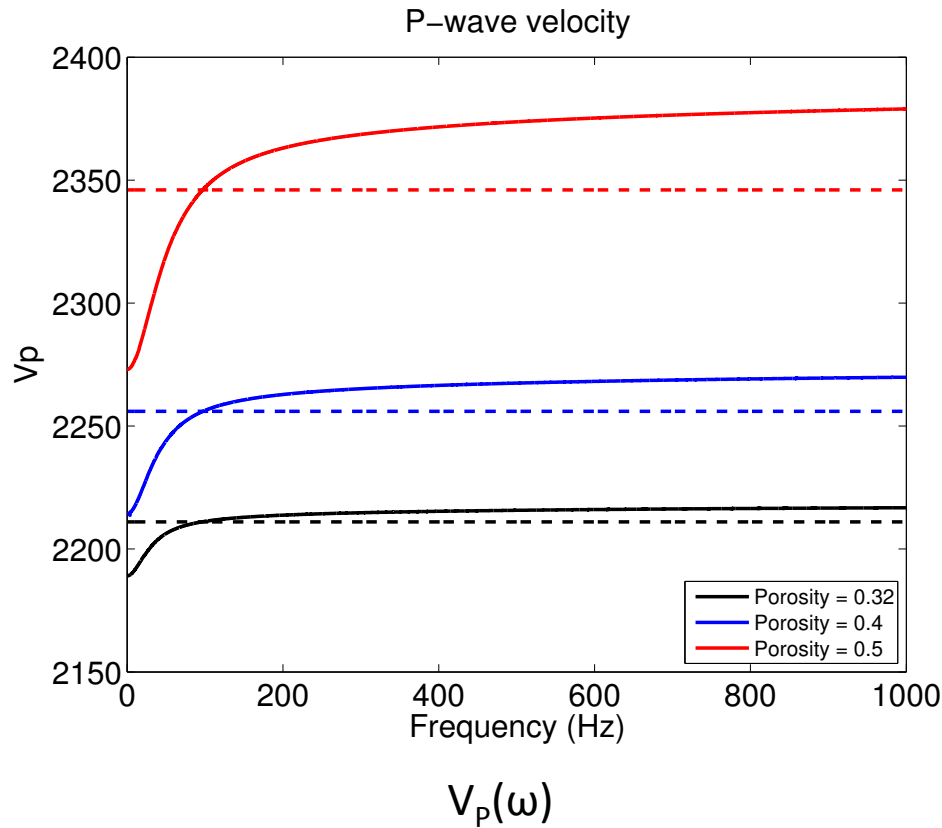
$$\phi = 50 \%$$

$$V_p = 2346 \text{ m/s}$$

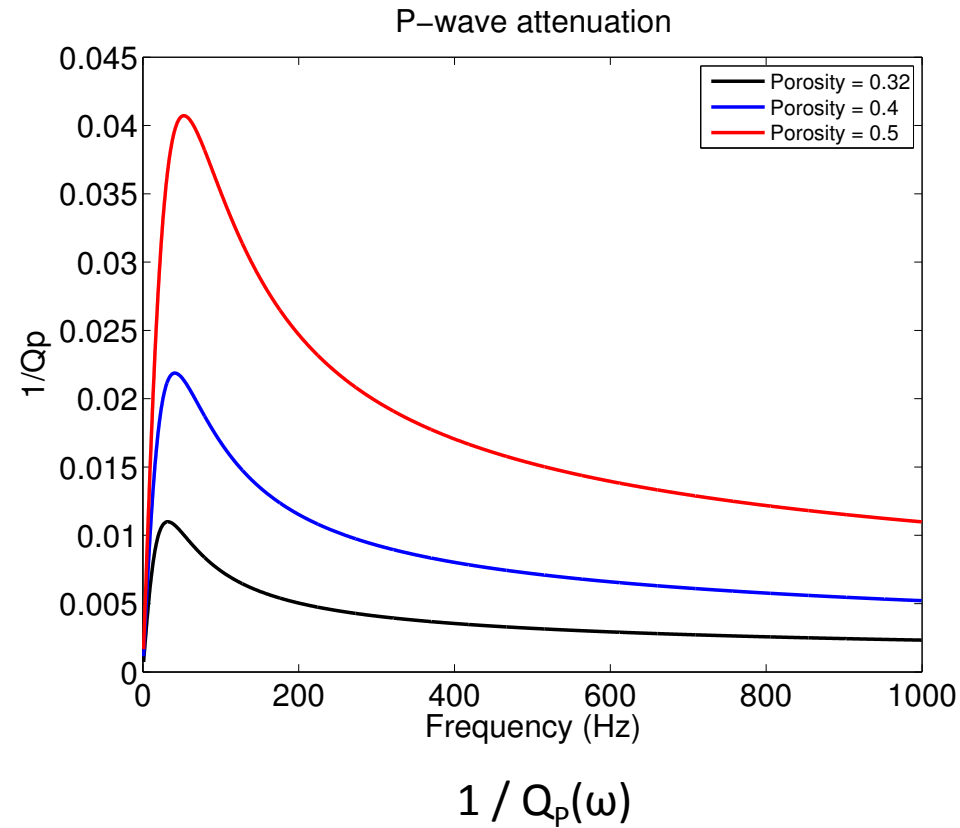
$$V_s = 1358 \text{ m/s}$$

$$\rho = 1837 \text{ kg/m}^3$$

P-wave dispersion and attenuation



V_p dispersion between 1.5 % and 5 %



Q_p max between 25 and 100

Computation of R/T responses

Propagator matrix for 1 cycle (2 layers):

$$\mathbf{S}_k(\omega) = \frac{1}{1-r^2(\omega)} \begin{pmatrix} e^{i\theta_1} & 0 \\ 0 & e^{-i\theta_1} \end{pmatrix} \begin{pmatrix} 1 & r(\omega) \\ r(\omega) & 1 \end{pmatrix} \begin{pmatrix} e^{i\theta_2(\omega)} & 0 \\ 0 & e^{-i\theta_2(\omega)} \end{pmatrix} \begin{pmatrix} 1 & -r(\omega) \\ -r(\omega) & 1 \end{pmatrix}$$

$r(\omega)$ = reflection coefficient

t_1 and $t_2(\omega)$ = traveltimes

θ_1 and $\theta_2(\omega)$ = phase factors

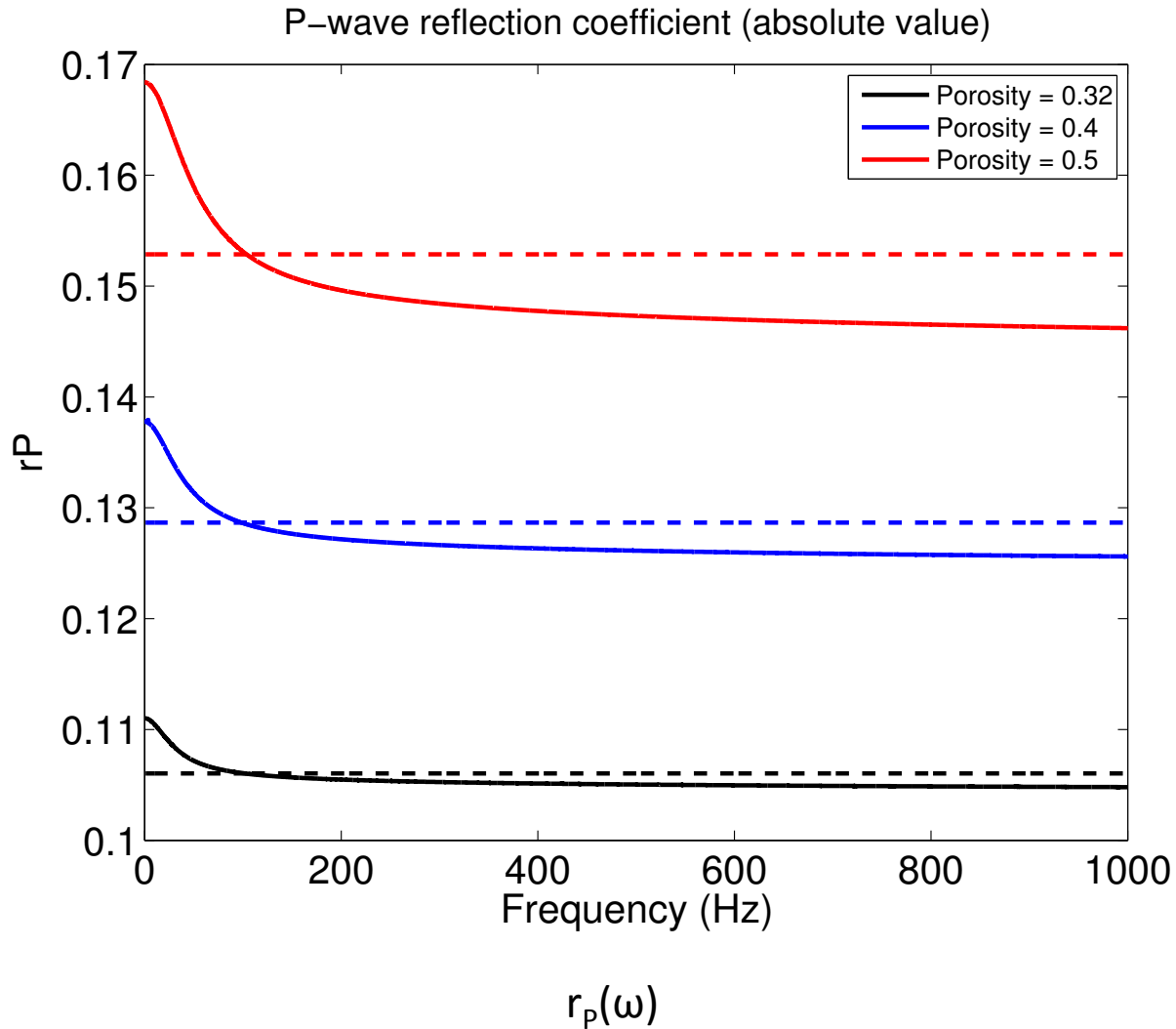
$$r(\omega) = \frac{\rho_2 V_2(\omega) - \rho_1 V_1}{\rho_2 V_2(\omega) + \rho_1 V_1} ,$$

