

# Resolution of 3D Elastic Full Waveform Inversion

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# Outline

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- The Elastic Wave Equation

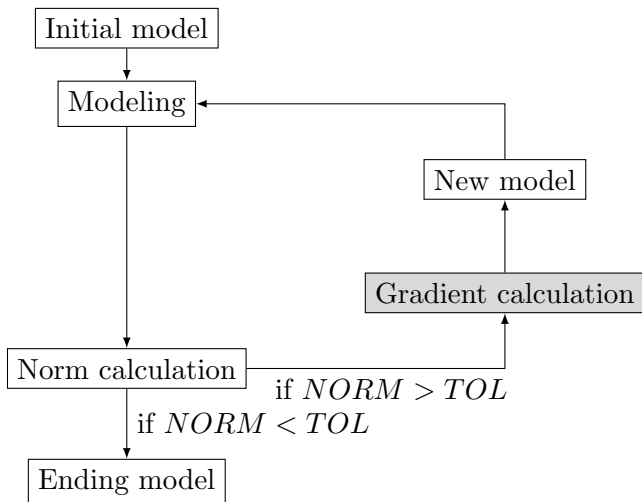
## The Misfit Functionals

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- Gradients
- Numerical Results

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- References

# Full Waveform Inversion



# The Elastic Wave Equation

Wave equation for the particle displacement  
([Aki and Richards, 2002])

$$\rho(x)\ddot{u}_i(x, t) = \partial_j \tau_{ij}(x, t) + f_i(x, t) \quad (1)$$

$$\tau_{ij}(x, t) = c_{ijkl}(x) \partial_l u_k(x, t) - I_{ij}(x, t) \quad (2)$$

$\rho$ : density,  $u$ : particle displacement,  $\tau_{ij}$ : stress tensor,  $f$ : body force,  $c_{ijkl}$ : stiffness tensor,  $I_{ij}$ : volume force.

Wave equation for the stress tensor

$$s_{pqij}(x)\ddot{\tau}_{ij}(x,t) = \frac{1}{2} \left[ \partial_q \left( \frac{1}{\rho(x)} \partial_j \tau_{pj}(x,t) \right) + \partial_p \left( \frac{1}{\rho(x)} \partial_j \tau_{qj}(x,t) \right) \right] \\ + \frac{1}{2} \left[ \partial_q \left( \frac{1}{\rho(x)} f_p(x,t) \right) + \partial_p \left( \frac{1}{\rho(x)} f_q(x,t) \right) \right] \\ + \ddot{Q}_{ij}(x,t), \quad (3)$$

$$e_{qp}(x,t) = s_{pqij}(x)\tau_{ij}(x,t) - Q_{pq}(x,t) \quad (4)$$

$s_{pqij}$ : compliance tensor,  $e_{qp}$ : strain,  $Q_{pq}(x,t) = s_{pqij}(x)I_{ij}(x,t)$ : volume source.

# Modeling

- Full three dimensional elastic modeling.
- Staggered finite difference method described by Virieux ([Virieux, 1986]).
- Perfectly Matched Layer (PML) ([Zhen et al., 2009]) used as Absorbing Boundary Conditions (ABCs).
- Free surface modeled using approach by Mittet ([Mittet, 2002]).
- Problems: Large memory requirements, computer time, parallellization, etc.

## The Misfit Functionals

### General definition

$$\Psi(d, f(m)) = C \int_T \int_{\Omega_r} W(d, f(m)) dS dt, \quad (5)$$

Three cases investigated further;

$$\Psi_{L^1}(d, f(m)) = \int_T \int_{\Omega_r} |d - f(m)| dS dt, \quad (6)$$

$$\Psi_{L^2}(d, f(m)) = \frac{1}{2} \int_T \int_{\Omega_r} (d - f(m))^2 dS dt, \quad (7)$$

$$\Psi_C(d, f(m)) = \frac{1}{2} \int_T \int_{\Omega_r} \ln(1 + (d - f(m))^2) dS dt. \quad (8)$$

$\Omega_r$ : receiver surface,  $T$ : time interval,  $d$ : measured field,  $f(m)$ : modeled field.

# Gradients

## General formulation

$$\nabla_m \Psi = \int_T \frac{\partial W(d, f(m))}{\partial f(m)} \frac{\partial f(m)}{\partial m} dt \quad (9)$$

See [Fichtner, 2011].

- Dependent on how the problem is parametrized; i.e. Lamé parameters, velocities, etc.
- Problem: Due to computer power “impossible” to find the Fréchet kernel.
- Solution: Tarantola ([Tarantola, 1984]) forward/backward wave field formulation.



The general forward/backward gradients:

$$\nabla_{\rho} \Psi = - \int_T \int_{\Omega} \dot{u}_p(t) \left[ \dot{\Gamma}_{pij}^0(-t) * \frac{\partial W(d, f(m))}{\partial f(m)} \right] dV dt, \quad (10)$$

$$\nabla_{\Lambda} \Psi = - \int_T \int_{\Omega} \tau_{nn}(t) \left[ \Gamma_{ppij}^0(-t) * \frac{\partial W(d, f(m))}{\partial f(m)} \right] dV dt, \quad (11)$$

$$\nabla_M \Psi = - \int_T \int_{\Omega} \tau_{np}(t) \left[ \Gamma_{npij}^0(-t) * \frac{\partial W(d, f(m))}{\partial f(m)} \right] dV dt, \quad (12)$$

where

$$\Lambda = -\frac{\lambda}{2\mu(3\lambda + 2\mu)} \quad \text{and} \quad M = \frac{1}{4\mu}. \quad (13)$$

Conversion between parameters is done by using differential calculus.

## Principle formulas for gradients

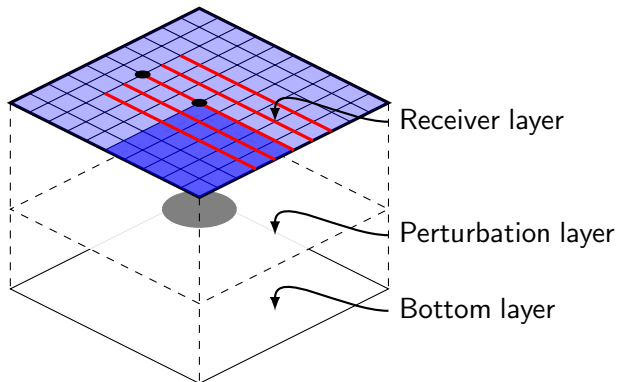
$$\nabla_{\rho} \Psi = C_{\rho} \int_T (\vec{v}_z + \vec{v}_x + \vec{v}_y) (\overleftarrow{v}_z + \overleftarrow{v}_x + \overleftarrow{v}_y) dt, \quad (14)$$

$$\nabla_{v_p} \Psi = C_{v_p} \int_T (\overrightarrow{\tau}_{zz} + \overrightarrow{\tau}_{xx} + \overrightarrow{\tau}_{yy}) (\overleftarrow{\tau}_{zz} + \overleftarrow{\tau}_{xx} + \overleftarrow{\tau}_{yy}) dt, \quad (15)$$

$$\nabla_{v_s} \Psi = C_{v_s} \int_T (\overrightarrow{\tau}_{zx} + \overrightarrow{\tau}_{yx} + \overrightarrow{\tau}_{zy}) (\overleftarrow{\tau}_{zx} + \overleftarrow{\tau}_{yx} + \overleftarrow{\tau}_{zy}) dt. \quad (16)$$

$v$ : particle velocity,  $\tau_{ij}$ : stress tensor,  $C_i$ : constant dependent on parameter under consideration.

## Numerical Results

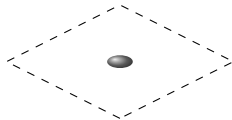


- 500 meters grid in each direction; sampling 5 meters.
- Four source-receiver geometries: one-shot-many-receivers geometries.

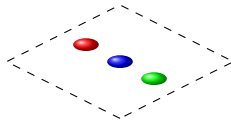
## Source-receiver geometries

- G1: The receivers are placed in the whole receiver layer, and the source is in the middle of this layer.
- G2: The receivers are placed in a square which is one quarter of the full layer. The source is placed in the middle of the full layer, i.e. on the corner of the square.
- G3: The receivers consist of eight streamers that are separated by 50 meters. The streamers are placed in the middle of the receiver layer. The source is placed in front of the middle streamers.
- G4: The receivers consist of a single streamer, which is placed in the middle of the receiver layer. The source is in front of the streamer.