$$\theta_1 = \frac{2\pi f d_1}{V_1} = 2\pi f t_1 ,$$

$$\theta_2(\omega) = \frac{2\pi f d_2}{V_2(\omega)} = 2\pi f t_2(\omega) ,$$

Equations valid for P- or S-waves independently

Reflection coefficients



Computation of R/T responses

Propagator matrix for 1 cycle (2 layers):

$$\mathbf{S}_k(\omega) = \frac{1}{1-r^2(\omega)} \begin{pmatrix} e^{i\theta_1} & 0 \\ 0 & e^{-i\theta_1} \end{pmatrix} \begin{pmatrix} 1 & r(\omega) \\ r(\omega) & 1 \end{pmatrix} \begin{pmatrix} e^{i\theta_2(\omega)} & 0 \\ 0 & e^{-i\theta_2(\omega)} \end{pmatrix} \begin{pmatrix} 1 & -r(\omega) \\ -r(\omega) & 1 \end{pmatrix}$$

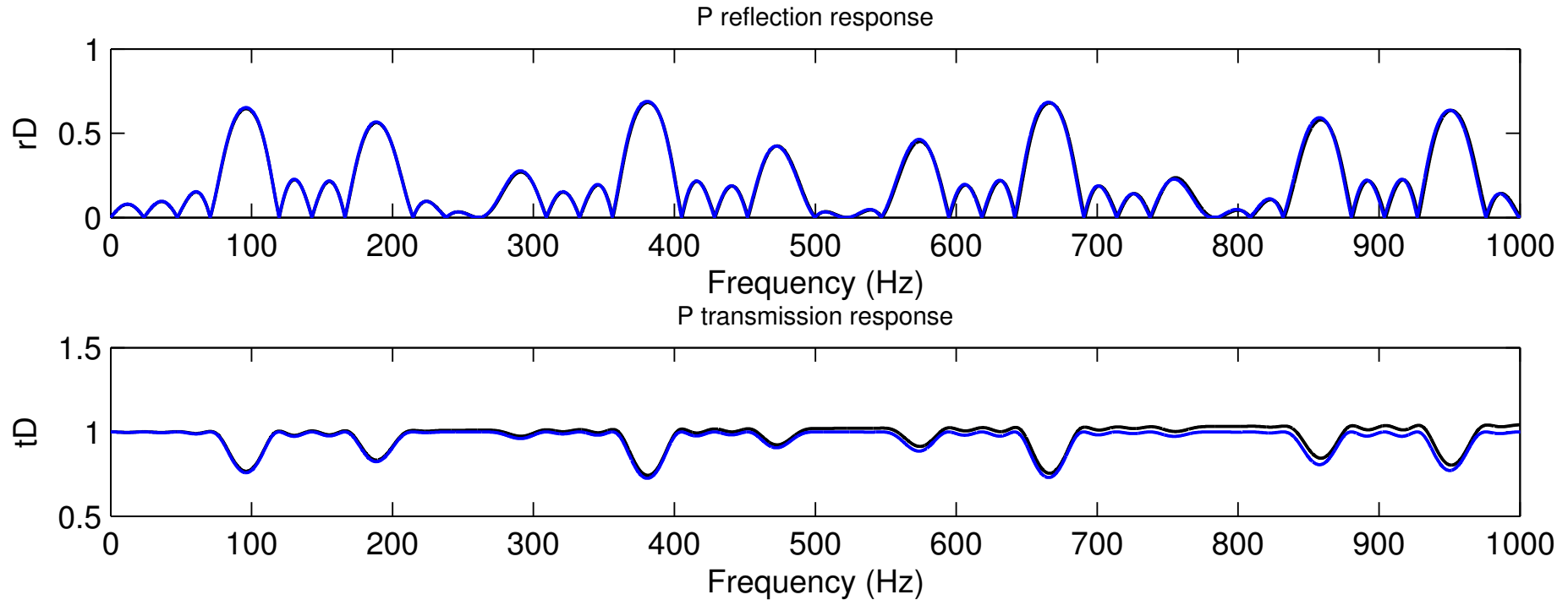
Total response for m cycles:

$$\mathbf{S}_m(\omega) = \prod_{k=1}^m \mathbf{S}_k = \begin{pmatrix} a_m(\omega) & b_m(\omega) \\ c_m(\omega) & d_m(\omega) \end{pmatrix}$$

Transmission $t_D(\omega)$ and reflection $r_D(\omega)$ responses for a downgoing wave:

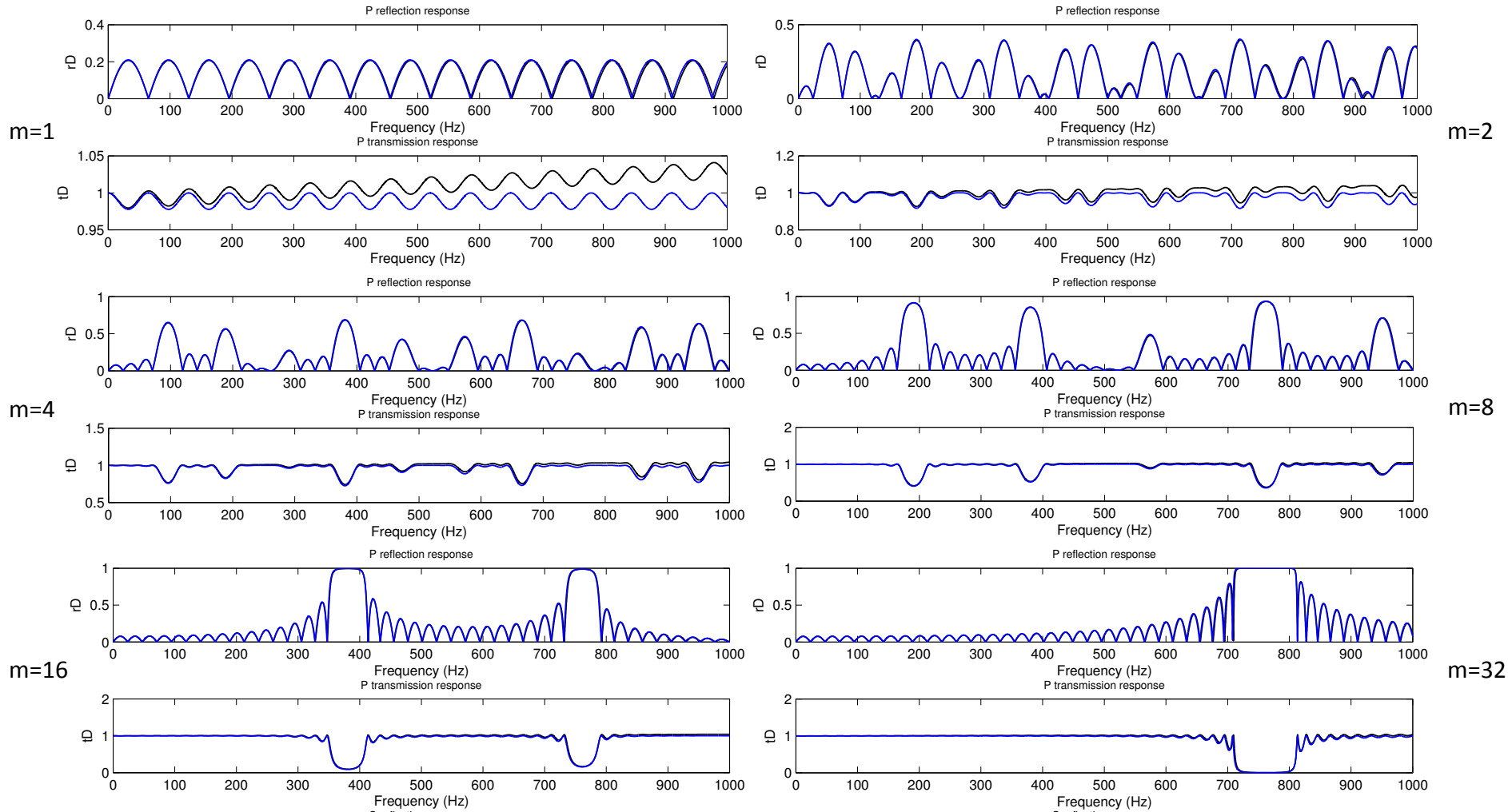
$$t_D(\omega) = \frac{1}{d_m(\omega)},$$
$$r_D(\omega) = \frac{b_m(\omega)}{d_m(\omega)}.$$

R/T responses for $m=4$ and $\phi=32\%$



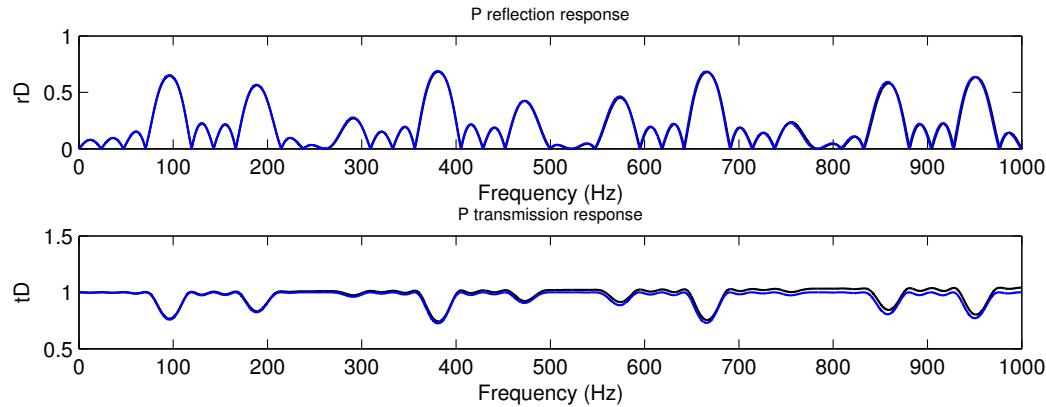
- Anelastic sand layers
- Elastic sand layers (no dispersion)

R/T responses ($\phi=32\%$)

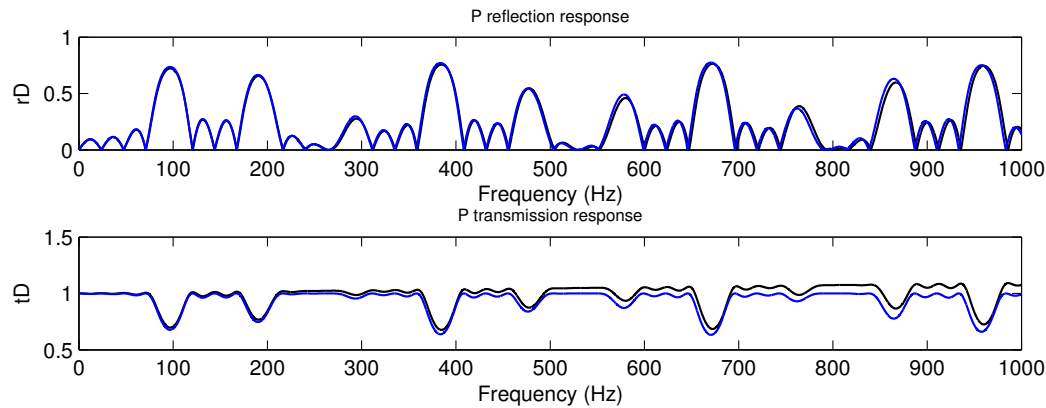


R/T responses (m=4)

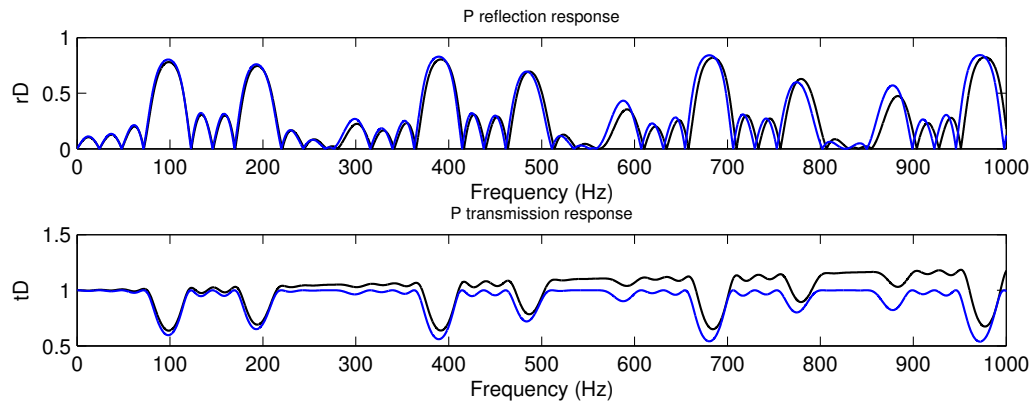
$\phi=32\%$



$\phi=40\%$

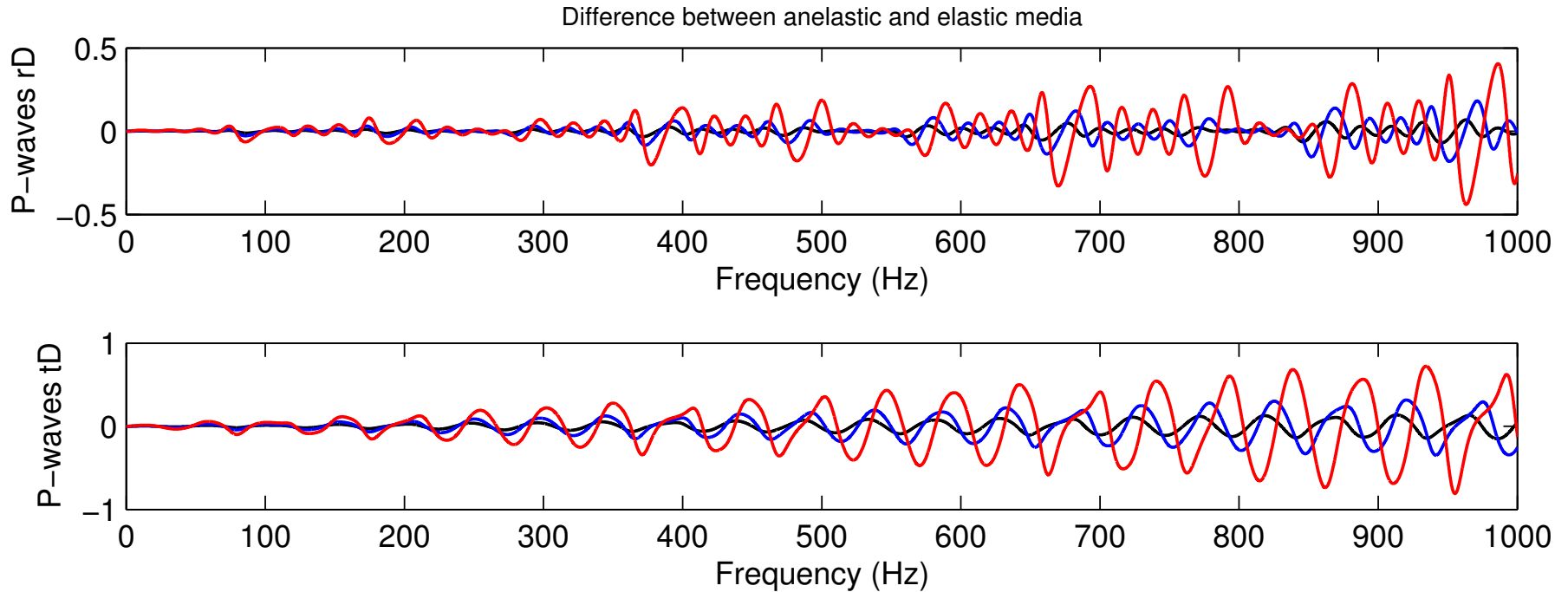


$\phi=50\%$



— Anelastic sand layers
— Elastic sand layers (no dispersion)