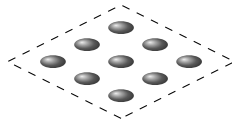
# Perturbation layer



(a)



(b)



(c)

(a): model 1, (b): model 2, (c): model 3.

## Resolution matrix

In matrix notation

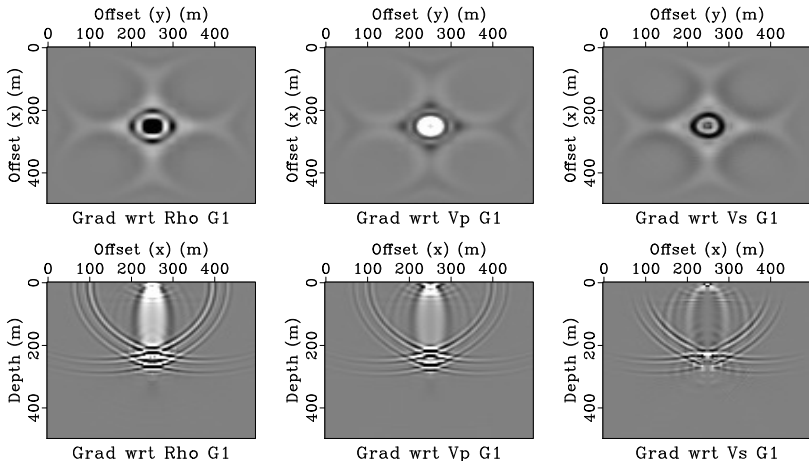
$$\Delta \hat{v}_p = c \nabla_{v_p} \Psi(d, f(m)) = c \mathbf{J}^T \mathbf{J} \Delta v_p, \quad (17)$$

$$\Delta \hat{v}_p = c \mathbf{R} \Delta v_p, \quad (18)$$

$\mathbf{R} = \mathbf{J}^T \mathbf{J}$ : resolution matrix,  $c$ : gradient constant.

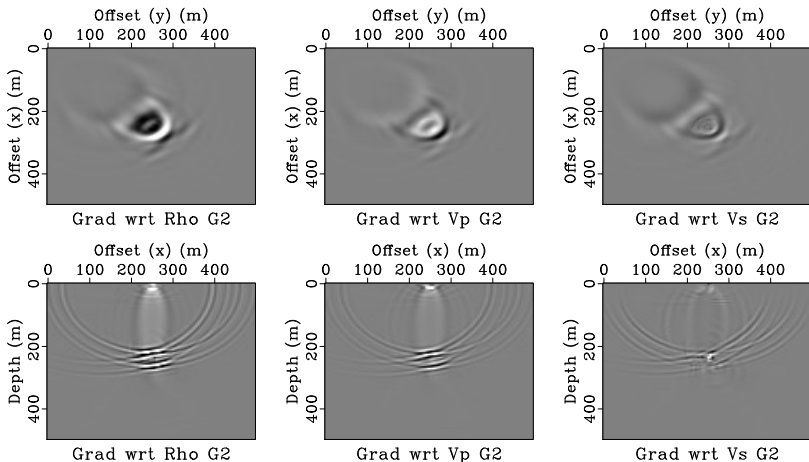
$$R \Delta v_p = \begin{bmatrix} R_{11} & R_{12} & \dots & R_{1n} \\ R_{21} & R_{22} & \dots & R_{2n} \\ \vdots & \vdots & & \vdots \\ \vdots & \vdots & \ddots & \vdots \\ \vdots & \vdots & & \vdots \\ R_{(m-1)1} & R_{(m-1)2} & \dots & R_{(m-1)n} \\ R_{m1} & R_{m2} & \dots & R_{mn} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \vdots \\ \Delta v_{p,k} \\ \vdots \\ 0 \\ 0 \end{bmatrix} \quad (19)$$

## $L^2$ gradient images: Model 1



Geometry 1; *top*: Horizontal slice at 250 m depth, *bottom*: vertical slice at 250 m offset.