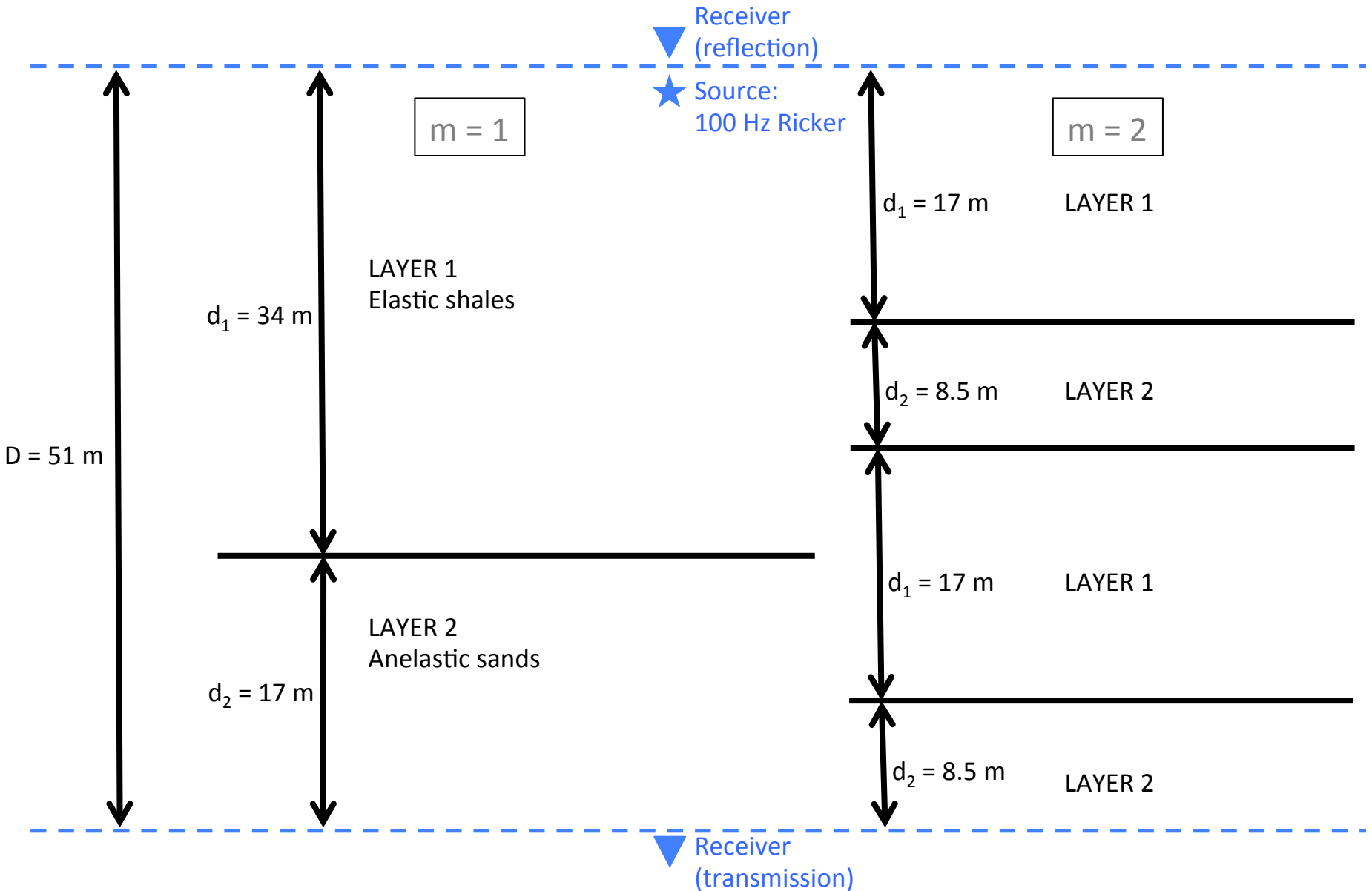
R/T responses differences (m=4)



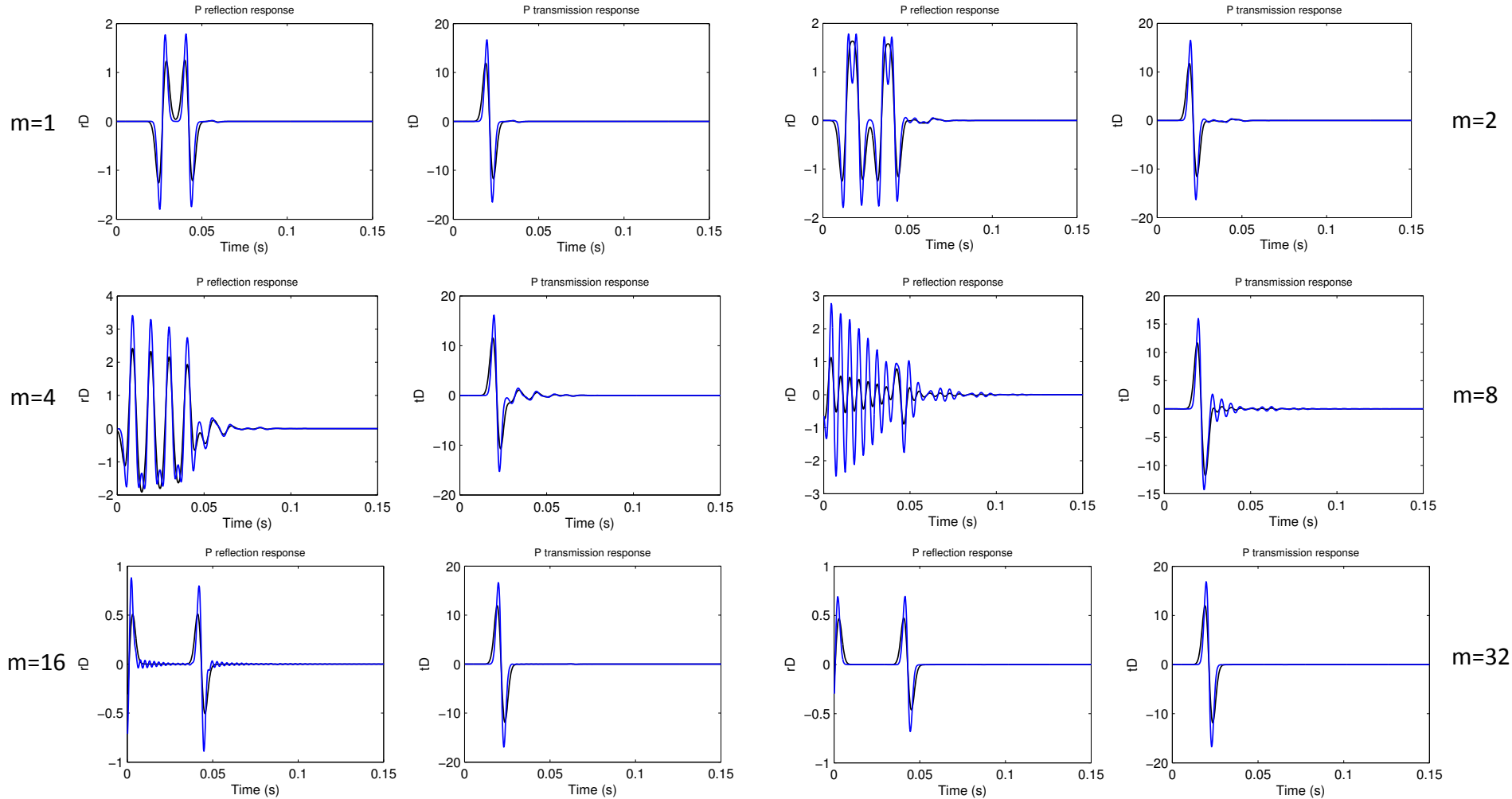
Difference between anelastic and equivalent elastic layers for:

- $\phi = 32\%$
- $\phi = 40\%$
- $\phi = 50\%$

Time domain responses

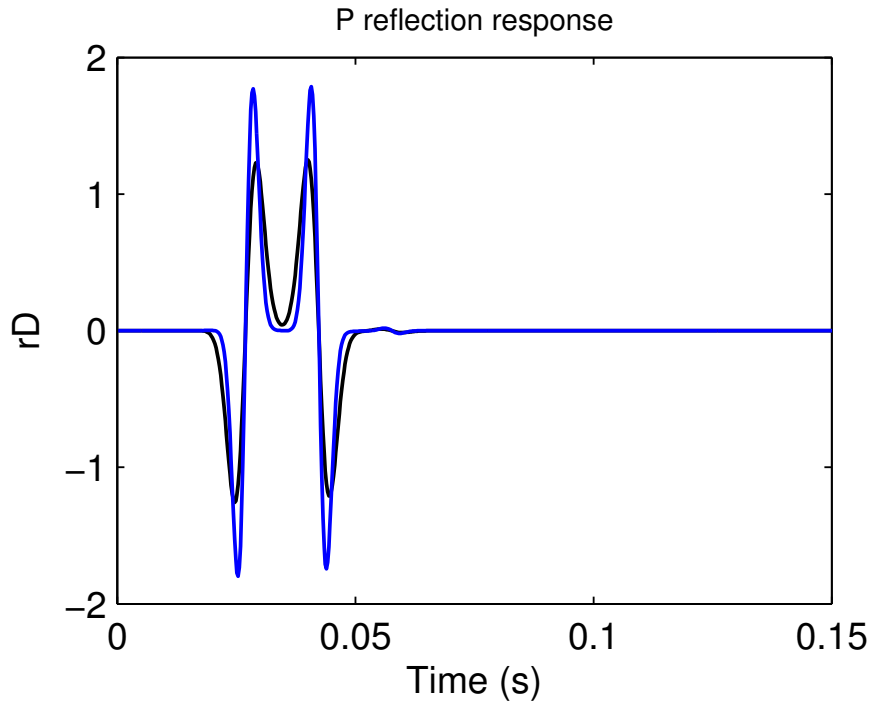


R/T time responses ($\phi=32\%$)

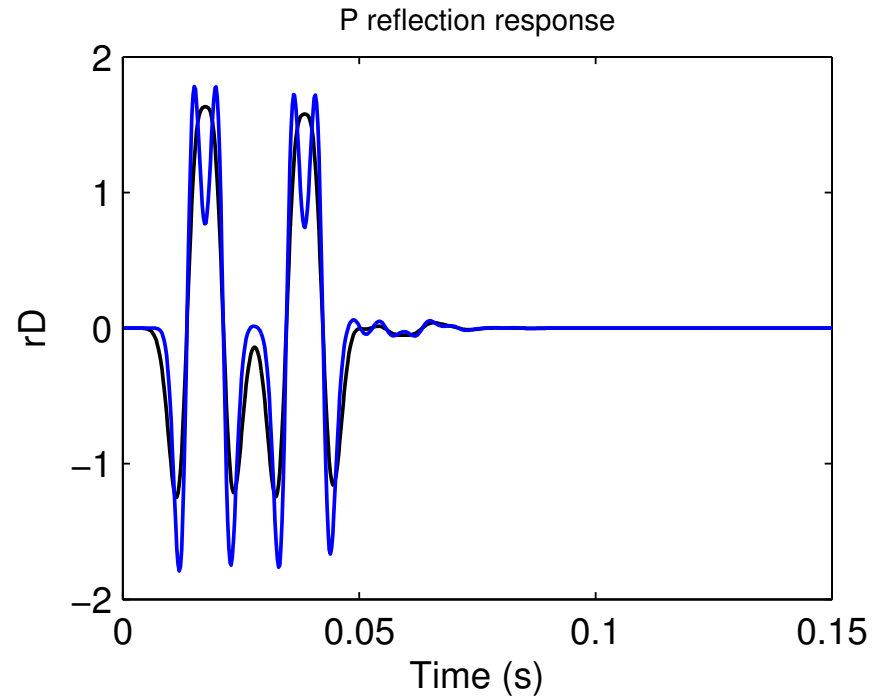


— Anelastic sand layers
— Elastic sand layers (no dispersion)

R/T time responses ($\phi=32\%$): reflected events for $m=1$ and $m=2$



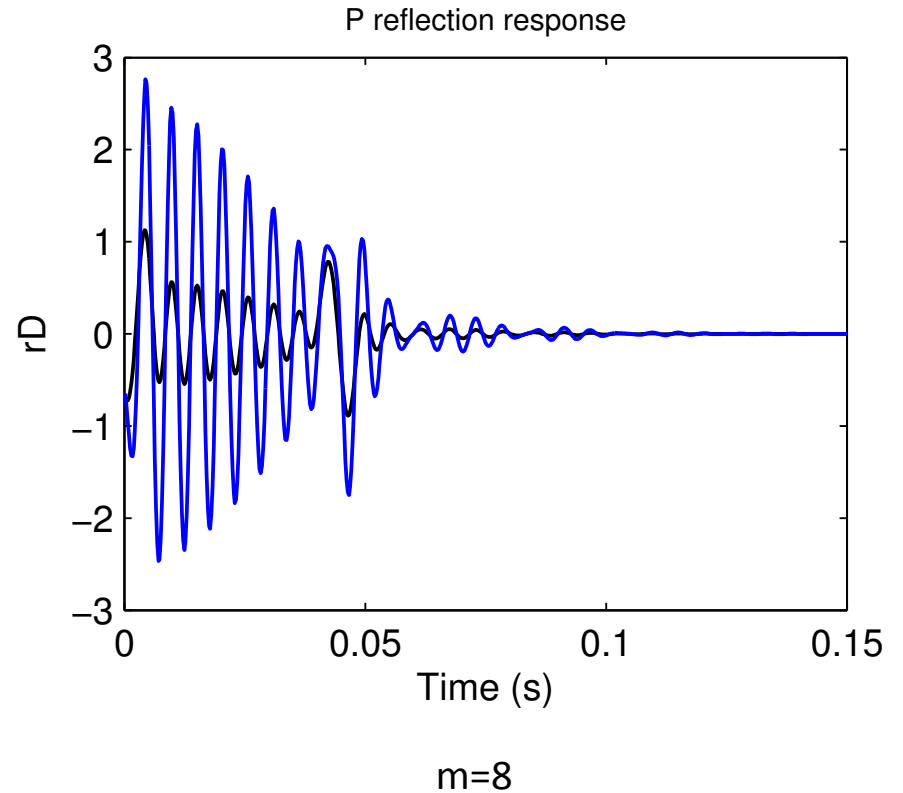
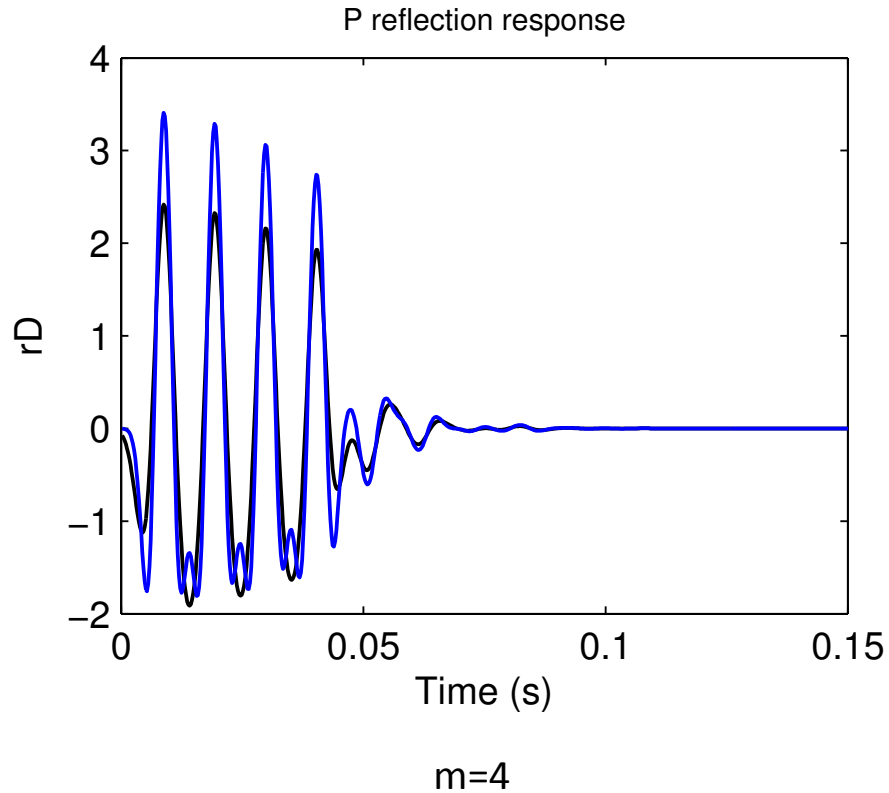
$m=1$



$m=2$

- Anelastic sand layers
- Elastic sand layers (no dispersion)