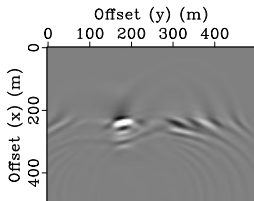
## $L^2$ gradient images: Model 1



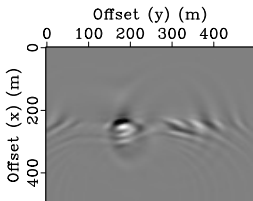
Geometry 2; *top*: Horizontal slice at 250 m depth, *bottom*: vertical slice at 250 m offset.



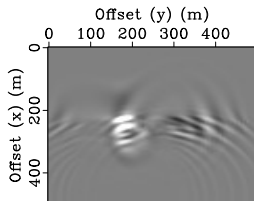
## $L^2$ gradient images: Model 1



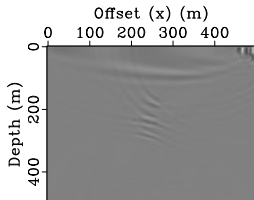
Grad wrt Rho G3



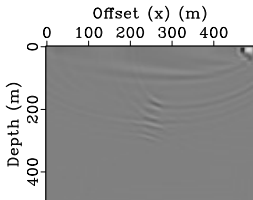
Grad wrt Vp G3



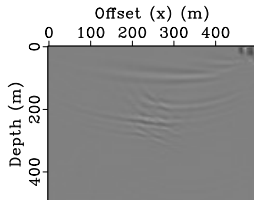
Grad wrt Vs G3



Grad wrt Rho G3



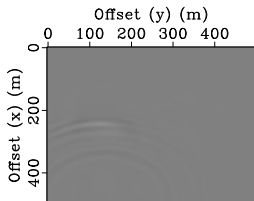
Grad wrt Vp G3



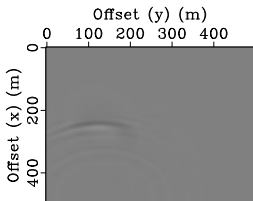
Grad wrt Vs G3

Geometry 3; *top*: Horizontal slice at 250 m depth, *bottom*: vertical slice at 250 m offset.

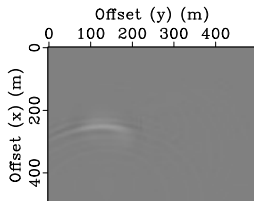
## $L^2$ gradient images: Model 1



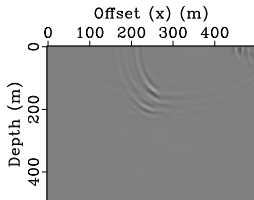
Grad wrt Rho G4



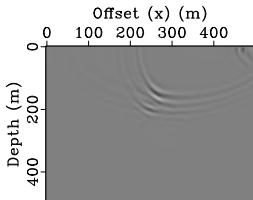
Grad wrt Vp G4



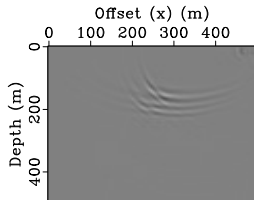
Grad wrt Vs G4



Grad wrt Rho G4



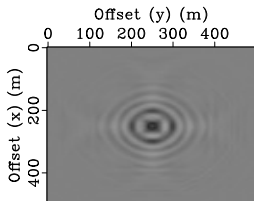
Grad wrt Vp G4



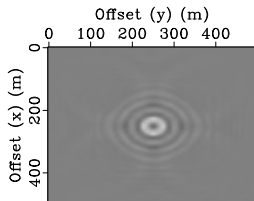
Grad wrt Vs G4

Geometry 4; *top*: Horizontal slice at 250 m depth, *bottom*: vertical slice at 250 m offset.