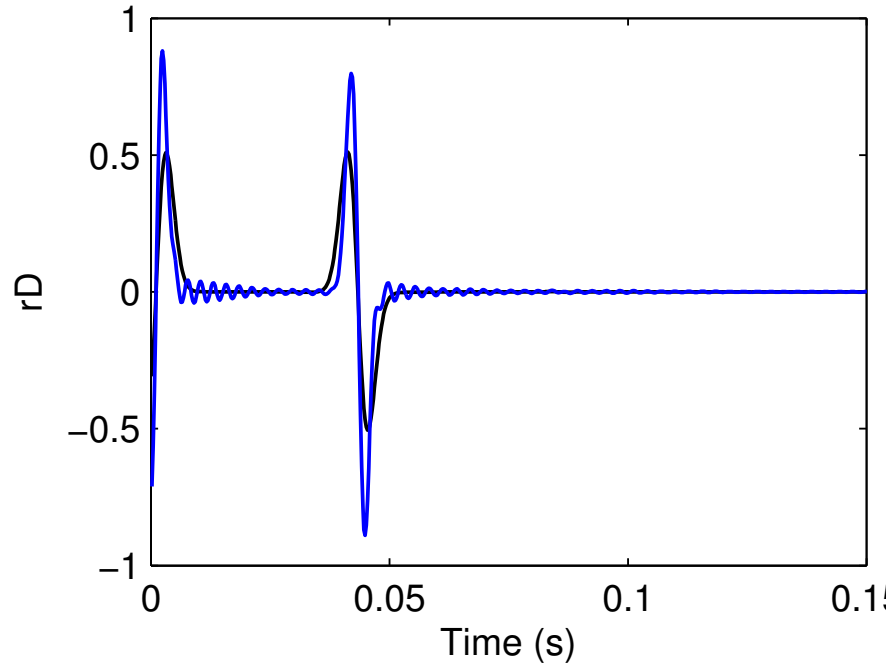
R/T time responses ($\phi=32\%$): resonance for $m=4$ and $m=8$



- Anelastic sand layers
- Elastic sand layers (no dispersion)

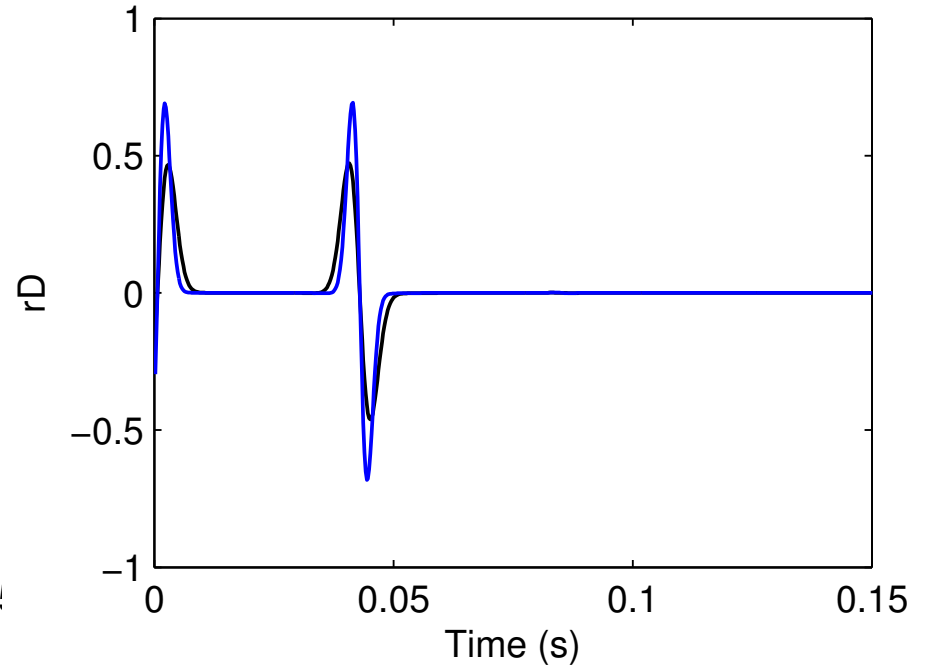
R/T time responses ($\phi=32\%$): effective medium for $m=16$ and $m=32$

P reflection response



$m=16$

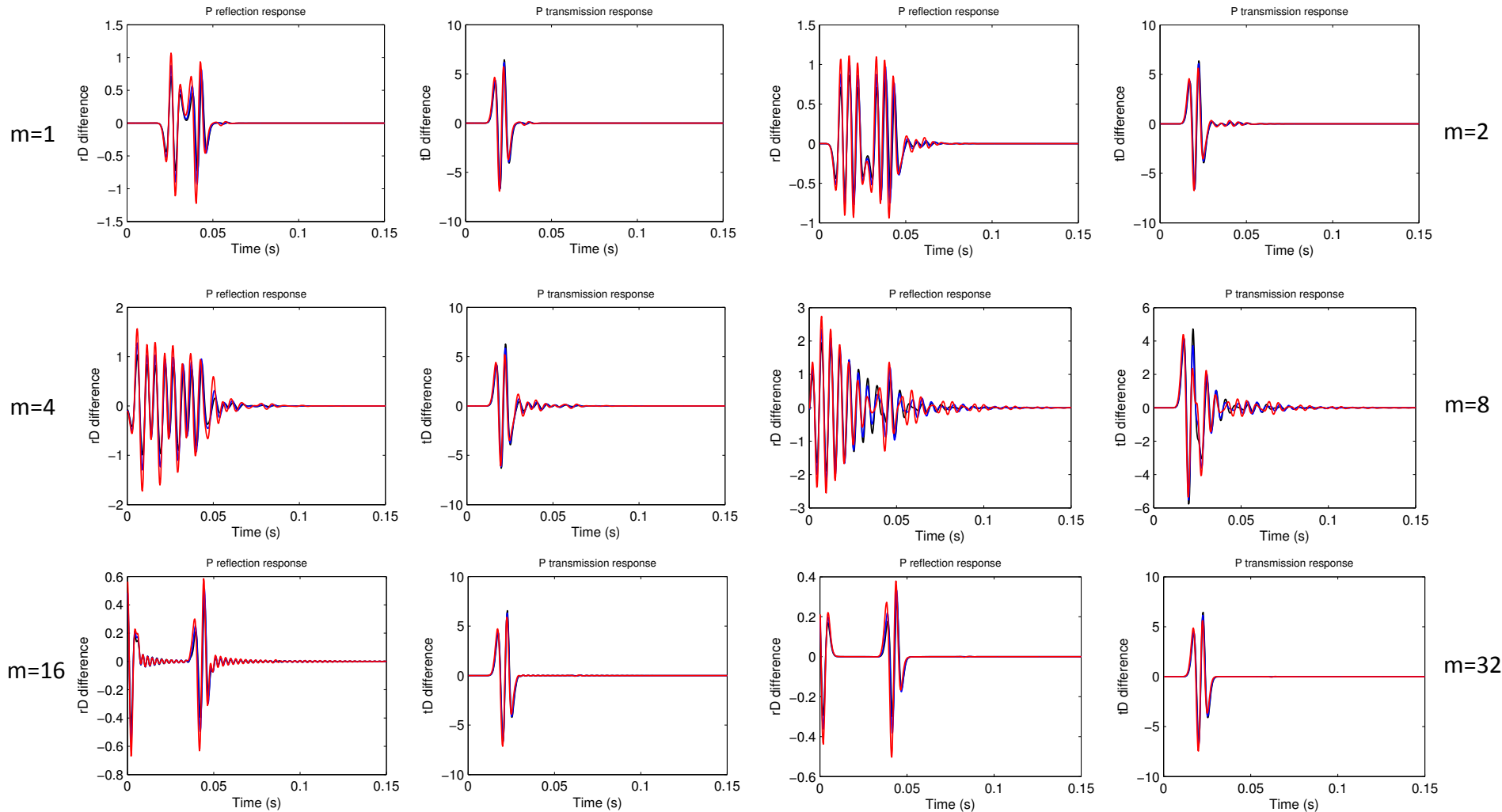
P reflection response



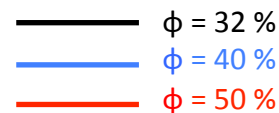
$m=32$

- Anelastic sand layers
- Elastic sand layers (no dispersion)

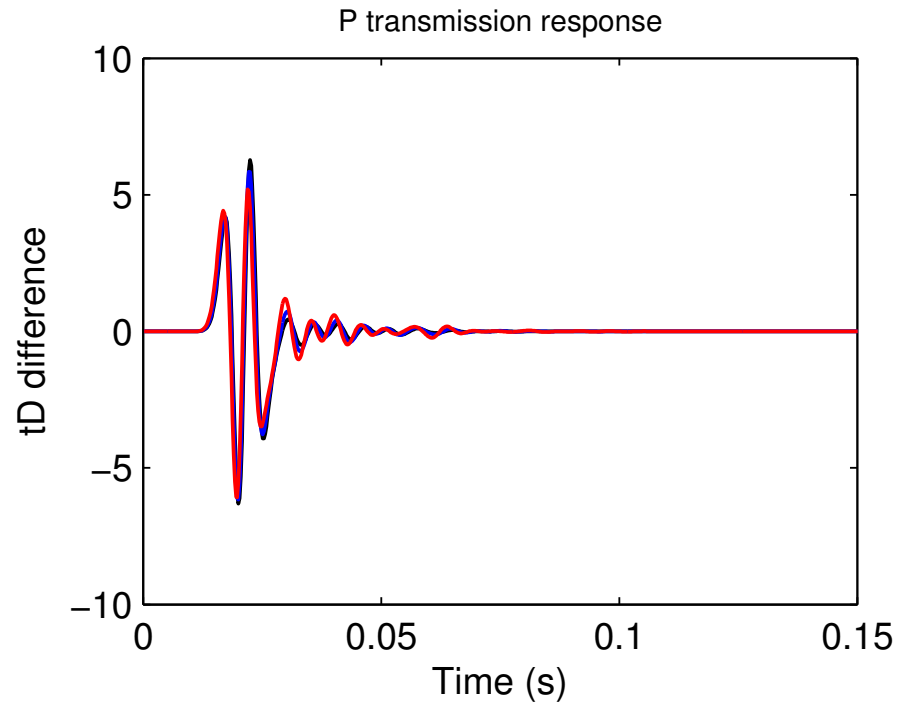
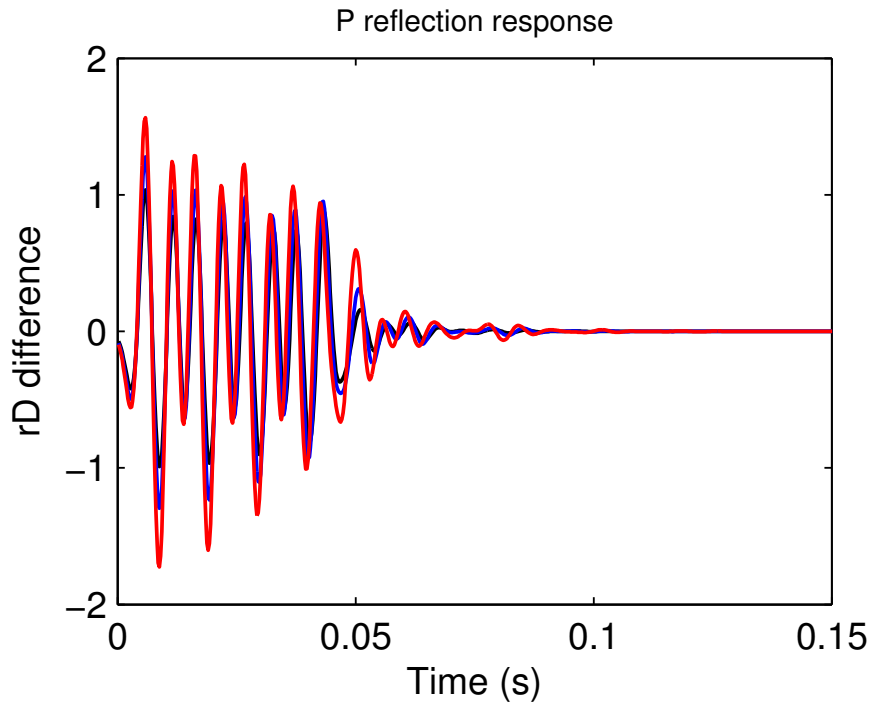
R/T time responses differences



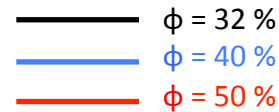
Difference between anelastic and equivalent elastic layers for:



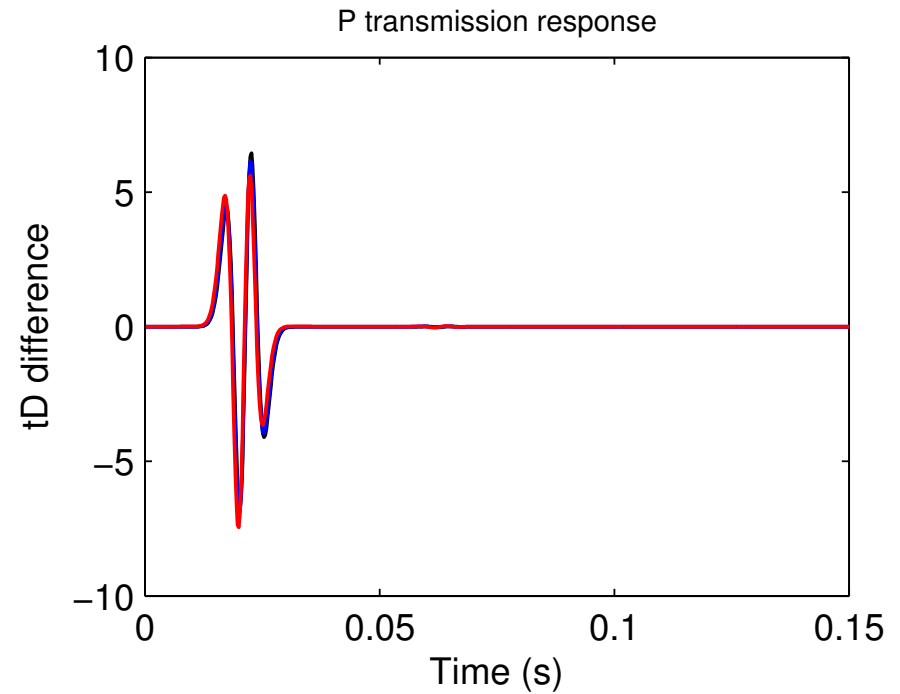
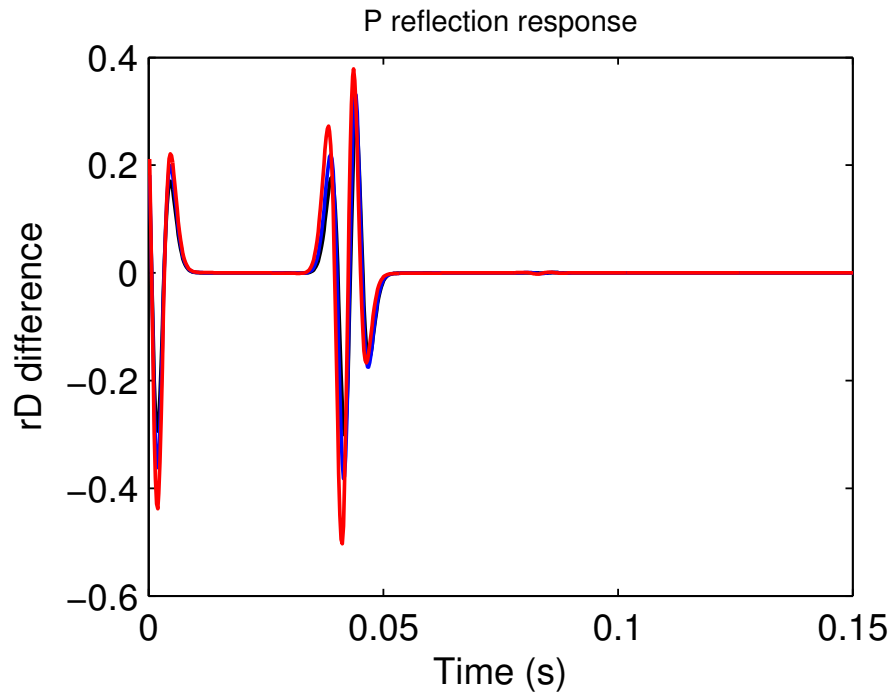
R/T time responses differences (m=4)



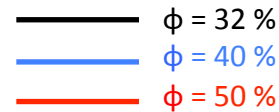
Difference between anelastic and equivalent elastic layers for:



R/T time responses differences ($m=32$)



Difference between anelastic and equivalent elastic layers for:



Conclusions

- 3 porosity models = 3 levels of dispersion → dispersion and attenuation peak frequency around 50 Hz
- Frequency domain:
 - The differences between anelastic and elastic R/T responses increase when porosity increases
 - The layering generally dominates the responses (for realistic porosities)
 - The number of resonance peaks is higher when the number of cycles decreases. These peaks are more pronounced when m increases.
 - If we consider weaker contrast between the 2 layers (here, rP is about 0.11 to 0.17), the effect of anelasticity could be stronger.