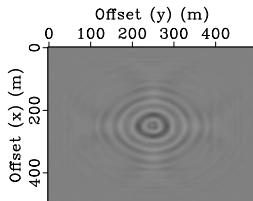
# $L^1$ gradient images: Model 1



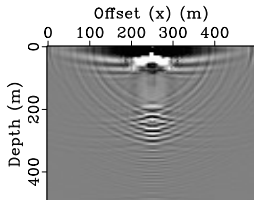
Grad wrt Rho G1



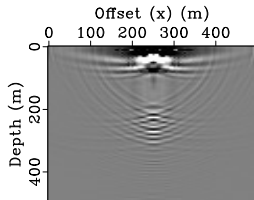
Grad wrt Vp G1



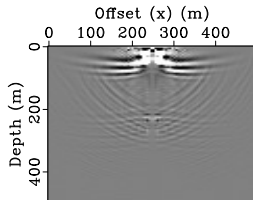
Grad wrt Vs G1



Grad wrt Rho G1



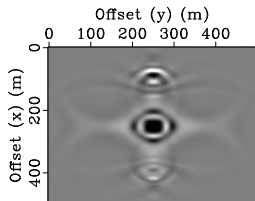
Grad wrt Vp G1



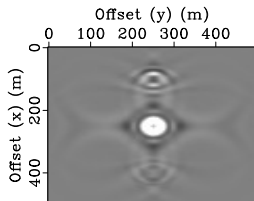
Grad wrt Vs G1

Geometry 1; *top*: Horizontal slice at 250 m depth, *bottom*: vertical slice at 250 m offset.

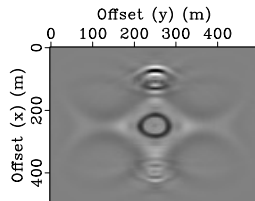
## Gradient images: Model 2



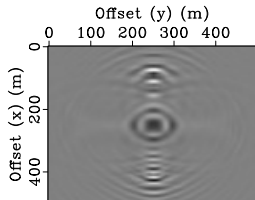
Grad wrt Rho G1



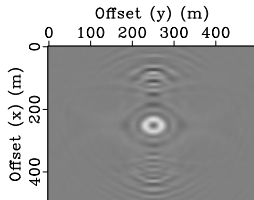
Grad wrt Vp G1



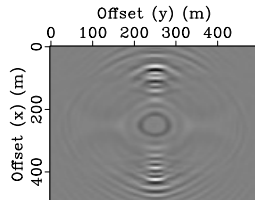
Grad wrt Vs G1



Grad wrt Rho G1



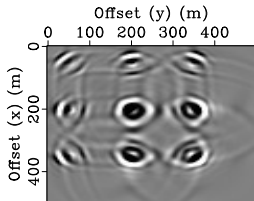
Grad wrt Vp G1



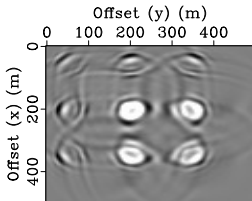
Grad wrt Vs G1

Geometry 1, horizontal slices at 250 m depth; *top*:  $L^2$ -norm,  
*bottom*:  $L^1$ -norm.

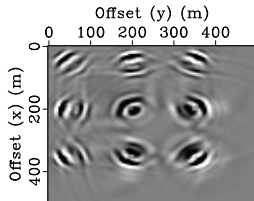
## Gradient images: Model 3



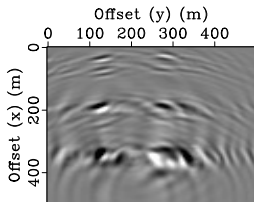
Grad wrt Rho G1



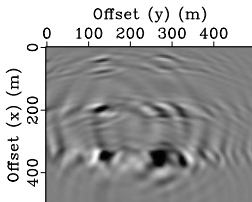
Grad wrt Vp G1



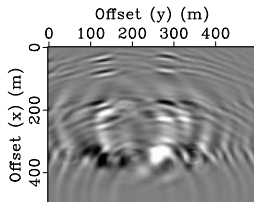
Grad wrt Vs G1



Grad wrt Rho G3



Grad wrt Vp G3



Grad wrt Vs G3

$L^2$ -norm, horizontal slices at 250 m depth; *top*: Geometry 1,  
*bottom*: Geometry 3.

## Summary

- The source-receiver geometry has *major* impact on the gradient.
- Denser receiver grid gives more focusing of the gradient.
- Many receivers compared to few receivers give better focusing. Conclusion: Use as many receivers as possible and put the source in the middle of the receiver grid.
- Coupled gradients.
- Different numerical artifacts for the gradients:  $L^1$  seems to be the worst.
- The Cauchy and  $L^2$  gradients have the same properties.

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# Acknowledgments

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