Conclusions

- Time domain:

- Typical elastic behavior: reflected events, resonance system and then, effective medium are observed when m increases.
- On the contrary to frequency domain results, the anelasticity has a strong influence on the amplitude of responses

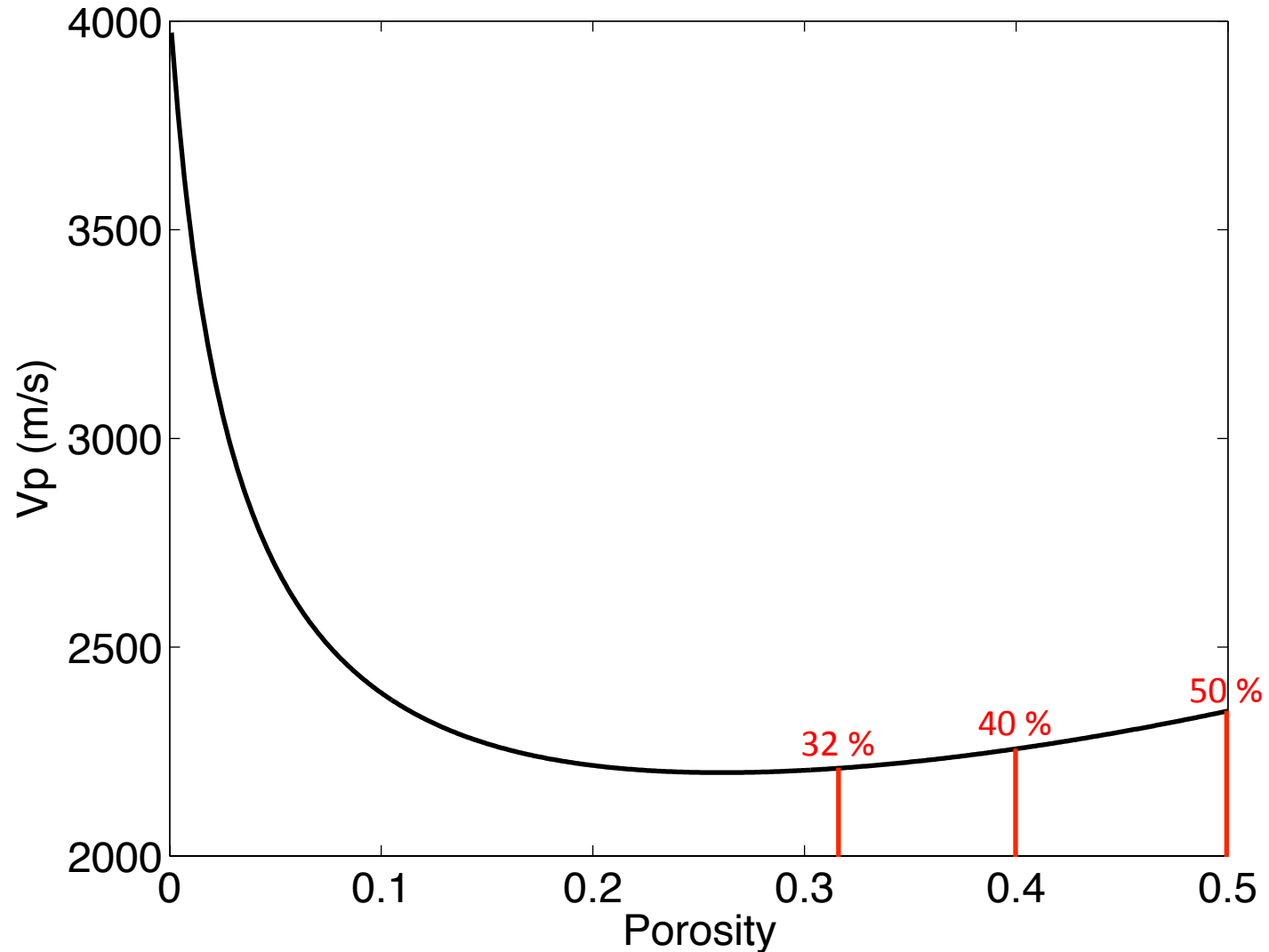
➔ Important conclusion when we deal with seismic interpretation of a layered system: the dispersion and attenuation of the effective R/T responses **are not only due to the layering and can be controlled by intrinsic anelasticity of layers.**

- Acknowledgements:
 - The ROSE project for financial support

- Bibliography:
 - Stovas and Ursin (2003). *Reflection and transmission responses of a layered transversely isotropic visco-elastic media*, GP
 - Pride, Berryman and Harris (2004). *Seismic attenuation due to wave-induced flow*, JGR
 - White (1975), *Computed seismic speeds and attenuation in rocks with partial gas saturation*, Geophysics
 - Dupuy and Stovas (2014). *Reflection and Transmission Responses of a Periodic Layered Medium Constituted by Shales and patchy Saturated Sands*, EAGE expanded Abstract 2014

V_p with respect to the porosity

P-wave velocity



Model

Layers 1 = shales

$$V_p = 5500 \text{ m/s}$$

$$V_s = 3000 \text{ m/s}$$

$$\rho = 2700 \text{ kg/m}^3$$

Elastic, frequency-independent

Layers 2 = partially saturated sandstones

Gas saturation = 10 %

Patchy saturation: frequency-dependent

OR

Equivalent elastic layer: frequency-independent



K_s	(GPa)	40			
ρ_s	(kg/m ³)	2690			
m		1			
ϕ		0.32			
k_0	(m ²)	$9 \cdot 10^{-10}$			
K_D	(GPa)	4			
G_D	(GPa)	3			
K_{f_1} (water)	(GPa)	3.01			
K_{f_2} (gas)	(GPa)	0.13			
ρ_{f_1} (water)	(kg/m ³)	1055			
ρ_{f_2} (gas)	(kg/m ³)	336			
η_1 (water)	(Pa.s)	0.001			
η_2 (gas)	(Pa.s)	0.00004			
a	(cm)	1			
V_1		0.1	0.2	0.8	0.9
V_P	(m/s)	2085	2077	2107	2192
V_S	(m/s)	1259	1253	1197	1189
V_{Biot}	(m/s)	580	640	311	414
Q_P		74	70	94	153
Q_S		44	39	44	39
Q_{Biot}		1.70	1.57	0.83	0.72
ρ	(kg/m ³)	1960	1983	2121	2144
f_c	(Hz)	7.3	8.1	22	32

Computation of R/T responses

Propagator matrix for 1 cycle (2 layers):

$$\mathbf{S}_k(\omega) = \frac{1}{1-r^2(\omega)} \begin{pmatrix} e^{i\theta_1} & 0 \\ 0 & e^{-i\theta_1} \end{pmatrix} \begin{pmatrix} 1 & r(\omega) \\ r(\omega) & 1 \end{pmatrix} \begin{pmatrix} e^{i\theta_2(\omega)} & 0 \\ 0 & e^{-i\theta_2(\omega)} \end{pmatrix} \begin{pmatrix} 1 & -r(\omega) \\ -r(\omega) & 1 \end{pmatrix}$$

$$\mathbf{S}_k(\omega) = \begin{pmatrix} a_k(\omega) & b_k(\omega) \\ c_k(\omega) & d_k(\omega) \end{pmatrix},$$

$$a_k(\omega) = \frac{1}{t_1 t_2(\omega)} \left(e^{i(\theta_1 + \theta_2(\omega))} \left(1 - r^2(\omega) e^{-2i\theta_2(\omega)} \right) \right),$$

$$b_k(\omega) = \frac{1}{t_1 t_2(\omega)} \left(-r e^{i(\theta_1 + \theta_2(\omega))} + r(\omega) e^{i(\theta_1 - \theta_2(\omega))} \right),$$

$$c_k(\omega) = \frac{1}{t_1 t_2(\omega)} \left(r e^{i(\theta_1 - \theta_2(\omega))} - r(\omega) e^{-i(\theta_1 + \theta_2(\omega))} \right),$$

$$d_k(\omega) = \frac{1}{t_1 t_2(\omega)} \left(e^{-i(\theta_1 + \theta_2(\omega))} \left(1 - r^2(\omega) e^{2i\theta_2(\omega)} \right) \right).$$

$r(\omega)$ = reflection coefficient
 t_1 and $t_2(\omega)$ = traveltimes
 θ_1 and $\theta_2(\omega)$ = phase factors

$$r(\omega) = \frac{\rho_2 V_2(\omega) - \rho_1 V_1}{\rho_2 V_2(\omega) + \rho_1 V_1},$$

$$\theta_1 = \frac{2\pi f d_1}{V_1} = 2\pi f t_1,$$

$$\theta_2(\omega) = \frac{2\pi f d_2}{V_2(\omega)} = 2\pi f t_2(\omega),$$

Equations valid for P- or S-waves independently